



Landfill Gas Extraction Feasibility Study

Eloy S. Inos Peace Park

(formerly Puerto Rico Dump) and Marpi Solid Waste Facility Commonwealth of the Northern Mariana Islands

> Prepared for Commonwealth of the Northern Mariana Islands Capital Improvement Projects Office of the Governor

Prepared by EA Engineering, Science and Technology, Inc., PBC 1001 Army Drive, Suite 103 Barrigada, Guam 96913 (671) 646-5231

US Department of Interior Empowering Insular Communities Grant 017AP00092

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LIST OF ACRONYMS AND ABBREVIATIONS

°F % %v/v	Degree Fahrenheit Percent Percent volume per volume
Btu BECQ	British thermal unit Bureau of Environmental and Coastal Quality
cfm CNMI	Cubic feet per minute Commonwealth of the Northern Mariana Islands
EA EPA	EA Engineering, Science, and Technology, Inc., PBC U.S. Environmental Protection Agency
ft	Foot (feet)
hr	Hour(s)
in.	Inch(es)
kW kWh	Kilowatt(s) Kilowatt-hour(s)
LFG	Landfill gas
min MSW MSWF	Minute(s) Municipal solid waste Marpi Solid Waste Facility
ND NMOC NPV	Non-detect Non-methane organic compound Net present value
O&M	Operation and maintenance
ppmv ppmv-C PRD	Part(s) per million by volume Part(s) per million by volume as carbon Puerto Rico Dump
scf	Standard cubic foot (feet)
RCRA	Resource Conservation and Recovery Act
TNMOC	Total non-methane organic compound

1. INTRODUCTION

EA Engineering, Science, and Technology, Inc., PBC (EA) was contracted by the Commonwealth of the Northern Mariana Islands (CNMI) Office of Grants Management, Office of the Governor, to perform a Landfill Gas (LFG) Extraction Feasibility Study at two landfills on Saipan: Eloy S. Inos Peace Park, formerly known as the Puerto Rico Dump (PRD), and the Marpi Solid Waste Facility (MSWF), also known as the Marpi Landfill (RFP18-OGM-045). The work to complete the feasibility study includes characterization of waste, assessment of LFG generation potential and techniques to increase gas generation, and conceptual design of a LFG collection system at each site. In addition, regulatory requirements, potential LFG beneficial uses, and economic viability are discussed.

The CNMI, a U.S. territory, is a 14-island archipelago in the North Pacific Ocean. Both the Eloy S. Inos Peace Park, formerly the Puerto Rico Dump, and the Marpi Solid Waste Facility are located on the CNMI island of Saipan, CNMI's capital. As of 2015, the island had a population of approximately 48,000 with a substantial influx of tourists (U.S. Census Bureau 2015). Recently, large-scale tourism has been the main economic driver in the CNMI. From 1983 to 2004, the garment industry was a principal source of revenue on the island; however, the industry plummeted thereafter due to tariff and trade barriers (*Saipan Tribune* 2005). The climate of Saipan is tropical, hot and humid all year round, with daytime temperature ranging from 82 to 84 degrees Fahrenheit (°F) in the coolest period and 86 to 88 °F in the warmest, with an average humidity of 79 percent (%) (World Climate Guide 2018). There are two main seasons in Saipan: a relatively cool and dry season from December to June, and a warmer and rainy season from July to November. Rainfall is abundant and mean annual rainfall is approximately 80 in. in Saipan.

1.1 ELOY S. INOS PEACE PARK (FORMERLY THE PUERTO RICO DUMP)

The PRD is a 20-acre facility located in the town of Puerto Rico, Saipan, at the edge of Tanapag Lagoon and adjacent to an oil terminal, approximately 3,500 feet (ft) northeast of Garapan village (Figure 1-1). It is bordered by Tanapag Lagoon on the northwest and southwest, by a dock on the northeast, and by land on the southeast.

PRD began operation as a military heavy scrap metal dump as early as 1945. Debris was initially dumped directly onto sediment in a backwater area of Tanapag Lagoon. Ownership of PRD was transferred to the CNMI government in 1978, which leased the dump to the U.S. Navy from 1983 to 1988. CNMI closed the dump to waste disposal on 11 February 2003 after opening the Resource Conservation and Recovery Act (RCRA) Subtitle D Marpi Solid Waste Management facility (CNMI PRD Closure Alternative Analysis [EA 2011a]). After an Administrative Order of Consent issued by the U.S. Environmental Protection Agency (EPA) in 2005 to prevent continued discharge of leachate into Tanapag Lagoon, PRD was closed and capped in 2011. In order to improve environmental quality and the tourism industry, PRD was converted to a community park (Eloy S. Inos Peace Park) in compliance with the federal regulations and was finally completed in March 2017.

EA Engineering, Science, and Technology, Inc., PBC



Figure 1-1 Eloy S. Inos Peace Park

1.2 MARPI SOLID WASTE FACILITY

The MSWF is located in Saipan Municipality, Saipan. The landfill was designed in 2002 to include six cells with a total design capacity of 2.5 million cubic yards in a 25-acre lined facility (Harding ESE 2002). The MSWF was designed as a RCRA Subtitle D compliant municipal solid waste (MSW) landfill, with the goal for the new facility to bring Saipan into compliance with federal environmental regulations and utilize state-of-the-art waste reduction and diversion technologies to the island. The full build-out of the facility will include site support facilities (truck weigh scales and scale house, office building, and maintenance building), drop-off areas, leachate storage facilities, water and wastewater systems, stormwater control systems, fuel storage systems, and site access roads and parking.

Cell 1 of the MSWF began operation in 2003, with filling operations anticipated to continue through 2019. The cell was constructed with a landfill liner system including a geosynthetic clay liner, 60-mil high-density polyethylene geomembrane, and geocomposite drainage layer. Leachate collection within the cell consists of a rock drainage layer with high-density

polyethylene header and lateral pipes, and sump riser pipes for leachate removal. Currently, waste acceptance is expected to continue in Cell 1 until Cell 2 is ready for waste acceptance.



Figure 1-2 Marpi Solid Waste Facility

1.3 REGULATORY REQUIREMENTS

Under the 1991 Clean Air Act, 40 Code of Federal Regulations Part 60 Subpart WWW – Standards of Performance for MSW Landfills, and 40 Code of Federal Regulations 60.32c Amendments, landfills with a permitted capacity greater than 2.5 million tons and annual nonmethane organic compound (NMOC) emissions greater than 50 megagrams are subject to the New Source Performance Standards. When NMOC exceeds 50 megagrams per year, as determined by Tier I or Tier II analysis, the site is obligated to install a LFG emissions collection and control system. Given that the PRD and Marpi landfills are smaller than the federal threshold, and that observed NMOC is lower than regulatory thresholds, installation of a LFG emissions collection and control system is not required, and neither Tier I nor Tier II analysis is required at PRD (EA 2011b), nor MSWF.

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Eloy S. Inos Peace Park (formerly Puerto Rico Dump) Landfill Gas Extraction Feasibility Study and Marpi Solid Waste Facility, Commonwealth of the Northern Mariana Islands

2. HISTORICAL, CURRENT, AND FUTURE WASTE ACCEPTANCE RATES

The most important information to estimate future LFG generation rate and total potential lifetime LFG generation from a solid waste landfill is the amount, type, and location of waste placed in the landfill and projected to be placed there during the remaining landfill life. Waste characterization for the Eloy S. Inos Peace Park, formerly PRD, and the MSWF are discussed in this chapter.

2.1 PUERTO RICO DUMP

During its operation between 1945 and 2003, PRD received military waste including unexploded ordnance and metal scrap, commercial and household waste, batteries, and garment factory wastes. Due to a thriving garment industry during PRD's operation, it is estimated that up to 33% of Saipan's solid waste stream may have been garment waste (Earth Tech, Inc. 2006).

The total volume of PRD is estimated to be approximately 1.75 million cubic yards (AECOM 2011). However, in order to assess LFG generation potential only the total biodegradable waste placed is considered for LFG generation potential. The total biodegradable waste is estimated to be approximately 260,000 tons placed between 1975 and landfill closure in 2003 above elevation 10 ft, based on findings that organic waste placed below elevation 10 ft may have been burned during waste fires attributed to unexploded ordnance explosions, or has decayed since its original placement (AECOM 2011). Of the biodegradable waste placed be approximately 260,000 tons per year.

The PRD waste characteristics are summarized in Table 2-1.

Summary Item	PRD
Operational Status	Closed in 2003 and capped in 2011;
	biodegradable waste volume placed
	between 1975 and landfill closure in 2003
Landfill Total Area (acres)	20
Estimated Total Waste Volume (cubic yards)	1,750,000
Estimated Biodegradable Waste Volume (tons)	260,000
Average Annual Solid Waste Placement (tons per year)	9,000

 Table 2-1
 Summary of Puerto Rico Dump Waste Characterization

2.2 MARPI SOLID WASTE FACILTY

Since Cell 1 began waste acceptance in 2003, the MSWF has been primarily used for disposal of MSW and other non-hazardous waste, including light industrial and textile waste, green waste, special waste, free waste, and inert waste. Detailed waste records have been maintained during the life of the facility and are provided in Appendix A. Unlike PRD, garment waste comprises a much smaller fraction of the waste stream due to closure of many of the garment industry facilities previously located on the island. Diverted materials, such as green waste, soil, concrete, cardboard, white goods (fridges, stoves, washers, dryers), used tires, glass,

office paper, aluminum, old newsprint, and plastic bottles, are removed from the waste stream prior to waste placement within Cell 1.

CNMI waste records indicate that between 2003 and 2017, the MSWF received and managed approximately 554,000 tons of material, with approximately 371,000 tons landfilled after diversion (recycling rate 33%). Over the 14 years these data have been maintained, this equates to an annual average waste placement of 24,700 tons per year.

MSWF design drawings (Harding ESE 2002) note a design capacity of 2.5 million cubic yards per day of airspace volume. Assuming a waste density of 1,000 pounds per cubic yards, landfill Cells 1 through 6 may accommodate a total waste tonnage of up to 1.25 million tons. Given historical waste placement and assuming a population growth of 7% every 10 years based on recent census data (U.S. Census Bureau 2015), the MSWF may be capable of accepting waste until 2048.

The summary of total projected waste capacity and assumed parameters is provided in Table 2-2.

Summary Item	MSWF Cells 1–6			
Operational Status	Cell 1 only currently accepting waste			
Landfill Total Area (acres)	25			
Estimated Total Volume (cubic yards)	2,500,000			
Assumed Density (pounds/cubic yard)	1,000			
Total Capacity Projected (tons)	1,250,000			
Assumed Population Growth (% in 10 years)	7			

 Table 2-2
 Summary of Marpi Solid Waste Facility Waste Characterization

3. LANDFILL GAS GENERATION AND EXTRACTION POTENTIAL

3.1 LANDFILL GAS GENERATION AND COMPOSITION

Various gases are generated through the action of microorganisms that begin decomposing organic waste within 3–6 months after disposal. The rate of LFG generation caused by waste decomposition depends on the type, volume, age, and spatial distribution, and a number of environmental factors, including moisture, temperature, oxygen, and waste degradability. Typical changes in LFG composition over time are shown in Figure 3-1 below.

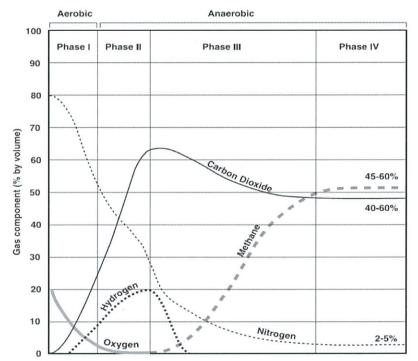


Figure 3-1 Production Phases of Typical Landfill Gas (Agency for Toxic Substances and Disease Registry 2008)

With high ambient temperature, moist climate, and low amount of compaction applied during waste placement, LFG generation would be expected to occur rapidly following placement. The LFG generation rate is highest after waste disposal, and gradually declines over decades as organic waste is depleted. Maximum LFG generation typically occurs within the first 2 years after a landfill stops accepting waste. This trend of LFG generation over time is typically incorporated into LFG models by applying a first-order exponential decay equation, which assumes that LFG generation is at its peak following a time lag (period prior to methane generation), and then decreases exponentially as the organic fraction of waste is consumed.

The goal in collecting LFG is to maximize gas collection while maintaining high gas quality, generally defined as high methane content (around 50%) and low nitrogen (less than 20%) and

oxygen (less than 5%) in the collected gas. Adequate methane content and low oxygen are necessary for energy conversion devices such as engines or boilers. Nitrogen and oxygen in collected LFG are mostly due to atmospheric air being drawn into the waste mass due to the vacuum applied by the collection system. Gas quality is important both for energy recovery and combustion, and for landfill safety (i.e., to prevent landfill fires). Typical LFG is composed of approximately half methane and half carbon dioxide, with trace quantities of NMOCs.

3.2 LANDFILL GAS SAMPLING

LFG sampling was conducted at PRD and MSWF to determine the components of gaseous emissions to estimate future LFG generation.

LFG samples were collected as part of the PRD landfill closure in 2011 and as part of the gas feasibility study at MSWF in 2018. The collected samples were analyzed for fixed gases by EPA Method 25C and total gaseous NMOCs (i.e., hexane by EPA Method 3C). Based on EPA Method 3C, samples may contain no more than 20% nitrogen, since high nitrogen concentrations may indicate air intrusion. Sampling efforts at both sites are described in additional detail below. All lab analyses were performed according to the laboratory's National Environmental Laboratory Accreditation Program and Department of Defense Environmental Laboratory Accreditation Program approved quality assurance program.

3.2.1 Puerto Rico Dump Landfill Gas Sampling Results

A total of 19 LFG sample probes were installed per the Tier II Testing Services for Puerto Rico Closure Work Plan (Puerto Rico Dump Landfill Gas Testing Method, Results and Recommendations [EA 2011b]). In June 2011, samples were collected from all probe locations; however, only 5 samples had less than 20% nitrogen, and are the basis for this LFG assessment. The 5 PRD LFG samples with less than 20% nitrogen contained typical concentrations for methane, carbon dioxide, and nitrogen. PRD LFG sampling results are summarized in Table 3-1 with sampling locations and detailed results provided in Appendix B. Sampling results show that the average methane content (%) generated from PRD was 46.1%.

	EPA	and Salarah	Sample Location					
Analyte	Method	Units	LFG-05	LFG-06	LFG-11	LFG-12	LFG-15	
Hydrogen	3C	%v/v	ND	ND	ND	ND	ND	
Argon	3C	%v/v	3.42	3.22	1.28	2.94	2.39	
Nitrogen	3C	%v/v	12.1	11.5	5.78	10.4	12.4	
Carbon Monoxide	3C	%v/v	ND	ND	ND	ND	ND	
Methane	3C	%v/v	44.3	44.7	50.8	46.1	44.5	
Carbon Dioxide	3C	%v/v	40.2	40.6	42.1	40.6	40.7	
Non-Methane Organic Compounds	25C	ppmv	11	8.9	22	20	19	
ND = Nc	rcent volume on-detect. rts per millio		ne. ne as hexane.					

Table 3-1 Puerto Rico Dump Landfill Gas Sampling Results

3.2.2 Marpi Solid Waste Facility Landfill Gas Sampling Results

Five LFG samples were collected at the MSWF on 10 July 2018 (Figure 1 in Appendix C). At the time of the sample collection the waste in Cell 1 had approximately 10–12 in. of soil cover which varied in depth and may have allowed different degrees of off-gassing. Analytical discrepancies between the samples are likely due to the incomplete status of the landfill cap; the poor cover system likely prevented a uniform accumulation of gas within the cell and the variability in the waste material impacted the depth at which the sampling gas wells were installed. Variations in waste composition, size, and degradation rates likely had impacts on localized gas concentrations. Additionally, at the time of the sample collection there was a pile of wastewater sludge on top of the cell. The pile was located on the east-central part of the cell, this area was avoided during sampling due to the high likelihood of gas production from the sludge.

MSWF LFG sampling results are summarized in Table 3-2 with sampling locations and detailed results included in Appendix C. Based on the site conditions described, NMOC results for MSWF samples were corrected at locations where nitrogen concentration was higher than 20%. After sample correction, collected MSWF LFG samples contained typical concentrations for methane, carbon dioxide, and nitrogen. Sampling results show that the average methane content (%) generated from MSWF was 60.3%.

	1.5.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		Sample Location					
Analyte	EPA Method	Units	MARPI- 1B- 071018	MARPI- 2A- 071018	MARPI- 3A- 071018	MARPI- 4A- 071018	MARPI- 5B- 071018	
			TNMOC			10 m	H. H.	
TNMOC N ₂ corrected	25C	ppmv-C	1,400	1,300	850	1,600	1,400	
TNMOC O ₂ corrected	25C	ppmv-C	1,400	1,400	890	1,600	1,400	
		Fixe	ed Gases in A	Air				
Carbon dioxide	3C	%v/v	44	25	25	42	39	
Methane	3C	%v/v	61	36	36	59	61	
Nitrogen	3C	%v/v	<3.2	37	35	<3.2	5.9	
Oxygen	3C	%v/v	<1.6	10	10	<1.6	1.6	
$\%v/v = Perprovement{Perp}{ppmv-C} = Parprovement{Perp}{prove$		per volume. h by volume a ane organic c applicable if	as carbon. ompound. nitrogen <209	%).		ing limit.		

 Table 3-2
 Marpi Solid Waste Facility Landfill Gas Analytical Results

3.3 LANDFILL GAS GENERATION POTENTIAL

Utilizing the LFG sampling results, a year-by-year estimate of LFG emissions for PRD and MSWF has been developed using EPA's Landfill Gas Emissions Model – LandGEM Version 3.02. LandGEM is a software program based on the first-order decomposition rate equation used to estimate emission rates for total LFG, methane, carbon dioxide, NMOC, and individual air pollutants from MSW landfills as described by the following relation:

$$\boldsymbol{Q}_{\mathsf{M}} = \sum_{i=1}^{n} 2 \; k \; \boldsymbol{L}_{\mathsf{o}} \boldsymbol{M}_{i} \Big(e^{-k t_{i}} \Big) \label{eq:Q_M_model}$$

Where:

- $Q_{\rm M}$ = Maximum expected gas generation flow rate, cubic meters per year.
- k = Methane generation rate constant in year ⁻¹.
- L_o = Methane generation potential in cubic meters per megagram of MSW.

 M_i = Mass of MSW placed in the ith year in megagrams.

 t_i = Age of the MSW placed in the ith year (n total years).

The equation above demonstrates that the annual volume of LFG produced in a landfill is proportional to the mass of waste in place, modified by two parameters (k and L_0), and decays exponentially with time after an initial peak. The methane generation rate constant, k, is a function of the moisture content of the waste mass, the nutrients available to the methaneforming bacteria, and the pH and temperature of the waste mass. The higher the methane generation rate constant (k), the earlier LFG generation peaks and begins to taper off. Values of k have been empirically derived by EPA based on actual field measurements at landfills. The potential methane generation capacity (L_0) represents the total potential LFG generation capacity of the waste mass and is a function of the amount of cellulose (biomass) present in the MSW. The higher the value of L_0 , the greater the total potential volume of LFG that can be generated from the waste mass. Values of L_0 have been theoretically derived by EPA based on the chemical composition of typical MSW. The LandGEM model was run utilizing methane generation rate (k) and potential methane generation capacity constant (L₀) provided by AP-42 emissions estimation guidelines (EPA 1995). These values are believed to be more realistic than the Clean Air Act default values and more representative of actual projected LFG generation rates.

Given the above model input, the model estimates the amount of LFG generated by the waste mass. The amount of LFG captured by a LFG collection system varies by the capture efficiency of the system. The volume of LFG that is captured is the volume that is available for beneficial use. Many different factors influence LFG capture efficiency, including the permeability of the final cover, distribution and number of gas wells, and design and operation of the collection system.

The following model assumptions were utilized for the LandGEM analysis at PRD and MSWF:

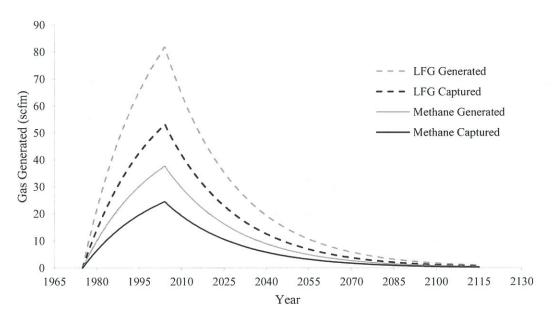
- $k = 0.040 \text{ year}^{-1}$
- $L_o = 100$ cubic meters per megagram.

A summary and discussion of LFG generation potential at each site is included below.

3.3.1 Landfill Gas Generation Potential at Puerto Rico Dump

The PRD was modeled based on waste placement from 1975 to 2003. The volume of waste from metals, industrial waste, textile debris, special waste, and free waste does not contribute to LFG generation and, therfore, was not considered in the LandGEM model (Earth Tech, Inc. 2006).

Figure 3-2 shows estimated LFG peak generation occurred in 2004, with LFG production declining thereafter. The peak gas generation rate in that year was 82 cubic feet per minute (cfm) and methane gas generation rate was 38 cfm. With active (negative pressure) LFG collection systems, overall capture efficiency can range from 60 to 90%. Since, the PRD has existing passive vents (GHD 2017), it is assumed that 65% of the total LFG produced can be captured by those shallow vents if connected to an active LFG collection system. Assuming 65% capture efficiency, the LFG and methane capture curves are also shown in Figure 3-2. The tabulated model output showing estimated gas generation for each year is provided in Appendix D.





3.3.2 Landfill Gas Generation Potential at Marpi Solid Waste Facility

The MSWF was modeled based on actual tonnage of accepted waste between 2003 and 2017, with waste disposal through 2048 projected closure. From 2003 to 2017, MSWF accepted a total of 371,000 tons of waste, of which 330,000 tons was considered biodegradable. Throughout this time, average annual waste placement was 24,711 tons per year, of which 70–80% was MSW each year (Appendix A).

For consistency with the PRD LandGEM evaluation, textile debris was excluded from the fraction of biodegradable waste. Additional items excluded from biodegradable waste capture in CNMI annual data include white waste, metals, batteries, glass, plastic bottles, and construction and demolition waste.

Figure 3-3 presents the estimated LFG and methane generation from MSWF. LandGEM estimates peak LFG generation will occur in 2049, approximately 1 year after the projected landfill closure; beyond 2049, LFG generation declines. The peak LFG generation and methane generation in 2049 was found to be 182 cfm and 109 cfm, respectively. Since, MSWF will not be capped until the end of the waste acceptance year of 2048, it is assumed that 75% of the LFG produced before 2048 may be captured by the active LFG collection system, when interim soil cover will be in place. Assuming 75% capture efficiency, the LFG and methane capture curves are also shown in Figure 3-2. The tabulated model output showing estimated gas generation for each year is provided in Appendix E.

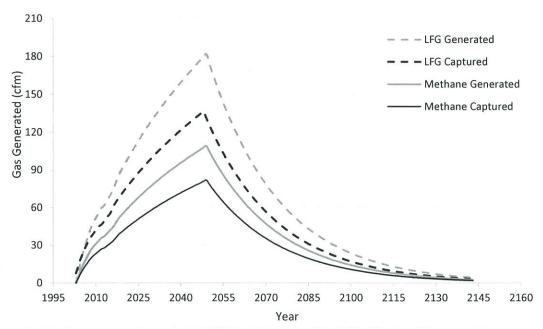


Figure 3-3 Predicted Landfill Gas and Methane Generation from MSWF

3.3.3 Landfill Gas Generation Potential Summary

Based on the findings for LFG generation potential at PRD and MSWF, the following model results summarized in Table 3-3 will be utilized in developing conceptual site design at each site, and assessing the potential for beneficial reuse of LFG captured.

For both PRD and MSWF, the initial project year is assumed to be 2025. Based on PRD having passed peak landfill gas production, beneficial energy reuse is assumed to extend to 2039. At

Eloy S. Inos Peace Park (formerly Puerto Rico Dump) Landfill Gas Extraction Feasibility Study and Marpi Solid Waste Facility, Commonwealth of the Northern Mariana Islands

MSWF, project life is significantly longer since the site continues filling operations; project life is assumed to extend until 2069, evaluated in 15-year increments for viability.

	IND	Sector & Colored and The Color	IVID VVI.	arabeel and set in the	
Parameter	2025-2039	2025-2039	2040-2054	2055-2069	
Peak Year	2004	2049			
LFG Generation (cfm) 35 (2025) ^(a) 182 (2049) ^(a)					
Average LFG Captured (cfm) ^(b)	18	102	126	82	
Average Annual Electricity Generation (kW) ^(c)	41	286	353	230	
 used for LFG collection system design at PRJ (b) Average LFG captured will be used for both 1 (c) kW capacity = 0.9^(d) * (scf LFG/min) * (60 m methane) * (kWh/11,700 Btu) (EPA 2016). (d) A gross capacity factor of 90% was applied to losses due to potential problems in the gas co interruptions of the local utilities, and shut-do 	PRD and MSW nin/hr) * (% of s o electricity gen ollection system	F beneficial rescf methane/sc neration to acc or project equ	ount for energ	12 Btu/scf by production her related	
Notes: % = Percent. Btu = British thermal unit(s). hr = Hour. kW = Kilowatt(s). kWh = Kilowatt-hour(s). min = Minute. scf = Standard cubic feet.					

 Table 3-3
 Potential Landfill Gas Generation and Capture Summary Table

PRD MSWF

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4. TECHNICAL VIABILITY OF LANDFILL GAS EXTRACTION

LFG extraction is routinely performed at active and closed landfills and can benefit the environment by reducing hazardous air pollutants, greenhouse gas emissions, LFG subsurface migration, and odors. When cells are capped and closed properly, up to 90% of the total LFG generated can be captured and utilized, with the remainder of the gas escaping into the atmosphere or subsurface. Capping allows for the LFG wells to sustain increased vacuum with less potential for air intrusion through the cap into the waste. In addition, landfill capping impacts the time horizon of LFG generation, due to the reduction of moisture infiltration into the waste mass.

LFG collection can be performed once enough waste is placed to install a collection system that will not draw air into the waste. LFG can be collected by either a passive or an active collection system, configured as vertical wells, horizontal trenches, or a combination. The efficiency of the LFG collection depends on a number of factors including, but not limited to, the thickness of waste in the area of the LFG extraction well, distribution of wells within the landfill, and type of cover over the area where gas extraction is taking place.

4.1 LANDFILL GAS COLLECTION SYSTEMS

4.1.1 Passive Gas Collection Systems

Passive gas collection systems (Figure 4-1) use existing variations in landfill pressure and gas concentrations to vent LFG into the atmosphere or to a control system. The system can be installed during active operation of a landfill or after closure. The purpose of a passive gas collection system is to prevent the buildup of gas pressure within the landfill, to maintain the stability of the landfill cover, and to prevent the offsite migration of LFG (U.S. Army Corps of Engineers 2008). Passive gas collection systems are typically used when the landfill is not required to have an active LFG collection system (below Tier II category), the landfill is old and/or small, and the LFG production is small.

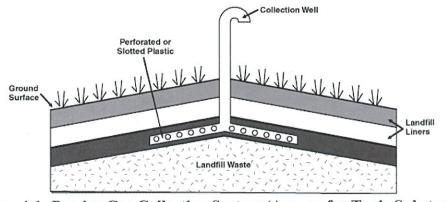


Figure 4-1 Passive Gas Collection System (Agency for Toxic Substances and Disease Registry 2001) Rules of thumb are commonly applied in the design of passive gas collection systems instead of strict design procedures. The passive vents or extraction wells are typically constructed of perforated or slotted plastic and are installed a minimum of 5 to 10 ft into the waste. Passive collection systems can be utilized for LFG reuse projects; however, collection efficiencies may be very low, especially for vents installed with small perforated lengths.

4.1.2 Active Gas Collection Systems

Active LFG systems function by applying a vacuum to a network of extraction wells and/or trenches located within the waste to extract LFG. Active extraction systems may include the following primary components:

- Extraction wells with well heads for monitoring and control
- Collection system piping, including laterals and header piping
- Condensate drains, sumps, pumps, and tanks
- Blower-flare facility with enclosed flares, blowers (primary and potentially standby), and condensate knockout and/or other gas conditioning equipment.

Figure 4-2 illustrates the design of a typical vertical LFG extraction well, including wellheads with valves to regulate gas flow, and to serve as a sampling port.

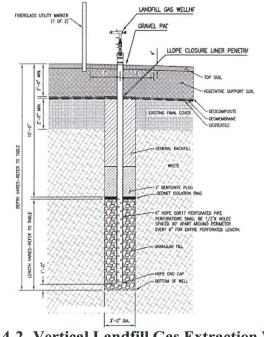


Figure 4-2 Vertical Landfill Gas Extraction Well Detail

Eloy S. Inos Peace Park (formerly Puerto Rico Dump) Landfill Gas Extraction Feasibility Study and Marpi Solid Waste Facility, Commonwealth of the Northern Mariana Islands

Depending on the potential health and environmental risks and local regulatory criteria, LFG can either be directly discharged to the atmosphere or collected for flaring or reuse. The energy potential from LFG generation is dependent on the quality of the LFG (i.e., methane content). It is common for landfills to flare gas due to odor concerns, even if the landfill is not required to collect gas based on regulations.

4.1.3 Landfill Gas Collection System Piping

Collection piping layout may include a looped collection header, allowing connection via laterals to extraction wells, while also providing the advantage of self-equalizing or balancing of the vacuum and flow. LFG collection system piping can be placed on the landfill surface, buried, or a combination. If buried, collection piping material and design should consider achieving minimum slopes to facilitate gas flow and consider potential for landfill settling. If aboveground collection system piping is utilized, it can impact site drainage and is not protected from cold weather conditions.

A wellhead is typically used to connect the vertical extraction well to the below-grade collection system. The wellhead provides for flow adjustment, gas monitoring, flow measurement, and leachate extraction, if needed. The placement of the existing extraction wells typically ranges from every 200 to 500 ft in triangular orientation. Vertical gas collection wells are typically extended from the surface to within 10 ft above the liner system to minimize the potential to damage the liner system or leachate collection system during well installation. Typically, the upper 20 ft of the vertical well is constructed of solid pipe casing to prevent non-LFG intrusion into the system.

4.1.4 Landfill Gas Condensate Collection

As LFG is extracted from the landfill and transported through the LFG collection system, it gradually cools and a liquid (condensate) is formed. The LFG condensate is primarily comprised of water and typically contains minimal quantities of volatile and miscible compounds and can have similar composition to leachate. Typically, the layout of the LFG piping is designed to maintain positive drainage to condensate drains in low-lying areas. Where possible, the pipe network is designed so the condensate runs with the flow of the LFG to minimize pipe surging.

4.1.5 Blower-Flare Facility

A blower applies the required vacuum on the LFG collection system and supplies the required discharge pressure for the flare. The amount of vacuum required depends on the size of the LFG collection system and typically varies from 40 to 60 in. of water column. The flare station for combustion of LFG can act as either the backup control device in conjunction with an end use project or as the single control device for the LFG collection system.

4.2 LANDFILL GAS MONITORING

LFG monitoring probes can be used in conjunction with either active or passive systems to ensure LFG migration offsite can be detected. The regulatory compliance point is the property boundary, with maximum acceptable concentration of methane in the probes typically limited to 0.5–5% by volume. Federal regulations require that LFG concentrations not exceed the lower explosive limit for methane (i.e., 5% methane by volume) at the property boundary or 25% of the lower explosive limit for methane (i.e., 1.25% methane by volume) in facility structures. Increased monitoring and/or modifications to the operating procedures of the LFG collection system are required if methane concentrations exceed acceptable levels.

4.3 OPERATOR TRAINING

LFG collection and control system operations require a certain level of expertise. As such, LFG system operators must have adequate training to properly operate and maintain the system. Some local regulatory agencies recommend a Best Management Practice LFG course including classroom training and field training, often supplemented by annual refresher training and specialty training classes offered by equipment vendors for typical LFG equipment and controls, such as well heads, flares, blowers, flow meters, gas analyzers, and data recorders.

5. TECHNIQUES TO INCREASE LANDFILL GAS PRODUCTION

Due to the organic nature of most of the waste in an MSW landfill, the decay and stabilization of waste largely depends on biological action. The rate of the biological action directly affects the LFG generation rate; degrading waste more quickly increases LFG generation. By providing appropriate and controlled means of introducing leachate into a landfill cell, along with adequate means of measuring and monitoring system operations, leachate recirculation can increase LFG generation while providing a variety of additional benefits to landfill operations, including reducing the volume of leachate for treatment, and maximizing the capacity of the permitted airspace for waste disposal.

Leachate may be applied to landfills via surface application, or horizontal or vertical piping installed within the waste mass. An example of a leachate application system EA designed for another landfill site is shown in Figure 5-1, in which a leachate recharge well was coupled with a LFG extraction well, for leachate application and LFG extraction.



Figure 5-1 Leachate Recharge

5.1 LEACHATE RECIRCULATION DESIGN CONSIDERATIONS

While landfill leachate recirculation can be designed so a system is relatively easy to operate and does not require significant infrastructure, minimum requirements must be met. Typical leachate recirculation design considerations include:

- Leachate recirculation can only occur over a liner and leachate collection system that includes a composite liner system incorporating a geomembrane. Approval of alternate liner systems may be pursued with local regulators.
- EPA regulations require all Subtitle D landfills to maintain less than 12 in. of head on the liner system, with notification to state and or federal regulators within 24 hours if this is exceeded. Typically, leachate head on liner is monitored daily or continuously and reported as a weekly average. As an alternative, some local jurisdictions may allow

demonstrated compliance with a leachate head on liner system by using a water balance method.

- Measurement systems may be required to measure leachate head, flow rate, recirculation flow into the landfill, and leachate collected from the landfill.
- Only leachate and LFG condensate generated from the landfill may be recirculated.
- Leachate may be distributed throughout the waste mass as much as practical.
- Due to the potential for leachate seeps, distribution systems should not be installed within 50 linear ft of exterior side slopes.
- Due to higher moisture content as a result of recirculation, slope stability should be determined on the liner, intermediate waste, and cover interfaces with the design providing for a factor of safety greater than 1.5 for saturated conditions.

5.2 LANDFILL GAS GENERATION WITH LEACHATE RECIRCULATION AT PRD

For the purposes of this analysis, EA has assumed leachate recirculation is not a feasible option at PRD because it is not currently operational and has already been capped; therefore, only minimal leachate will be generated.

5.3 LANDFILL GAS GENERATION WITH LEACHATE RECIRCULATION AT MARPI SOLID WASTE FACILITY

The goal of a leachate recirculation system at the MSWF would be to increase LFG generation over a shorter operational period to improve the efficiency of a LFG collection system. Depending on the ultimate use of the LFG, it may be advantageous to produce more gas over a shorter time period, rather than less gas over a longer time period.

Utilizing the LandGEM model with previous input, and modified to account for recirculation, a year-by-year estimate of LFG emissions with leachate recirculation was developed. The model results show that leachate recirculation does reduce the time horizon over which LFG is generated. Figure 5-2 illustrates that additional moisture will increase the rate of generation of methane; the peak methane generation will begin sooner and remain steady from the years 2021 to 2049. LandGEM estimated methane generation will decrease substantially after a year. The tabulated model output showing estimated gas generation with leachate recirculation for each year is provided in Appendix E.

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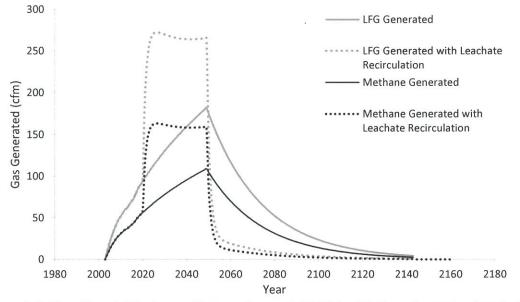


Figure 5-2 Predicted Methane Generation at MSWF with Leachate Recirculation

While landfill leachate recirculation can be designed so a system is relatively easy to operate and does not require significant infrastructure, leachate recirculation can be difficult to permit for landfills with single-liner systems like MSWF. Negotiations would be required with CNMI Bureau of Environmental and Coastal Quality (BECQ) to allow MSWF to begin recirculating leachate without installing a liner system that meets EPA requirements.

For the purposes of this analysis, EA has assumed leachate recirculation is not a feasible option at MSWF. The Department of Public Works could initiate conversations with BECQ to determine if leachate recirculation could be performed with the current liner system at MSWF. EA has initiated discussion with BECQ regarding the potential; however, no definitive guidance has been provided. This page intentionally left blank

6. CONCEPTUAL LANDFILL GAS COLLECTION SYSTEM DESIGN

6.1 LANDFILL GAS EXTRACTION FROM PUERTO RICO DUMP

6.1.1 Landfill Gas Collection Feasibility

Since beneficial reuse of LFG is directly dependent upon the quantity and quality of methane produced by a landfill, and the fact that PRD peak LFG production has already occurred (2004), the potential for beneficial use of methane collection from PRD may not be economical. However, since passive vents were installed at the site as part of the PRD closure, EA has investigated the feasibility of LFG collection at PRD via these existing vents.

For the basis of design, the LFG production in 2025, 35 cfm (Table 3-3), was utilized for conceptual component layout.

6.1.2 Landfill Gas Collection System Conceptual Design

Currently, the Eloy S. Inos Peace Park has a total of five LFG monitoring probes and 23 passive vents at the top deck and along the perimeter bench (GHD 2017). Since the Eloy S. Inos Peace Park is not required to have an active LFG collection, and to minimize disruption to the existing landfill cap, no additional LFG wells were considered. However, the spacing of existing LFG vents is expected to be sufficient for LFG capture, based on the LandGEM sampling and model results.

In order to collect LFG from existing passive vents, passive vents can be converted to an active system. This may include removing existing vent heads, and other associated piping, extending gas well standpipes, and installing blowers and/or energy generating equipment (if applicable). However, the existing vents may require further investigation before performing any modifications. Figure 6-1 shows the modifications that may be performed to convert from passive vents to an active collection system.

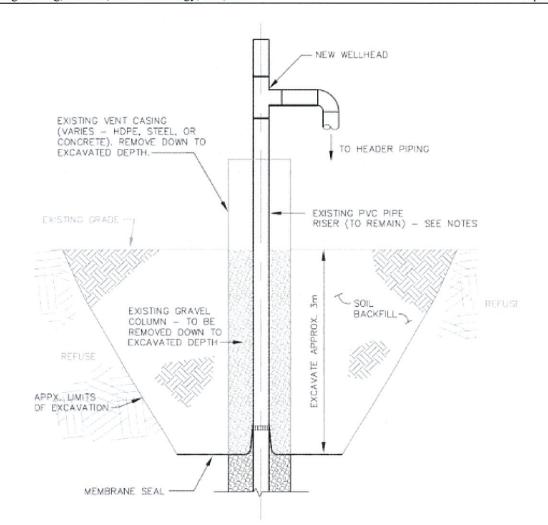


Figure 6-1 Typical LFG Vent Modification (Conestoga-Rovers & Associates 2004).

Collection piping layout includes a looped collection header designed to maintain positive drainage to two condensate drains placed at low points in the collection header. Collection piping would consist of a buried system placed above the closure cap drainage layer and below the final cap. This approach may cause maintenance requiring cap excavation and repair for LFG system installation after cap installation. Based on projected LFG flow rates from LandGEM and EA's experience with LFG collection system design, pipe size for the collection header pipe of 6-in. diameter and a lateral pipe of 4-in. diameter were assumed. A wellhead would be used to connect the extraction well to the below-grade collection system. Wellhead selection can provide for flow adjustment, gas monitoring, flow measurement, and leachate extraction, if needed. A proposed layout for LFG header pipe connecting all existing gas vents is shown in Appendix F.

6.2 LANDFILL GAS EXTRACTION FROM MARPI SOLID WASTE FACILITY

6.2.1 Landfill Gas Collection Feasibility

While a LFG collection system is not required based on landfill size and emissions, an active LFG management system is considered feasible for MSWF based on estimated LFG production. For the basis of design, peak LFG production of 182 cfm (Table 3-3) was utilized for conceptual component layout and sizing.

6.2.2 Landfill Gas Collection System Conceptual Design

As Cell 1 has already been filled and Cells 2–6 will be designed and filled subsequently, the most appropriate LFG extraction well will be a vertical well with a flow control valve that will be connected to a common collection system header. Well spacing was determined based on a calculated radius of influence and considering the LFG extraction capacity with the cost of the system; a spacing of approximately 260 ft was chosen. Based on the calculated spacing requirement, a total of 24 new extraction wells are required. Extraction well spacing calculations are provided in Appendix G.

A proposed LFG extraction well and collection header are shown on Figure 1 in Appendix G. Extraction wells were placed based on aforementioned separation, and to maintain a radius of influence separation distance from the edge of liner to prevent drawing oxygen into the system. Collection piping layout includes a looped collection header designed to maintain positive drainage to two condensate drains placed at low points in the collection header. Collection piping would consist of a buried system placed above the closure cap drainage layer, placed prior to final cap installation. This approach would prevent maintenance requiring cap excavation and repair for LFG system installation after cap installation. Based on projected LFG flow rates from LandGEM, a collection header pipe of 6-in. diameter and a lateral pipe of 4-in. diameter were assumed.

Based on analysis of liner grades and proposed cap closure grades, EA evaluated the proposed extraction well depth. Vertical wells are typically designed to terminate no less than 10 ft above the liner system, with the upper 20 ft of the well to be constructed of solid pipe casing to prevent non-LFG intrusion into the system. The bottom portion of the wells will be placed in the waste and is perforated to provide a preferential pathway. A wellhead would be used to connect the extraction well to the below-grade collection system. Wellhead selection can provide for flow adjustment, gas monitoring, flow measurement, and leachate extraction, if needed.

In addition, the proposed site figure includes an approximately 100-ft × 100-ft area for location of a blower facility. This area would allow adequate spacing for LFG system appurtenances, which may include flares, blowers, backup generators, condensate knockout tank, and gas-to-energy and/or leachate evaporation system.

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7. POTENTIAL BENEFICIAL REUSE

Beneficial reuse options for LFG generally fall into three broad categories: direct-use, electric power generation, and upgrade to pipeline quality gas (Figure 7-1). Direct use options are most attractive when potential users are in fairly close proximity to the landfill and able to employ the gas directly with minimal gas pretreatment. Electric power generation is generally most attractive when power can be sold to a local utility at a favorable rate or when a potential user who would like to displace power purchased from a utility is close to the landfill. Options that require upgrading the gas to pipeline quality are usually favored by situations where larger volumes of LFG are available, and the upgraded gas can compete favorably on the open market with natural gas or other fossil fuels.

Before LFG can be used in an energy conversion process, it may require treatment to remove condensate, particulates, and other impurities (EPA 2017b), depending on the end use. As an example, treatment systems may include a series of filters to remove contaminants that could damage engines and turbines, thereby reducing system efficiency. Advanced treatment is required to produce high-Btu (British thermal unit) gas for injection into natural gas pipelines or production of alternative fuels, including primary processing systems such as de-watering and filtration, and secondary treatment processing such as physical and chemical treatments necessary to remove specific constituents, such as siloxanes and sulfur compounds, depending on the end use.

Each option is discussed in detail in this chapter, with site-specific application of beneficial reuse presented in Chapter 8.

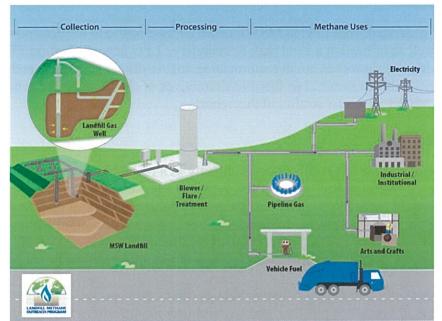


Figure 7-1 Example Landfill Gas End Use Options (EPA 2017b)

7.1 ELECTRIC POWER GENERATION

Currently, the most common beneficial use for LFG is as fuel for power generation. The fuel energy-to-electric power conversion efficiencies of various technologies range from less than 30% for simple-cycle combustion turbines to nearly 50% for fuel cells. Essential elements include gas compression, gas cleanup, a pipeline, the power generation system, and an interconnection with either the onsite user of the power or an electric utility. Primary factors determining optimal generation includes landfill size, variability in LFG flows, energy conversion efficiency of the various electric power generation options, and beneficial end uses. LFG can be used as a fuel energy source in several methods including:

- Firing the gas in a high-pressure boiler connected to a:
 - Reciprocating internal combustion engine driven generator
 - Microturbine driven generator
 - Steam turbine driven generator
 - Combustion turbine driven generator (simple or combined-cycle)
- Direct chemical-to-electric energy conversion in a fuel cell

Both reciprocating engine-driven generators and microturbine-driven generators are well proven in LFG service and are available in various module sizes. Fuel cells create electricity by combining hydrogen (taken from the LFG's methane) and oxygen in an electrochemical reaction. While fuel cells are more efficient, have ultra-low emissions, and are very quiet, extensive gas pretreatment is required to remove the carbon dioxide and impurities from LFG.

Electric power generated from LFG at MSWF could be used onsite to displace power currently purchased, as well as utilized at a local park or cemetery. LFG generation form PRD is much lower than the MSWF; however, small reciprocating engine-driven generators and microturbine-driven generators will be examined as feasible alternatives of electrical power generation from both PRD and MSWF in a later section of this report.

7.2 DIRECT USE

Direct use alternatives for LFG utilize the gas directly as a fuel without significant processing. LFG is considered "medium Btu" gas and generally has a heating value in the range of 400 to 600 Btu per standard cubic ft—roughly half the energy density of natural gas. Many well-established energy conversion technologies capable of operating on natural gas or other fossil fuel can be modified to use LFG as a fuel. Relatively limited filtration and drying are needed prior to direct-use as fuel; however, end-use equipment modification may be necessary.

Essential elements of a direct-use system include gas collection, gas pre-treatment (compressor station, gas cleanup system), a pipeline, and any end-user modifications necessary to fire LFG instead of a fossil fuel. Potential direct use options for LFG include:

- Hot water and steam boilers
- Stationary internal combustion engines and combustion turbines operating as prime movers
- Fired process heaters and dryers
- Industrial furnaces and kilns
- Leachate evaporators (Figure 7-2)
- Greenhouse heat, power, and carbon dioxide enhancement.



Figure 7-2 Leachate Evaporator (EPA 2017b)

Although direct use of LFG is often the least complex and least expensive beneficial use option to implement, it depends on favorable circumstances to be a viable option. These circumstances include the proximity of an end user that can readily substitute LFG for other fuels and derive an economic benefit. Based on current leachate management practices at MSWF, direct use of LFG for operation of a leachate evaporator will be examined as a feasible option in in a later section of this report.

7.3 UPGRADE TO PIPELINE QUALITY

Processing and treatment of LFG can be used to produce a gas roughly equivalent in content and quality to natural gas. This process requires separation of the carbon dioxide, which constitutes roughly half of LFG by volume. In order to meet the "pipeline standards," treatment to remove moisture, hydrogen sulfide, and NMOCs from LFG are often necessary. This processing yields a

gas that is essentially pure methane, increasing the heating value to roughly 1,000 Btu per standard cubic foot. Once the quality specifications of the end-user are met, the pipeline quality LFG is suited for any application for which natural gas is suited, including:

- Direct feed into a natural gas distribution or transmission pipeline system
- Compression or liquefaction for use as vehicle fuels (compressed natural gas or liquefied natural gas)
- Substitution for natural gas as a chemical feedstock.

Due to the significant requirements for compression; gas cleanup; and pretreatment for hydrogen sulfide, NMOC, and moisture, and the complexity of the various carbon dioxide separation technologies, upgrading LFG to pipeline quality is typically not a cost-effective option for low volumes. For LFG flow rates below 2,800 to 3,000 cfm, upgrade of LFG to pipeline quality gas is considered economically infeasible. In addition, due to a limited natural gas distribution network, absence of potential beneficial end users, and smaller volume of LFG generation from both PRD and MSWF, upgrading the LFG to pipeline quality is not considered a feasible option.

8. ENERGY RECOVERY SYSTEM AND ECONOMIC VIABILITY EVALUATION

Implementation of a LFG collection system and energy production system is greatly dependent on the quality and quantity of LFG produced. Additionally, it is important to note that the greatest variable for LFG production is the waste acceptance rate of a landfill. Since PRD stopped operation in 2002, the peak LFG generation year has already passed, and current LFG generation is very low, both energy production alternatives may appear economically nonprofitable if implemented in 2025 (Figure 3-2). On the other hand, MSWF is still in operation and will expand in the future with a potential of producing higher amounts of LFG (Figure 3-3). If future waste receipts are not as predicted and modeled in the LandGEM model (i.e., additional waste is accepted at the MSWF), the LFG generation model and the feasibility of the LFG extraction for beneficial use projects can be greatly affected. For example, a significant increase in the quantity of waste disposed could accelerate the feasibility of a LFG to electricity project. The maximum benefit of a LFG collection system will correspond with peak LFG production.

Although PRD has already passed the peak generation period and is currently producing very limited quantities of LFG (Figure 3-2), two energy recovery systems will be considered for further evaluation of beneficial reuse feasibility. For MSWF, after considering the various beneficial uses, end user proximity, gas pretreatment requirements, and energy conversion efficiency for LFG, three alternative options will be evaluated. Alternatives investigated are summarized in Table 8-1 below and discussed in detail in this section.

Alternatives	Description	PRD	MSWF
Option 1	Electric Power Generation Using Small Reciprocating Engine	PRD Option 1	MSWF Option 1
Option 2	Electric Power Generation Using Microturbine Generator	PRD Option 2	MSWF Option 2
Option 3	Direct Use for Leachate Evaporation	-	MSWF Option 3

Table 8-1Alternatives Matrix

For the active LFG collection system and beneficial reuse alternatives discussed within this section, the EPA LFG energy cost model (EPA 2017a) was utilized for cost comparison, with detailed assumptions documented in Appendix H. Detailed feasibility studies apply project-specific costs, such as cost quotes for a specific model of equipment appropriate to the landfill, right-of-way costs for anticipated pipeline routes and current land owners, state-specific permitting requirements, and interest rates. The EPA model was developed for cost assessment of projects on the mainland of the United States; therefore, a factor of 40% was applied to all costs estimated at PRD and MSWF to account for the increased cost of specialized work in a remote location and contingency to address unknown issues that may arise during project development. A detailed economic feasibility analysis including annual and operation and maintenance (O&M) costs, annual return, and net present value (NPV) calculations for both landfills is provided in Appendix I. A 6% interest rate (based on projected 2025 prime interest rate) and 3% discount rate are utilized to determine annual debt service and NPV, respectively.

8.1 ACTIVE LFG COLLECTION AND ENERGY PRODUCTION ALTERNATIVES AT PRD

The cost estimated for a LFG collection system at PRD is common to the two alternatives presented and is based on the costs for conversion of passive vents to an active collection system, based on a LFG energy collection startup year of 2025. Since 23 passive vents exist at the site, costs associated with drilling and pipe crew mobilization for installation of vertical gas extraction wells are not considered. The detailed header pipe layout connecting all gas vents located at the top deck and bench is shown in Appendix F. The components considered in the cost estimate include:

- Engineering, permitting, and administration
- Site survey, preparation, and utilities
- Wells and wellheads
- Pipe gathering system (includes additional fittings/installation)
- Condensate knockout system
- Blower system
- Instrument control.

The total estimated capital and annual O&M costs for installing a LFG collection system are estimated as \$617,000 and \$59,800, respectively (Table 8-2) and are included in the economic analysis for each of the options presented below. The capital and O&M cost components were estimated based on the EPA LFG energy cost model; the relevant equations are provided in Appendix H.

Table 8-2 Cost Estimation for Conversion to Active LFG Collection System at PRD

Item Description	Cost	
Total Capital Cost	\$617,000	
Annual Operation and Maintenance cost	\$59,800	

To utilize the LFG generated from the PRD in the most effective way, two alternatives for electricity generation were considered—electric power generation using small reciprocating engine and electricity generation using microturbine generator. These alternatives are discussed in detail in Sections 8.1.1 and 8.1.2.

8.1.1 PRD Option 1 – Electric Power Generation Using Small Reciprocating Engine

The most common beneficial use for LFG is as fuel for power generation, with reciprocating engine-driven generators being well proven. However, the quality and quantity of LFG generation from PRD is minimal as described in Section 3.3.1. The initial project year and project-life were assumed to be 2025 and 15 years, respectively.

A rough order of magnitude assessment of capital and O&M costs for this option includes: gas compression and treatment (includes dehydration equipment and filtration); reciprocating engine

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and generator (includes motor controls, switch-gear, radiators, exhaust silencers, and wiring and plumbing); electrical interconnect equipment; and site work, housings, utilities, and total facility engineering, design, and permitting (Table 8-3). The capital cost of electricity generating equipment size was calculated based on the average LFG captured (18 cfm) during the project life (Table 3-3).

Table 8-3	PRD Option 1 – Cost for Electricity Generation Using Small Reciprocating
	Engine

Item Description	2025–2039	
Capital Costs		
Active LFG Collection System (Table 8-2)	\$617,000	
Electricity Generation Using Small Reciprocating Engine	\$133,000	
Annual O&M Costs		
Active LFG Collection System	\$59,800	
Electricity Generation Using Small Reciprocating Engine	\$11,200	
Cost-Benefit Analysis		
Net Present Value	\$(1,513,000)	
Average Electricity Rate (\$/kWh) ^(a) \$0.14		
Annual Return from Beneficial Reuse ^(b) \$21,7		
 (a) Average electricity rate for commercial use was based on <i>Northern Mariana Islands Quick Facts – Northern Mariana Islands Territory Energy Profile</i> (U.S. Energy Information Administration 2018). (b) Assuming consumption of 10 hours of continuous electricity per day from 41 kW capacity PRD energy production system. Future demand may vary. Notes: kW = Kilowatt(s). 		
kWh = Kilowatt-hour(s).		

8.1.2 PRD Option 2 – Electricity Generation Using Microturbine Generator

Microturbine technology is widely used for landfill applications and is often preferred to the internal combustion engine since less LFG volume is required, can use LFG with a lower percent methane (35% methane), produces lower emissions of nitrogen oxides, can add and remove microturbines as gas quantity changes, and interconnection is relatively easy because of the lower generation capacity (EPA 2017b). Installed capital and annual O&M costs were determined utilizing the EPA LFG energy cost model user manual (EPA 2017a) and are summarized in Table 8-4.

Table 8-4 PRD Option 2 – Cost Electricity Generation Using Microturbine Generator

Item Description	2025–2039		
Capital Costs			
Active LFG Collection System (Table 8-2)	\$617,000		
Electricity Generation Using Microturbine Generator	\$271,000		
Annual O&M Costs			
Active LFG Collection System	\$59,800		
Electricity Generation Using Microturbine Generator	\$14,000		
Cost-Benefit Analysis			
Net Present Value	\$(1,715,000)		
Average Electricity Rate (\$/kWh) ^(a) \$0.145			
Annual Cost Savings from Electricity \$21,7			
 (a) Average electricity rate for commercial use was based on <i>Northern Mariana Islands Quick Facts – Northern Mariana Islands Territory Energy Profile</i> (U.S. Energy Information Administration 2018). (b) Assuming consumption of 10 hours of continuous electricity per day from 41 kW capacity PRD energy production system. Future demand may vary. 			
Notes: kW = Kilowatt(s). kWh = Kilowatt-hour(s).			

8.2 ACTIVE LFG COLLECTION SYSTEM AND ENERGY PRODUCTION ALTERNATIVES AT MSWF

The cost estimated for a LFG collection system at MSWF is common to the three alternatives presented and was developed based on LFG energy collection startup year of 2025, landfill closure year 2048, and projected annual tonnage through landfill closure. The detailed LFG collection system layout is shown in Figure 1 of Appendix G. The components considered in the cost estimate include:

- Engineering, permitting, and administration
- Site survey, preparation, and utilities
- Wells and wellheads
- Pipe gathering system (includes additional fittings/installation)
- Condensate knockout system
- Blower system
- Instrument control.

The total estimated capital and annual O&M costs for installing a LFG collection system are estimated as \$1,079,000 and \$62,400, respectively (Table 8-5) and is included in the economic analysis for each of the options presented below. The assumptions and relevant equations for the capital and O&M cost estimations are provided in Appendix H.

Table 8-5	Cost Estimation for Active LFG Collection System at MSWF	
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Item Description	Cost	
Total Capital Cost	\$1,079,000	
Annual O&M cost	\$62,400	

8.2.1 MSWF Option 1 – Electric Power Generation Using Small Reciprocating Engine

Similar to the alternatives discussed earlier for PRD, LFG generated from MSWF has more potential to be utilized for energy production. Since the reciprocating engine-driven generators are well proven as the most common LFG to energy generation method, the cost-benefit analysis will be performed for MSWF and discussed in this section.

Average LFG flow rates for 15-year periods were used as the basis of cost estimates and are meant to capture differences in three phases (2025–2039, 2040–2054, and 2055–2069) of LFG production at MSWF. It is assumed that the project will begin operation in 2025 and, in the beginning of the next two operational periods, an additional 25% capital cost will be incurred due to the replacement of any damaged system components or due to the landfill expansion. A rough order of magnitude cost for capital and O&M costs for electricity generation using a small reciprocating engine was developed using the EPA model and presented in Table 8-6 (EPA 2017a).

 Table 8-6
 MSWF Option 1 – Cost for Electric Power Generation Using Small

 Reciprocating Engine

Item Description	2025-2039	2040-2054	2055-2069
Ca	pital Costs		
Active LFG Collection System (Table 8-5)	\$1,079,000	\$269,800	\$269,800
Electricity Generation Using Small Reciprocating Engine	\$921,000	\$230,300	\$230,300
Annua	al O&M Costs	Service Services	i i i i i i i i i i i i i i i i i i i
Active LFG Collection System	\$62,400	\$62,400	\$62,400
Electricity Generation Using Small Reciprocating Engine	\$77,600	\$95,900	\$62,400
Cost-B	Senefit Analysis		
Net Present Value \$(3,629,100)			
Average Electricity Rate (\$/kWh) ^(a)	\$0.145		
Annual Cost Savings from Electricity	\$153,100		

(a) Average electricity rate for commercial use was based on *Northern Mariana Islands Quick Pacts - Northern Mariana Islands Territory Energy Profile* (U.S. Energy Information Administration 2018).

(c) Average annual electricity (kW) of 290 kW was obtained from average annual electricity generation in three phases, 2025–2039, 2040–2054, and 2055–2069 at MSWF (Table 3-3).

Notes: kW = Kilowatt(s). kWh = Kilowatt-hour(s).

⁽b) Assuming consumption of 10 hours of continuous electricity per day from 290 kW^(c) capacity MSWF energy production system. Future demand may vary.

8.2.2 MSWF Option 2 – Electricity Generation Using Microturbine Generator

As microturbine technology is also widely used for landfill applications, this method is considered for the LFG to energy production at MSWF. Microturbine generator is often preferred to the internal combustion engine as mentioned in Section 8.1.2.

Table 8-7 illustrates a rough order of magnitude cost estimation for capital and O&M costs for electricity generation using a microturbine generator was developed using the EPA model (EPA 2017a). Similar to Option 1, it is assumed that the project will begin operation in 2025 and, in the beginning of the next two operational periods, an additional 25% capital cost will be incurred due to the replacement of any damaged system components or due to the landfill expansion.

Table 8-7 MSWF Option 2 – Cost for Electricity Generation Using Microturbine Generator

Item Description	2025-2039	2040-2054	2055-2069
Ca	pital Costs		_
Active LFG Collection System (Table 8-5)	\$1,079,000	\$269,800	\$269,800
Electricity Generation Using Microturbine Generator	\$903,000	\$225,800	\$225,800
Annuc	al O&M Costs		
Active LFG Collection System	\$62,400	\$62,400	\$62,400
Electricity Generation Using Microturbine Generator	\$51,100	\$57,000	\$45,300
Cost-B	enefit Analysis		
Net Present Value \$(2,897,000)			
Average Electricity Rate (\$/kWh) ^(c) \$0.145			
Annual Cost Savings from Electricity	m Electricity \$153,100		

(a) Average electricity rate for commercial use was based on Northern Mariana Islands Quick Facts - Northern Mariana Islands Territory Energy Profile (U.S. Energy Information Administration 2018).
 (a) Average electricity rate for commercial use was based on Northern Mariana Islands Quick Facts - Northern Mariana Islands - Northern Mariana Islands - Northern Mariana Islands - Northern Mariana Islands - Northern Mariana

(b) Assuming consumption of 10 hours of continuous electricity per day from 290 kW^(c) capacity MSWF energy production system. Future demand may vary.

(c) Average annual electricity (kW) of 290 kW was obtained from average annual electricity generation in three phases, 2025–2039, 2040–2054, and 2055–2069 at MSWF (Table 3-3).

Notes: kW = Kilowatt(s). kWh = Kilowatt-hour(s).

8.2.3 MSWF Option 3 – Direct Use with Leachate Evaporator

Currently, the MSWF manages leachate onsite in a lined holding pond and adjacent leachate reactor beds. Leachate from Cell 1 at the MSWF is currently pumped to an existing 4.9-million-gallon leachate treatment pond via a 15-horsepower pump (190 gallons per minute) operated an estimated 8 hours a week, or approximately 91,200 gallons a week. The amount of leachate collected from MSWF was assumed to be approximately 5 million gallons per year. The leachate generation volume will increase as the new cells come online and additional leachate

treatment capacity may be required. The installation and operation of a leachate evaporator may prevent the need for future construction of additional leachate reactor beds. LFG-fueled evaporation is a technology that effectively integrates the control of LFG and landfill leachate. It can reduce the total volume of leachate to less than 5% of original volume (Purchwitz 1999). Leachate evaporation systems are typically insensitive to changes in leachate characteristics including concentrations of biological oxygen demand, chemical oxygen demand, suspended and dissolved solids, and variations in feed temperature. The only factor to which the evaporative systems are sensitive is pH, and this is due solely to the potential corrosiveness of acidic leachate on alloys used in the evaporators (Purchwitz 1999); therefore, pH adjustment may be required if pH drops below 7.0. An air permit to operate a leachate evaporator and/or a modification to the landfill's solid-waste permit to address leachate-management practices may be required.

A rough order of magnitude cost for capital and O&M for direct use with a leachate evaporation system was developed using the EPA model, and includes the leachate evaporation unit, leachate storage tank, process control instruments and site work, housing, utilities, and total facility engineering, design and permitting.

Table 8-8 presents the LFG collection system and leachate evaporator installation cost estimates for the MSWF. It is assumed that the construction and installation of a LFG collection system and leachate evaporator system will be completed before 2025 and 25% of the capital cost will be incurred in 2040 and 2055 for replacing the damaged system components (if any) or for any additional cost due to landfill expansion. Based on current MSWF leachate operation data, the leachate production rate was assumed to be 10,000 gallons per year. The leachate evaporation rate was assumed to be 95% according to the EPA model (EPA 2017a).

Item Description	2025-2039	2040-2054	2055-2069
Capital and Annual	O&M Costs		
Capital Cost for Active LFG Collection System (Table 8-5)	\$1,079,000	\$269,800	\$269,800
Annual O&M Cost for Active LFG Collection System	\$62,400	\$62,400	\$62,400
Annualized Capital and O&M Costs for Leachate Evaporator	\$146,200	\$36,600	\$36,600
Cost-Benefit Ar	alysis		
Net Present Value		\$(7,397,400)	
Savings from Future Leachate Pond Construction	\$50,000	\$50,000	\$50,000

Table 8-8 Cost for Direct Use with Leachate Evaporator at MSWF (Option 3)

8.3 ECONOMIC VIABILITY

8.3.1 Summary of Findings

A summary table (Table 8-9) is presented below to compare key findings from the economic analysis, including NPV (Appendix I).

Table 8-9 LFG beneficial Keuse Financial Summary			
Landfill – Option	Net Present Value		
PRD – Option 1	\$(1,513,000)		
PRD – Option 2	\$(1,715,000)		
MSWF – Option 1	\$(3,629,100)		
MSWF – Option 2	\$(2,897,000)		
MSWF – Option 3	\$(7,397,400)		

Table 8-9	LFG	Beneficial	Reuse	Financial	Summary
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Based on the values presented in Table 8-9, the estimated NPV values for all energy production options at PRD and MSWF are negative, suggesting projects will not be profitable if implemented.

8.3.2 Incentive Options for LFG Energy Project

Economic factors that may make LFG beneficial reuse attractive to smaller landfills are incentives related to generating electric power from renewable energy sources. Various funding options or incentives that could be available for the energy project are given below and may be available both as tax credits and/or as preferential electric power sales rates.

- Renewable Energy Production Tax Credit
- Renewable Energy Production Incentive
- Renewable Energy Credits
- Greenhouse Gas Emission Credits.

The incentives or funding opportunities may need to be assessed further before implementing any beneficial reuse project at MSWF.

9. CONCLUSIONS AND RECOMMENDATIONS

Based on information available for both the PRD and MSWF sites, EA has estimated LFG production, developed conceptual LFG collection system design, and provided an economic analysis of proposed LFG collection and beneficial reuse projects. Unlike the PRD, which is a closed landfill where LFG production is not expected to increase, variance in waste acceptance rates experienced at MSWF over the life of the facility may significantly affect LFG production, and the success of a beneficial reuse project. Additional discussion for each site is included below.

9.1 LFG BENFICIAL REUSE SUMMARY FOR PRD

- Based on facility size and emissions, installation of a LFG emissions collection and control system is not required by federal regulations.
- The LandGEM model results show that peak LFG production is estimated to have occurred in 2004 (Section 3.3.2).
- For a LFG collection project initiated in 2025 as investigated in this analysis, LFG produced and collected would be very low (Figure 3-2). However, LFG collected at PRD could be utilized to power a small reciprocating engine or microturbine. The energy projects may replace the existing power source currently in operation for electricity supply to the Eloy S. Inos Peace Park office building and other onsite facilities.
- The economic analysis shows that the NPV is negative for both energy project options (Table 8-9).
- Based on these findings, installation of an active LFG collection system and operation of a beneficial reuse project is not currently economically viable at PRD. Additional considerations for project implementation are presented in Section 9.3.

9.2 LFG BENFICIAL REUSE SUMMARY FOR MSWF

- Based on facility size and emissions, installation of a LFG emissions collection and control system is not required by federal regulations.
- The LandGEM model results shows that peak LFG production is estimated to occur in 2049 (Figure 3-3), during the proposed project life.
- For a LFG collection project initiated in 2025 as investigated in this analysis, LFG produced and collected at MSWF could be utilized to power a small reciprocating engine or microturbine or leachate evaporator. The energy projects may replace the existing generator currently in operation for electricity supply to the office building, scale house, maintenance building, generator house, and pumps.

- Electric power generated from LFG at MSWF could also be used onsite to replace purchased electricity at local park or cemetery.
- The economic analysis shows that the NPV is negative for both energy project options and the leachate evaporator option (Table 8-9).
- Based on these findings, installation of a LFG collection system and operation of a beneficial reuse project is not currently economically viable at MSWF. Additional considerations for project implementation are presented in Section 9.3.

9.3 OTHER CONSIDERATIONS

If CNMI desires to pursue any options investigated herein, additional evaluation, detailed cost estimation, engineering design, and permitting would be required. Moreover, the availability of grant funding may enable project implementation.

In addition to the findings presented in this report, additional considerations may affect the approach of developing LFG collection systems and beneficial reuse projects at PRD and MSWF. The implementation of either an active LFG collection system or beneficial reuse systems depend on many factors, such as available project funding, local resources, public acceptance, and project efficiency. In addition, constructability and equipment mobilization to the remote island should be considered in planning for on-island construction. Moreover, while the economic analysis has considered system costs and NPV, CNMI may also consider local sustainability efforts and carbon footprint considerations when recommending a project proceed.

While the leachate evaporator option was not found to be economically viable at MSWF, the leachate evaporator system may be a good alternative to deal with future leachate volume as additional leachate pond construction will be required as new MSWF cells begin operation.

Upon project implementation, active LFG collection system installation and maintenance, and beneficial reuse system installation and maintenance may require additional training and development of local resources to provide expertise necessary for LFG systems.

EA Engineering, Science, and Technology, Inc., PBC

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Appendix A

Marpi Solid Waste Facility Tonnage Data

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DPW/SWMD Waste Delivery Period: February 1, 2003 through January 31, 2004

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. 1	Total Disposal %	% of Disposal	Include in the Model
Auminum	35.00	0.07%	7.22	0.02%	7.22	0.07%	00.00	%00.0	z
Animal	4.00	0.01%	2.12	0.00%	0.00	%00.0	2.12	0.01%	×
Backfill	69.00	0.14%	680.17	1.53%	680.17	6.24%	00.0	%00.0	z
Battery	2.00	0.00%	1.43	0.00%	1.43	0.01%	00'0	%00.0	z
C&D	1,048.00	2.10%	793.89	1.78%	358.00	3.29%	435.89	1.29%	z
Cardboard	1,839.00	3.69%	1,121.28	2.51%	1,121.28	10.29%	00.0	0.00%	7
Garment Waste	3,576.00	7.17%	7,051.61	15.82%	6,983.78	64.11%	67.83	0.20%	Z
Glass	238.00	0.48%	46.92	0.11%	46.92	0.43%	00.0	%00.0	z
Gov. C&D	5.00	0.01%	16.65	0.04%	0.00	%00.0	16.65	0.05%	z
Gov. Free-loads	4,124.00	8.27%	2,116.62	4.75%	0.00	%00.0	2,116.62	6.28%	Z
Gov. Greenwaste ^(a)	299.00	0.60%	283.68	0.64%	283.68	2.60%	0.00	%00.0	×
Gov. Special Waste (b)	14.00	0.03%	129.54	0.29%	0.00	%00.0	129.54	0.38%	z
Gov. White Goods	18.00	0.04%	17.12	0.04%	17.12	0.16%	0.00	0.00%	z
Greenwaste Clean	3,008.00	6.03%	1,175.91	2.64%	1,175.91	10.79%	00.0	0.00%	7
Greenwaste Mixed	81.00	0.16%	72.42	0.16%	0.00	%00.0	72.42	0.21%	7
Metal	104.00	0.21%	39.89	%60.0	39.89	0.37%	00.0	%00.0	z
MSW	17,924.00	35.95%	25,251.89	56.63%	0.00	%00.0	25,251.89	74.95%	7
Mixed Recycling	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	z
Garments Not for Recycle	519.00	1.04%	3,129.63	7.02%	0.00	%00.0	3,129.63	9.29%	z
Plastic Bottles	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	z
Newspaper	5.00	0.01%	5.15	0.01%	5.15	0.05%	0.00	0.00%	7
Office Paper	88.00	0.18%	22.72	0.05%	22.72	0.21%	0.00	0.00%	×
Recycle Garments	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	z
Rejected Garments	23.00	0.05%	32.97	0.07%	0.00	%00'0	32.97	0.10%	z
Resi. Batteries	16.00	0.03%	1.99	0.00%	1.99	0.02%	0.00	0.00%	z
Resi. Charged	577.00	1.16%	143.78	0.32%	0.00	%00.0	143.78	0.43%	۲
Resi. Free ^(c)	15,009.00	30.11%	1,737.46	3.90%	0.00	%00.0	1,737.46	5.16%	z
Resi. Metal	46.00	%60'0	8.18	0.02%	8.18	0.08%	0.00	%00.0	z
Resi. White Goods	17.00	0.03%	3.64	0.01%	3.64	0.03%	0.00	%00.0	z
Special Waste	698.00	1.40%	557.04	1.25%	0.00	0.00%	557.04	1.65%	z
Tip Floor MSW	0.00	%00.0	00.00	0.00%	0.00	%00.0	00.0	0.00%	۲
Tip Floor Waste	0.00	%00.0	0.00	0.00%	0.00	%000.0	0.00	0.00%	۲
Tires	434.00	0.87%	127.84	0.29%	127.84	1.17%	00.00	0.00%	z
White Goods	32.00	%90.0	8.63	0.02%	8.63	0.08%	0.00	%00.0	z
Total	49,852.00	100.00%	44,587.39	100.00%	10,893.55	100.00%	33,693.84	100.00%	83.91%
					Recycling Percentage	24.43%			
Monthly Average	4,154.33		3,715.62		907.80		2,807.82		
Daily Average	161.86		144.76		35.37		109.40		
(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kritchen wastes.	d of organic waste t	hat can be compos	ted, i.e. refuse from	1 gardens, grass c	lippings or leaves, and dom	estic or indu	strial kitchen waste	S.	
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.	ed of industrial proc	ess waste, pollutior	1 control waste, or t	oxic waste, which	may pose a threat to humar	health or th	e environment.	i	
(c) Waste that were not propoerly cat	oerły categorized.								

DPW/SWMD Waste Delivery Period: February 1, 2004 through January 31, 2005

	Total Vehicles	% of Vehicles	Total Delivered %	% of total Waste	Diverted for Recycling	% of Rec. T	Total Disposal %	% of Disposal	Include in the Model
Aluminum	191.00	0.35%	24.46	0.06%	24.46	0.22%	0.00	0.00%	z
Animal	0.00	0.00%	00.0	%00'0	0.00	%00.0	00.00	%00.0	Y
Backfill	264.00	0.49%	2,489.60	5.65%	2,489.60	22.52%	00.00	%00.0	z
Battery	3.00	0.01%	0.53	%00.0	0.53	0.00%	00.00	%00'0	z
C&D	858.00	1.58%	761.08	1.73%	222.25	2.01%	538.83	1.63%	z
Cardboard	1,577.00	2.90%	964.38	2.19%	964.38	8.72%	00.0	%00.0	Y
Garment Waste	1,098.00	2.02%	2,289.76	5.20%	2,201.50	19.92%	88.26	0.27%	z
Glass	464.00	0.85%	80.04	0.18%	80.04	0.72%	00.00	0.00%	z
Gov. C&D	67.00	0.12%	79.95	0.18%	0.00	%00.0	79.95	0.24%	z
Gov. Free-loads	3,858.00	7.09%	2,208.68	5.02%	0.00	%00.0	2,208.68	6.70%	z
Gov. Greenwaste ^(a)	1,432.00	2.63%	1,497.19	3.40%	1,497.19	13.54%	00.00	0.00%	٢
Gov. Special Waste ^(b)	5.00	0.01%	50.48	0.11%	50.48	0.46%	00.00	%00.0	z
Gov. White Goods	111.00	0.20%	62.16	0.14%	62.16	0.56%	00.00	0.00%	z
Greenwaste Clean	6,084.00	11.18%	2,977.68	6.76%	2,977.68	26.94%	00.00	%00.0	Y
Greenwaste Mixed	59.00	0.11%	50.26	0.11%	0.00	%00.0	50.26	0.15%	¥
Metal	303.00	0.56%	121.67	0.28%	121.67	1.10%	00.00	0.00%	z
MSW	15,994.00	29.39%	24,765.87	56.24%	0.00	0.00%	24,765.87	75.08%	٢
Mixed Recycling	0.00	%00.0	0.00	%00.0	0.00	%00.0	00.00	0.00%	z
Garments Not for Recycle	521.00	0.96%	2,355.66	5.35%	0.00	0.00%	2,355.66	7.14%	z
Plastic Bottles	0.00	%00.0	0.00	%00.0	0.00	0.00%	00.0	0.00%	z
Newspaper	19.00	0.03%	1.62	%00.0	1.62	0.01%	00.00	0.00%	٢
Office Paper	276.00	0.51%	112.81	0.26%	112.81	1.02%	00.0	0.00%	Y
Recycle Garments	0.00	%00.0	0.00	%00.0	0.00	%00.0	00.00	0.00%	z
Rejected Garments	2.00	%00'0	3.72	0.01%	0.00	%00.0	3.72	0.01%	z
Resi. Batteries	25.00	0.05%	1.88	%00.0	1.88	0.02%	00.0	0.00%	z
Resi. Charged	676.00	1.24%	113.07	0.26%	0.00	%00.0	113.07	0.34%	٢
Resi. Free ^(c)	19,196.00	35.28%	2,206.68	5.01%	0.00	%00.0	2,206.68	6.69%	z
Resi. Metal	351.00	0.65%	61.15	0.14%	61.15	0.55%	00.00	0.00%	z
Resi. White Goods	82.00	0.15%	13.20	0.03%	13.20	0.12%	00.00	%00.0	z
Special Waste	408.00	0.75%	574.99	1.31%	0.00	%00'0	574.99	1.74%	z
Tip Floor MSW	0.00	%00.0	0.00	%00'0	0.00	%00'0	00.00	0.00%	٢
Tip Floor Waste	0.00	%00'0	0.00	0.00%	0.00	%00.0	00.00	%00.0	۲
Tires	415.00	0.76%	150.32	0.34%	150.32	1.36%	00.00	0.00%	z
White Goods	73.00	0.13%	21.00	0.05%	21.00	0.19%	00.00	0.00%	z
Total	54,412.00	100.00%	44,039.89	100.00%	11,053.92	100.00%	32,985.97	100.00%	85.81%
					Percentage Recycled	25.10%			83.91%
Monthly Average	4.534.33		3.669.99		921.16		2.748.83		
	00 01.7								

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not proposely categorized. 2,748.83 107.10 921.16 35.89 142.99 4,534.33 176.66 Daily Average

DPW/SWMD Waste Delivery Period: February 1, 2005 through January 31, 2006

L	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec.	% of Rec. Total Disposal % of Disposal	of Disposal	Include in the Model
Auminum	146.00	0.29%	10.60	0.02%	10.60	0.07%	00.00	0.00%	z
Animal	1.00	%00.0	0.02	0.00%	0.00	%00'0	0.02	0.00%	×
Backfill	584.00	1.18%	6,822.46	14.69%	6,822.46	43.84%	00.00	0.00%	z
Battery	4.00	0.01%	1.13	0.00%	1.13	0.01%	00.00	0.00%	z
C&D	858.00	1.73%	1,118.23	2.41%	00.00	%00.0	1,118.23	3.62%	z
Cardboard	2,138.00	4.30%	1,140.16	2.46%	1,140.16	7.33%	00.00	0.00%	×
Garment Waste	897.00	1.81%	2,022.18	4.35%	2,022.18	12.99%	00.00	0.00%	z
Glass	235.00	0.47%	64.66	0.14%	64.66	0.42%	00.00	0.00%	z
Gov. C&D	51.00	0.10%	15.31	0.03%	0.00	%00.0	15.31	0.05%	z
Gov. Free-loads	4,520.00	9.10%	1,852.41	3.99%	00.00	%00.0	1,852.41	6.00%	z
Gov. Greenwaste ^(a)	662.00	1.33%	507.33	1.09%	507.33	3.26%	00.00	0.00%	×
Gov. Special Waste ^(b)	228.00	0.46%	1,866.14	4.02%	1,866.14	11.99%	0.00	0.00%	z
Gov. White Goods	6.00	0.01%	2.38	0.01%	2.38	0.02%	00.00	0.00%	z
Greenwaste Clean	4,740.00	9.54%	2,583.23	5.56%	2,583.23	16.60%	00.00	0.00%	۲
Greenwaste Mixed	50.00	0.10%	92.57	0.20%	0.00	%00.0	92.57	0.30%	¥
Metal	324.00	0.65%	153.65	0.33%	153.65	0.99%	0.00	0.00%	z
MSW	13,792.00	27.77%	22,583.50	48.63%	0.00	%00.0	22,583.50	73.15%	¥
Mixed Recycling	182.00	0.37%	16.43	0.04%	16.43	0.11%	00.00	0.00%	z
Garments Not for Recycle	323.00	0.65%	2,188.01	4.71%	0.00	%00'0	2,188.01	7.09%	z
Plastic Bottles	81.00	0.16%	7.83	0.02%	7.83	0.05%	0.00	0.00%	z
Newspaper	44.00	%60.0	5.27	0.01%	5.27	0.03%	0.00	0.00%	¥
Office Paper	294.00	0.59%	68.80	0.15%	68.80	0.44%	0.00	0.00%	¥
Recycle Garments	0.00	%00.0	00.00	0.00%	0.00	%00.0	0.00	0.00%	z
Rejected Garments	25.00	0.05%	54.30	0.12%	0.00	%00.0	54.30	0.18%	z
Resi. Batteries	4.00	0.01%	0.13	0.00%	0.13	0.00%	00.00	0.00%	z
Resi. Charged	518.00	1.04%	80.48	0.17%	00'0	%00.0	80.48	0.26%	¥
Resi. Free ^(c)	17,720.00	35.68%	2,079.85	4.48%	0.00	%00'0	2,079.85	6.74%	z
Resi. Metal	256.00	0.52%	48.78	0.11%	48.78	0.31%	00.00	0.00%	z
Resi. White Goods	31.00	0.06%	5.78	0.01%	5.78	0.04%	00.00	%00.0	z
Special Waste	584.00	1.18%	808.05	1.74%	0.00	%00.0	808.05	2.62%	z
Tip Floor MSW	0.00	%00.0	00.00	0.00%	00.00	%00.0	00.00	0.00%	≻
Tip Floor Waste	00.00	%00.0	00.00	0.00%	00.00	%00.0	00.00	0.00%	۲
Tires	322.00	0.65%	207.98	0.45%	207.98	1.34%	00.00	0.00%	z
White Goods	45.00	%60'0	28.82	0.06%	28.82	0.19%	00.00	0.00%	z
Total	49,665.00	100.00%	46,436.47	100.00%	15,563.74	100.00%	30,872.73	100.00%	
					Recycled Percentage	33.52%			
Monthly Average	4,138.75		3.869.71		1.296.98		2.572.73		
	404 05								

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not proportly categorized. 2,572.73 100.24 50.53 150.77 4,138.75 161.25 Montnly Average Daily Average

DPW/SWMD Waste Delivery Period: February 1, 2006 through January 31, 2007

	Total Vehicles	% of Vehicles	Total Delivered %	% of total Waste	Diverted for Recycling	% OT KEC. 10	I otal Disposal % of Disposal		Include in the Model
Aluminum	33.00	0.07%	4.12	0.01%	4.12	0.03%	0.00	%00.0	z
Animal	2.00	%00.0	0.10	%00.0	00.00	%00.0	0.10	%00.0	۲
Backfill	823.00	1.80%	10,751.55	23.30%	10,751.55	66.16%	0.00	0.00%	z
Battery	0.00	%00.0	00.00	%00.0	00.00	%00.0	0.00	%00'0	z
C&D	685.00	1.50%	764.18	1.66%	00.00	%00.0	764.18	2.56%	z
Cardboard	2,426.00	5.31%	1,495.09	3.24%	1,280.30	7.88%	214.79	0.72%	۲
Garment Waste	236.00	0.52%	787.20	1.71%	00.00	%00'0	787.20	2.63%	z
Glass	103.00	0.23%	36.61	0.08%	36.61	0.23%	0.00	0.00%	z
Gov. C&D	58.00	0.13%	45.10	0.10%	0.00	0.00%	45.10	0.15%	z
Gov. Free-loads	4,778.00	10.45%	2,426.57	5.26%	00.00	%00.0	2,426.57	8.12%	z
Gov. Greenwaste ^(a)	494.00	1.08%	395.31	0.86%	395.31	2.43%	0.00	%00.0	۲
Gov. Special Waste ^(b)	50.00	0.11%	465.25	1.01%	465.25	2.86%	0.00	%00.0	z
Gov. White Goods	61.00	0.13%	36.41	0.08%	36.41	0.22%	0.00	%00.0	z
Greenwaste Clean	4,321.00	9.45%	2,851.31	6.18%	2,851.31	17.55%	0.00	%00.0	۲
Greenwaste Mixed	29.00	0.06%	47.98	0.10%	00.00	%00.0	47.98	0.16%	Υ.
Metal	106.00	0.23%	36.16	0.08%	36.16	0.22%	0.00	0.00%	z
MSW	12,118.00	26.50%	20,222.65	43.83%	0.00	%00.0	20,222.65	67.67%	٢
Mixed Recycling	382.00	0.84%	61.20	0.13%	61.20	0.38%	0.00	%00.0	z
Garments Not for Recycle	623.00	1.36%	2,659.49	5.76%	00.00	%00.0	2,659.49	8.90%	z
Plastic Bottles	53.00	0.12%	4.02	0.01%	4.02	0.02%	0.00	%00.0	z
Newspaper	33.00	0.07%	6.39	0.01%	6.39	0.04%	00.00	%00'0	7
Office Paper	181.00	0.40%	53.21	0.12%	53.21	0.33%	0.00	%00'0	۲
Recycle Garments	0.00	%00.0	00.00	%00.0	00.00	%00.0	0.00	0.00%	z
Rejected Garments	25.00	0.05%	33.64	0.07%	00.00	%00.0	33.64	0.11%	z
Resi. Batteries	0.00	%00.0	00.0	%00'0	0.00	%00.0	00.00	%00.0	z
Resi. Charged	494.00	1.08%	94.98	0.21%	0.00	%00.0	94.98	0.32%	۲
Resi. Free ^(c)	16,703.00	36.53%	1,943.97	4.21%	00.0	%00.0	1,943.97	6.50%	z
Resi. Metal	131.00	0.29%	18.89	0.04%	18.89	0.12%	00.00	%00.0	z
Resi. White Goods	33.00	0.07%	4.05	0.01%	4.05	0.02%	00.00	%00.0	z
Special Waste	438.00	0.96%	675.66	1.46%	30.95	0.19%	644.71	2.16%	z
Tip Floor MSW	0.00	%00.0	00.00	%00.0	0.00	%00'0	00.00	%00.0	۶
Tip Floor Waste	0.00	0.00%	00.00	%00.0	00.00	%00.0	0.00	%00.0	7
Tires	284.00	0.62%	206.04	0.45%	206.04	1.27%	00.00	0.00%	z
White Goods	25.00	0.05%	8.20	0.02%	8.20	0.05%	00.00	%00.0	z
Total	45,728.00	100.00%	46,135.33	100.00%	16,249.97	100.00%	29,885.36	100.00%	
					Recycling Percentage	35.22%			

 Monthly Average
 3,810.67
 3,844.61
 1,354.16
 2,490.45

 Daily Average
 148.47
 149.79
 52.76
 97.03

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 97.03

 (b) Special waste is composed of industrial pr
 0.00%
 0.00%
 0.00%

DPW/SWMD Waste Delivery Period: February 1, 2007 through January 31, 2008

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. 1	Total Disposal % of Disposal		Include in the Model
Aluminum	33.00	0.07%	4.12	0.01%	4.12	0.03%	0.00	0.00%	z
Animal	2.00	0.00%	0.10	%00.0	0.00	%00'0	0.10	0.00%	۲
Backfill	766.00	1.71%	10,446.69	23.22%	10,446.69	66.24%	00.00	0.00%	z
Battery	00.00	0.00%	00.00	0.00%	0.00	%00'0	00.00	0.00%	z
C&D	616.00	1.37%	657.94	1.46%	0.00	0.00%	657.94	2.25%	z
Cardboard	2,153.00	4.80%	1,280.30	2.85%	1,280.30	8.12%	00.00	%00.0	×
Garment Waste	186.00	0.41%	607.26	1.35%	0.00	%00'0	607.26	2.08%	z
Glass	98.00	0.22%	35.56	0.08%	35.56	0.23%	00.00	%00.0	z
Gov. C&D	49.00	0.11%	34.03	0.08%	0.00	%00'0	34.03	0.12%	z
Gov. Free-loads	4,453.00	9.92%	2,275.28	5.06%	0.00	%00'0	2,275.28	7.79%	z
Gov. Greenwaste ^(a)	460.00	1.02%	382.49	0.85%	382.49	2.43%	00.00	0.00%	7
Gov. Special Waste ^(b)	31.00	0.07%	305.99	0.68%	305.99	1.94%	0.00	0.00%	z
Gov. White Goods	57.00	0.13%	35.19	0.08%	35.19	0.22%	00.00	0.00%	z
Greenwaste Clean	4,321.00	9.63%	2,851.31	6.34%	2,851.31	18.08%	00.00	0.00%	Y
Greenwaste Mixed	29.00	0.06%	47.98	0.11%	0.00	%00'0	47.98	0.16%	Y
Metal	106.00	0.24%	36.16	0.08%	36.16	0.23%	00.00	0.00%	z
MSW	12,118.00	27.00%	20,222.65	44.95%	0.00	%00.0	20,222.65	69.20%	¥
Mixed Recycling	382.00	0.85%	61.20	0.14%	61.20	0.39%	0.00	0.00%	z
Garments Not for Recycle	623.00	1.39%	2,659.49	5.91%	0.00	%00.0	2,659.49	9.10%	z
Plastic Bottles	53.00	0.12%	4.02	0.01%	4.02	0.03%	0.00	0.00%	z
Newspaper	33.00	0.07%	6.39	0.01%	6.39	0.04%	00.00	0.00%	٢
Office Paper	181.00	0.40%	53.21	0.12%	53.21	0.34%	0.00	%00.0	Y
Recycle Garments	00.00	0.00%	0.00	0.00%	0.00	%00.0	00.00	0.00%	z
Rejected Garments	25.00	0.06%	33.64	0.07%	0.00	%00'0	33.64	0.12%	z
Resi. Batteries	0.00	0.00%	00.00	%00.0	0.00	%00'0	00.00	0.00%	z
Resi. Charged	494.00	1.10%	94.98	0.21%	0.00	%00'0	94.98	0.33%	۲
Resi. Free ^(c)	16,703.00	37.21%	1,943.97	4.32%	0.00	%00.0	1,943.97	6.65%	z
Resi. Metal	131.00	0.29%	18.89	0.04%	18.89	0.12%	00.00	%00'0	z
Resi. White Goods	33.00	0.07%	4.05	0.01%	4.05	0.03%	00.00	%00'0	z
Special Waste	438.00	0.98%	675.66	1.50%	30.95	0.20%	644.71	2.21%	z
Tip Floor MSW	00.00	0.00%	00.00	%00'0	0.00	%00'0	00.0	0.00%	×
Tip Floor Waste	00.00	0.00%	0.00	0.00%	0.00	%00'0	00.00	0.00%	7
Tires	284.00	0.63%	206.04	0.46%	206.04	1.31%	00.00	0.00%	z
White Goods	25.00	0.06%	8.20	0.02%	8.20	0.05%	00.00	0.00%	z
Total	44,883.00	100.00%	44,992.79	100.00%	15,770.76	100.00%	29,222.03	100.00%	82.67%
					Recycling Percentage	35.05%			
Monthly Average	3,740.25		3,749.40		1,314.23		2,435.17		
Contraction A villand	4 4 E 7 J		110.00		54.00		00 00		

 ually Average
 145.72
 2,435.17

 ually Average
 145.72
 2,435.17

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass dippings or leaves, and domestic or industrial kitchen wastes.
 94.88

 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 0.0

DPW/SWMD Waste Delivery Period: February 1, 2008 through January 31, 2009

Ĭ	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec.	Total Disposal %	% of Disposal	Include in the Model
Aluminum	0.00	0.00%	00.0	%00.0	0.00	0.00%	00.00	%00.0	z
Animal	2.00	0.01%	0.93	%00.0	0.00	%00.0	0.93	0.00%	×
Backfill	1,510.00	3.78%	13,589.87	34.92%	13,589.87	82.19%	00.00	0.00%	z
Battery	0.00	0.00%	00.0	%00.0	0.00	%00"0	00.00	%00.0	z
C&D	604.00	1.51%	734.76	1.89%	110.00	0.67%	624.76	2.79%	z
Cardboard	988.00	2.48%	389.58	1.00%	389.58	2.36%	00.0	%00"0	Y
Garment Waste	0.00	%00.0	00.00	%00.0	00.00	%00.0	00.00	%00.0	z
Glass	100.00	0.25%	29.93	0.08%	29.93	0.18%	00.0	0.00%	z
Gov. C&D	20.00	0.05%	10.10	0.03%	0.00	%00.0	10.10	0.05%	z
Gov. Free-loads	2,763.00	6.92%	1,106.24	2.84%	0.00	%00'0	1,106.24	4.94%	z
Gov. Greenwaste ^(a)	199.00	0.50%	104.82	0.27%	104.82	0.63%	00.0	0.00%	¥
Gov. Special Waste ^(b)	2.00	0.01%	25.80	0.07%	25.80	0.16%	00.0	0.00%	z
Gov. White Goods	3.00	0.01%	0.50	%00.0	0.50	%00.0	00.0	%00.0	z
Greenwaste Clean	3,947.00	9.89%	1,908.38	4.90%	1,908.38	11.54%	00.00	0.00%	¥
Greenwaste Mixed	26.00	0.07%	20.79	0.05%	0.00	%00.0	20.79	%60'0	Y
Metal	85.00	0.21%	33.34	%60.0	33.34	0.20%	0.00	%00.0	z
MSW	10,184.00	25.52%	17,266.51	44.37%	0.00	%00'0	17,266.51	77.14%	¥
Mixed Recycling	591.00	1.48%	75.68	0.19%	75.68	0.46%	00.00	%00.0	z
Garments Not for Recycle	311.00	0.78%	1,129.77	2.90%	0.00	%00.0	1,129.77	5.05%	z
Plastic Bottles	48.00	0.12%	4.55	0.01%	4.55	0.03%	0.00	%00.0	z
Newspaper	7.00	0.02%	1.53	0.00%	1.53	0.01%	0.00	0.00%	Y
Office Paper	227.00	0.57%	90.23	0.23%	90.23	0.55%	0.00	0.00%	Y
Recycle Garments	00.00	%00.0	00.00	0.00%	0.00	%00.0	00.00	%00.0	Z
Rejected Garments	1.00	0.00%	0.28	%00.0	0.00	%00'0	0.28	%00'0	z
Resi. Batteries	2.00	0.01%	0.10	%00.0	0.10	%00'0	0.00	%00'0	z
Resi. Charged	942.00	2.36%	146.12	0.38%	00.00	%00'0	146.12	0.65%	×
Resi. Free ^(c)	17,028.00	42.67%	2,077.89	5.34%	0.00	%00.0	2,077.89	9.28%	z
Resi, Metal	24.00	0.06%	3.43	0.01%	3.43	0.02%	00.0	%00'0	z
Resi. White Goods	44.00	0.11%	9.63	0.02%	9.63	%90.0	00.0	0.00%	z
Special Waste	0.00	0.00%	00.00	%00.0	0.00	%00'0	00.00	%00.0	z
Tip Floor MSW	0.00	%00.0	00.00	%00.0	00.00	%00'0	00.00	%00.0	Y
Tip Floor Waste	0.00	0.00%	00.00	%00.0	0.00	%00'0	00.00	%00'0	۲
Tires	244.00	0.61%	158.08	0.41%	158.08	0.96%	00.00	%00'0	z
White Goods	0.00	%00.0	00.00	%00.0	0.00	%00'0	00.00	%00.0	z
Total	39,902.00	100.00%	38,918.84	100.00%	16,535,45	100.00%	22,383.39	100.00%	89.36%
					Recycling Percentage	42.49%			82.67%
Monthly Average	3 325 17		3 243 24		1 377 95		1 865 28		
Denor function	120.66		136 36		63 60		72 67		
	CC-071		00.021			1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	10.71		

 Daily Average
 129.55
 126.36
 72.67

 (a) Green waste is composed of organic waste that can be composted, i.e. retuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 53.69
 72.67

 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not proporty categorized.

DPW/SWMD Waste Delivery Period: February 1, 2009 through January 31, 2010

0	I otal venicles				Conference and				
	0.00	%00.0	0.00	%00.0	0.00	%00'0	00.00	%00.0	Z
	1.00	0.00%	0.24	%00.0	0.00	%00'0	0.24	%00.0	¥
	585.00	1.76%	5,893.00	20.98%	5,893.00	63.63%	00.0	0.00%	z
	0.00	0.00%	0.00	0.00%	0.00	%00.0	00.0	0.00%	Z
	475.00	1.43%	472.94	1.68%	0.00	%00'0	472.94	2.51%	Z
	1,219.00	3.66%	659.54	2.35%	659.54	7.12%	00.0	0.00%	Y
	0.00	%00.0	0.00	%00.0	0.00	%00'0	00.0	0.00%	Z
	118.00	0.35%	36.16	0.13%	36.16	0.39%	00.0	0.00%	z
	2.00	0.01%	0.38	%00.0	0.00	%00.0	0.38	0.00%	z
	2,803.00	8.42%	1,337.46	4.76%	0.00	%00'0	1,337.46	7.10%	z
Gov. Greenwaste ^(a)	281.00	0.84%	146.16	0.52%	146.16	1.58%	00.0	0.00%	×
Gov. Special Waste (b)	54.00	0.16%	621.85	2.21%	621.85	6.71%	0.00	0.00%	Z
	61.00	0.18%	20.54	0.07%	20.54	0.22%	0.00	0.00%	z
	3,504.00	10.53%	1,518.91	5.41%	1,518.91	16.40%	00.0	0.00%	×
	18.00	0.05%	59.59	0.21%	0.00	%00.0	59.59	0.32%	¥
	42.00	0.13%	16.04	0.06%	16.04	0.17%	00.0	0.00%	Z
	8,166.00	24.54%	14,904.29	53.05%	0.00	%00.0	14,904.29	79.14%	٢
	391.00	1.17%	62.46	0.22%	62.46	0.67%	00.0	0.00%	z
Garments Not for Recycle	23.00	0.07%	142.58	0.51%	0.00	%00.0	142.58	0.76%	z
	89.00	0.27%	25.44	%60'0	25.44	0.27%	0.00	%00.0	z
	2.00	0.01%	2.93	0.01%	2.93	0.03%	0.00	0.00%	¥
	139.00	0.42%	86.60	0.31%	86.60	0.94%	0.00	0.00%	¥
	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	z
Rejected Garments	0.00	0.00%	0.00	%00'0	0.00	%00.0	0.00	0.00%	z
	2.00	0.01%	0.19	0.00%	0.19	%00'0	0.00	0.00%	z
	804.00	2.42%	123.60	0.44%	0.00	%00'0	123.60	0.66%	¥
	14,196.00	42.66%	1,779.48	6.33%	0.00	%00.0	1,779.48	9.45%	z
	6.00	0.02%	2.19	0.01%	2.19	0.02%	00.00	0.00%	z
	5.00	0.02%	0.77	0.00%	0.77	0.01%	0.00	0.00%	z
	9.00	0.03%	12.20	0.04%	0.00	%00'0	12.20	0.06%	z
	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	¥
	0.00	0.00%	0.00	%00.0	0.00	%00'0	0.00	0.00%	¥
	261.00	0.78%	162.10	0.58%	162.10	1.75%	0.00	%00.0	z
	22.00	0.07%	6.43	0.02%	6.43	0.07%	00.0	0.00%	z
Total	33,278.00	100.00%	28,094.07	100.00%	9,261.31	100.00%	18,832.76	100.00%	91.48%
					Recycling Percentage	32.97%			89.36%
									82.67%
Monthly Average	2,773.17		2,341.17		771.78		1.569.40		

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not proposedy categorized.

DPW/SWMD Waste Delivery Period: February 1, 2010 through January 31, 2011

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. 7	Total Disposal % of Disposal	of Disposal	Include in the Model
Aluminum	0.00	%00.0	00.00	%00.0	00.00	%00.0	00.00	0.00%	z
Animal	21.00	0.05%	06.0	%00.0	0.00	%00.0	0.90	%00'0	۲
Backfill	667.00	1.59%	7,995.22	25.04%	7,995.22	70.51%	00.00	%00'0	z
Battery	1.00	%00.0	0.02	%00.0	0.02	%00'0	00.00	%00'0	z
C&D	307.00	0.73%	322.99	1.01%	0.00	%00.0	322.99	1.57%	z
Cardboard	1,441.00	3.43%	871.48	2.73%	871.48	7.69%	00.0	%00.0	۲
Garment Waste	00.00	%00.0	00.00	%00.0	00.00	0.00%	00.00	%00'0	z
Glass	61.00	0.15%	14.33	0.04%	14.33	0.13%	00.00	0.00%	z
Gov. C&D	0.00	%00.0	00.00	%00.0	00.00	%00.0	00.0	%00'0	z
Gov. Free-loads	2,688.00	6.40%	1,336.96	4.19%	0.00	0.00%	1,336.96	6.49%	z
Gov. Greenwaste ^(a)	205.00	0.49%	80.15	0.25%	80.15	0.71%	0.00	%00'0	۲
Gov. Special Waste (b)	148.00	0.35%	1,609.62	5.04%	0.00	%00.0	1,609.62	7.82%	z
Gov. White Goods	1.00	%00.0	0.23	%00.0	0.23	%00'0	00.0	%00'0	z
Greenwaste Clean	3,171.00	7.55%	1,972.76	6.18%	1,972.76	17.40%	00.0	%00.0	۲
Greenwaste Mixed	2.00	%00.0	1.31	%00.0	0.00	%00.0	1.31	0.01%	۲
Metal	56.00	0.13%	22.55	0.07%	22.55	0.20%	0.00	%00.0	z
MSW	7,739.00	18.42%	15,351.56	48.09%		%00.0	15,351.56	74.58%	۲
Mixed Recycling	463.00	1.10%	66.70	0.21%	66.70	0.59%	0.00	%00'0	z
Garments Not for Recycle	0.00	0.00%	00.00	0.00%	0.00	%00'0	0.00	%00'0	z
Plastic Bottles	31.00	0.07%	4.78	0.01%		0.04%	0.00	%00.0	z
Newspaper	2.00	%00.0	0.22	0.00%	0.22	%00.0	0.00	%00.0	۲
Office Paper	247.00	0.59%	120.51	0.38%	120.51	1.06%	0.00	%00.0	7
Recycle Garments	0.00	0.00%	00.00	%00.0	0.00	%00.0	0.00	%00.0	z
Rejected Garments	0.00	%00.0	00.00	%00.0	00.00	%00'0	0.00	%00'0	z
Resi. Batteries	00.00	%00.0	00.00	%00.0	0.00	%00'0	0.00	%00.0	z
Resi. Charged	8,987.00	21.39%	144.58	0.45%	0.00	%00.0	144.58	0.70%	۲
Resi. Free ^(c)	15,454.00	36.79%	1,808.16	5.66%	00.00	%00'0	1,808.16	8.78%	z
Resi. Metal	6.00	0.01%	2.19	0.01%	2.19	0.02%	00.00	%00'0	Z
Resi. White Goods	24.00	0.06%	3.08	0.01%	3.08	0.03%	00.00	%00'0	z
Special Waste	8.00	0.02%	8.78	0.03%	0.00	%00.0	8.78	0.04%	z
Tip Floor MSW	00.00	%00.0	00.0	%00.0	0.00	%00'0	00.00	%00'0	۲
Tip Floor Waste	0.00	0.00%	00.00	%00.0	00.00	%00.0	0.00	%00'0	۲
Tires	271.00	0.65%	176.47	0.55%	176.47	1.56%	00.00	%00'0	z
White Goods	9.00	0.02%	8.35	0.03%	8.35	0.07%	00.00	%00'0	z
Total	42,010.00	100.00%	31,923.90	100.00%	11,339.04	100.00%	20,584.86	100.00%	92.80%
					Recycling Percentage	35.52%			91.48%
									89.36%
Monthly Average	3,500.83		2,660.33		944.92		1,715.41		
	the second s								

 илиу Average
 136.40
 103.65
 1,715.41

 илиу Average
 136.40
 103.65
 56.83

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 66.83

 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not propoerly categorized.

DPW/SWMD Waste Delivery Period: February 1, 2011 through January 31, 2012

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. 1	Total Disposal % of Disposal		Include in the Model
Aluminum	0.00	%00.0	0.00	0.00%	0.00	%00'0	0.00	%00.0	z
Animal	56.00	0.18%	6.45	0.02%	0.00	%00'0	6.45	0.03%	7
Backfill	754.00	2.43%	10,065.67	28.50%	10,065.67	70.08%	0.00	%00.0	z
Battery	0.00	%00.0	00.00	0.00%	0.00	%00'0	0.00	%00.0	z
C&D	291.00	0.94%	586.20	1.66%	420.00	2.92%	166.20	%67.0	z
Cardboard	941.00	3.04%	693.32	1.96%	693.32	4.83%	00.00	%00.0	×
Garment Waste	0.00	%00.0	0.00	%00.0	0.00	%00'0	0.00	%00.0	z
Glass	41.00	0.13%	25.46	0.07%	25.46	0.18%	00.00	%00.0	z
Gov. C&D	24.00	0.08%	66.66	0.19%	0.00	%00'0	66.66	0.32%	z
Gov. Free-loads	2,331.00	7.53%	1,218.73	3.45%	0.00	%00'0	1,218.73	5.81%	z
Gov. Greenwaste ^(a)	171.00	0.55%	211.70	0.60%	211.70	1.47%	00.00	%00.0	×
Gov. Special Waste (b)	190.00	0.61%	2,083.34	5.90%	0.00	%00'0	2,083.34	9.94%	z
Gov. White Goods	1.00	%00.0	0.29	0.00%	0.29	%00'0	0.00	%00.0	z
Greenwaste Clean	3,297.00	10.64%	2,562.71	7.26%	2,562.71	17.84%	0.00	%00.0	7
Greenwaste Mixed	5.00	0.02%	14.78	0.04%	0.00	%00'0	14.78	0.07%	7
Metal	12.00	0.04%	3.60	0.01%	3.60	0.03%	0.00	%00.0	z
MSW	7,142.00	23.06%	15,528.51	43.96%	0.00	%00'0	15,528.51	74.09%	7
Mixed Recycling	256.00	0.83%	39.84	0.11%	39.84	0.28%	00.00	%00.0	z
Garments Not for Recycle	0.00	%00.0	0.00	%00.0	0.00	%00'0	00.00	%00.0	z
Plastic Bottles	33.00	0.11%	4.78	0.01%	4.78	0.03%	0.00	%00.0	z
Newspaper	3.00	0.01%	1.65	0.00%	1.65	0.01%	0.00	%00.0	×
Office Paper	98.00	0.32%	59.28	0.17%	59.28	0.41%	00.00	0.00%	×
Recycle Garments	0.00	0.00%	0.00	0.00%	0.00	%00'0	00.00	%00.0	z
Rejected Garments	00.00	0.00%	00.00	%00.0	0.00	%00'0	0.00	%00.0	z
Resi. Batteries	0.00	%00.0	00.00	%00.0	0.00	%00'0	0.00	%00.0	z
Resi. Charged	926.00	2.99%	152.02	0.43%	0.00	%00'0	152.02	0.73%	×
Resi. Free ^(c)	13,900.00	44.88%	1,707.89	4.84%	0.00	%00'0	1,707.89	8.15%	z
Resi. Metal	7.00	0.02%	1.15	%00.0	1.15	0.01%	00.00	%00.0	z
Resi, White Goods	28.00	%60'0	3.20	0.01%	3.20	0.02%	0.00	%00.0	z
Special Waste	6.00	0.02%	15.02	0.04%	0.00	%00'0	15.02	0.07%	z
Tip Floor MSW	0.00	%00.0	00.00	%00'0	0.00	%00'0	0.00	0.00%	×
Tip Floor Waste	0.00	%00.0	00.00	%00.0	0.00	%00'0	0.00	%00'0	×
Tires	367.00	1.18%	215.75	0.61%	215.75	1.50%	00.00	%00'0	Z
White Goods	94.00	0.30%	54.98	0.16%	54.98	0.38%	0.00	%00'0	Z
Total	30,974.00	100.00%	35,322.98	100.00%	14,363.38	100.00%	20,959.60	100.00%	93.46%
					Recycling Percentage	40.66%			
Monthly Average	2,581.17		2,943.58		1,196.95		1,746.63		
Daily Average			114.69		46.63		68.05		
(a) Croan wasto is composed of orns	d of ornanic wasta	that and he compo	atod i a rafina fro	andress arobas m	main or look of do main do mai	indi an otion	down and all laide		

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not proportly categorized.

DPW/SWMD Waste Delivery Period: February 1, 2012 through January 31, 2013

	Total Vehicles	% of Vehicles	Total Delivered %	% of total Waste	Diverted for Recycling	% of Rec.	Total Disposal % of Disposal	of Disposal	Include in the Model
Aluminum	00.00	0.00%	00.00	%00.0	00.00	%00.0	00.00	%00.0	z
	14.00	0.05%	2.97	0.02%	0.00	%00.0	2.97	0.02%	۲
	59.00	0.22%	232.60	1.26%	232.60	7.27%	00.00	%00.0	z
	0.00	%00.0	00.0	%00'0	0.00	%00.0	0.00	%00.0	z
C&D	157.00	0.57%	159.21	0.86%	0.00	%00.0	159.21	1.04%	z
Cardboard	849.00	3.10%	455.28	2.46%	455.28	14.23%	0.00	%00.0	۲
Garment Waste	0.00	%00.0	00.00	%00.0	0.00	%00.0	00.0	%00.0	z
	117.00	0.43%	33.85	0.18%	33.85	1.06%	0.00	%00.0	z
Gov. C&D	13.00	0.05%	51.73	0.28%	0.00	%00.0	51.73	0.34%	z
Gov. Free-loads	2,618.00	9.57%	2,483.67	13.43%	0.00	%00.0	2,483.67	16.23%	z
Gov. Greenwaste ^(a)	244.00	0.89%	337.10	1.82%	307.51	9.61%	29.59	0.19%	۲
Gov. Special Waste (b)	7.00	0.03%	37.22	0.20%	0.00	%00.0	37.22	0.24%	z
Gov. White Goods	17.00	0.06%	10.30	%90.0	10.30	0.32%	0.00	%00.0	z
Greenwaste Clean	2,912.00	10.65%	1,768.55	9.56%	1,768.55	55.26%	0.00	%00.0	¥
Greenwaste Mixed	15.00	0.05%	33.24	0.18%	0.00	%00.0	33.24	0.22%	×
	38.00	0.14%	11.60	0.06%	11.60	0.36%	0.00	0.00%	z
	5,670.00	20.74%	10,805.60	58.41%	0.00	%00.0	10,805.60	70.63%	٢
Mixed Recycling	319.00	1.17%	46.51	0.25%	46.51	1.45%	00.0	%00.0	z
Garments Not for Recycle	0.00	%00.0	0.00	%00.0	0.00	%00.0	00.0	%00.0	z
Plastic Bottles	17.00	0.06%	2.47	0.01%	2.47	0.08%	0.00	%00.0	z
Newspaper	4.00	0.01%	2.36	0.01%	2.36	0.07%	00.00	%00.0	۲
Office Paper	83.00	0.30%	86.84	0.47%	86.84	2.71%	0.00	%00.0	۲
Recycle Garments	0.00	%00.0	00.0	%00.0	0.00	%00.0	00.0	%00.0	z
Rejected Garments	0.00	%00.0	00.0	%00.0	0.00	%00'0	0.00	%00.0	z
Resi, Batteries	0.00	%00.0	00.0	%00.0	0.00	%00'0	00.0	%00.0	z
Resi. Charged	581.00	2.12%	113.14	0.61%	0.00	%00'0	113.14	0.74%	7
Resi. Free ^(c)	13,073.00	47.81%	1,570.16	8.49%	0.00	%00'0	1,570.16	10.26%	z
Resi. Metal	18.00	0.07%	1.24	0.01%	1.24	0.04%	00.0	%00.0	Z
Resi. White Goods	26.00	0.10%	6.56	0.04%	6.56	0.20%	00.0	%00.0	z
Special Waste	6.00	0.02%	12.49	0.07%	0.00	%00.0	12.49	0.08%	z
Tip Floor MSW	0.00	%00.0	00.0	%00.0	0.00	%00'0	00.0	%00.0	7
Tip Floor Waste	0.00	%00.0	00.0	%00.0	0.00	%00'0	0.00	%00.0	۲
	414.00	1.51%	217.37	1.18%	217.37	6.79%	00.0	%00.0	z
White Goods	74.00	0.27%	17.18	%60.0	17.18	0.54%	0.00	%00'0	z
Total	27,345.00	100.00%	18,499.24	100.00%	3,200.22	100.00%	15,299.02	100.00%	83.03%
					Recycling Percentage	17.30%			93.46%
Monthly Average	2 278 75		1 541 60		266 69		1 274 92		
ofference of the second			pp-1 + p(1				1,11,14		

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not proposely categorized. 49.67 10.39 60.06 Daily Average

88.78

DPW/SWMD Waste Delivery Period: February 1, 2013 through January 31, 2014

			62.23		10.59		72.82	that any ha parent	92.24	Daily Average 92.24 72.82
			1,597.28		271.84		1,869.12		2,367.42	Monthly Average
93.46%					3					
83.03%				14.54%	Recycling Percentage					
94.08%		100.00%	19,167.37	100.00%	3,262.04	100.00%	22,429.41	100.00%	28,409.00	Total
z		0.03%	6.16	0.53%	17.18	0.10%	23.34	0.25%	70.00	White Goods
z	_	0.00%	0.00	4.44%	144.69	0.65%	144.69	1.09%	310.00	Tires
×		0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Tip Floor Waste
×		0.00%	0.00	0.00%	- 0.00	0.00%	0.00	0.00%	0.00	Tip Floor MSW
z		1.51%	288.49	0.00%	0.00	1.29%	288.49	0.15%	42.00	Special Waste
z		0.00%	0.00	0.18%	5.88	0.03%	5.88	0.13%	38.00	Resi. White Goods
z		0.00%	0.00	0.13%	4.31	0.02%	4.31	0.11%	32.00	Resi. Metal
z		7.64%	1,464.15	0.00%	0.00	6.53%	1,464.15	44.79%	12,725.00	Resi. Free ^(c)
¥		0.52%	99.53	0.00%	0.00	0.44%	99.53	1.78%	506.00	Resi. Charged
z		0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Resi. Batteries
z		0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Rejected Garments
z		0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Recycle Garments
Y		0.00%	0.00	1.24%	40.53	0.18%	40.53	0.31%	87.00	Office Paper
Y		0.00%	0.00	0.03%	0.96	0.00%	0.96	0.04%	10.00	Newspaper
z		0.00%	0.00	0.04%	1.17	0.01%	1.17	0.08%	24.00	Plastic Bottles
z		0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Garments Not for Recycle
z		0.00%	0.00	0.82%	26.74	0.12%	26.74	1.58%	449.00	Mixed Recycling
×		82.43%	15,799.34	0.00%	0.00	70.44%	15,799.34	26.40%	7,499.00	MSM
z		0.00%	0.00	0.19%	6.34	0.03%	6.34	0.07%	20.00	Metal
×		0.17%	31.93	0.00%	0.00	0.14%	31.93	0.07%	19.00	Greenwaste Mixed
×		0.00%	0.10	41.46%	1,352.28	6.03%	1,352.38	7.80%	2,216.00	Greenwaste Clean
z	_	0.00%	0.00	0.67%	21.76	0.10%	21.76	0.10%	27.00	Gov. White Goods
z	_	0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Gov. Special Waste (b)
×		0.00%	0.79	15.10%	492.69	2.20%	493.48	1.81%	513.00	Gov. Greenwaste ^(a)
z	_	5.33%	1,021.26	0.00%	0.00	4.55%	1,021.26	7.72%	2,192.00	Gov. Free-loads
z	_	0.21%	39.81	0.00%	0.00	0.18%	39.81	0.07%	20.00	Gov. C&D
z		0.04%	7.45	0.55%	17.84	0.11%	25.29	0.42%	120.00	Glass
z	_	0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Garment Waste
×		0.00%	0.00	8.79%	286.65	1.28%	286.65	3.23%	918.00	Cardboard
z	_	2.07%	395.84	0.00%	0.00	1.76%	395.84	1.30%	368.00	C&D
z	_	0.00%	0.00	0.00%	0.11	0.00%	0.11	0.01%	2.00	Battery
z		0.01%	1.45	25.84%	842.91	3.76%	844.36	0.56%	159.00	Backfill
×		0.06%	11.07	0.00%	0.00	0.05%	11.07	0.15%	43.00	Animal
z	_	0.00%	0.00	0.00%	0.00	0.00%	0.00	0.00%	0.00	Aluminum
Include in the Model	Include in	of Disposal	Total Disposal %		Diverted for Recycling % of Rec.	Total Delivered % of total Waste	Total Delivered	% of Vehicles	Total Vehicles	

11 of 16

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not proporty categorized.

DPW/SWMD Waste Delivery Period: February 1, 2014 through January 31, 2015

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. T	Total Disposal % of Disposal		Include in the Model
Aluminum	0.00	0.00%	00.00	%00.0	0.00	%00.0	00.00	0.00%	Z
Animal	56.00	0.21%	11.20	0.04%	0.00	%00'0	11.20	0.06%	×
Backfill	577.00	2.12%	5,915.29	18.81%	5,915.29	45.97%	0.00	0.00%	z
Battery	1.00	%00.0	0.12	%00.0	0.12	%00'0	0.00	%00'0	z
C&D	798.00	2.93%	1,000.72	3.18%	1,000.72	7.78%	0.00	%00.0	z
Cardboard	871.00	3.20%	230.01	0.73%	230.01	1.79%	0.00	0.00%	7
Garment Waste	00.00	%00.0	00.00	%00.0	0.00	%00'0	0.00	%00.0	z
Glass	102.00	0.37%	20.43	0.06%	20.43	0.16%	0.00	%00.0	z
Gov. C&D	14.00	0.05%	32.24	0.10%	32.24	0.25%	0.00	0.00%	z
Gov. Free-loads	2,512.00	9.23%	723.88	2.30%	0.00	%00.0	723.88	3.90%	z
Gov. Greenwaste ^(a)	281.00	1.03%	297.48	0.95%	297.48	2.31%	0.00	0.00%	۲
Gov. Special Waste (b)	0.00	%00.0	00.00	%00.0	0.00	%00'0	0.00	%00.0	z
Gov. White Goods	6.00	0.02%	1.90	0.01%	1.90	0.01%	0.00	%00.0	z
Greenwaste Clean	1,925.00	7.07%	1,462.83	4.65%	1,462.83	11.37%	0.00	%00.0	≻
Greenwaste Mixed	46.00	0.17%	138.36	0.44%	0.00	%00.0	138.36	0.74%	×
Metal	99.00	0.36%	28.63	%60.0	28.63	0.22%	0.00	%00.0	z
MSW	7,004.00	25.73%	16,081.18	51.15%	0.00	%00.0	16,081.18	86.58%	۲
Mixed Recycling	463.00	1.70%	34.37	0.11%	34.37	0.27%	0.00	0.00%	z
Garments Not for Recycle	00.00	%00.0	0.00	%00.0	0.00	0.00%	0.00	0.00%	z
Plastic Bottles	36.00	0.13%	1.90	0.01%	1.90	0.01%	0.00	%00.0	z
Newspaper	11.00	0.04%	4.14	0.01%	4.14	0.03%	0.00	%00.0	۲
Office Paper	147.00	0.54%	48.63	0.15%	48.63	0.38%	0.00	0.00%	¥
Recycle Garments	0.00	%00.0	0.00	%00.0	0.00	%00.0	0.00	%00.0	z
Rejected Garments	00.00	%00.0	0.00	%00.0	0.00	%00.0	0.00	%00'0	z
Resi, Batteries	00.00	%00.0	0.00	%00.0	0.00	%00.0	0.00	%00.0	z
Resi. Charged	504.00	1.85%	85.49	0.27%	0.00	%00.0	85.49	0.46%	۲
Resi. Free ^(c)	10,696.00	39.29%	1,245.34	3.96%	0.00	%00.0	1,245.34	6.70%	z
Resi. Metal	283.00	1.04%	3,414.05	10.86%	3,414.05	26.53%	0.00	%00.0	z
Resi. White Goods	386.91	1.42%	216.53	0.69%	216.53	1.68%	0.00	%00.0	z
Special Waste	42.00	0.15%	288.49	0.92%	0.00	%00.0	288.49	1.55%	z
Tip Floor MSW	0.00	%00.0	0.00	0.00%	0.00	%00.0	0.00	%00.0	7
Tip Floor Waste	0.00	%00.0	0.00	%00.0	0.00	%00.0	0.00	%00'0	×
Tires	310.00	1.14%	144.69	0.46%	144.69	1.12%	0.00	%00.0	z
White Goods	50.00	0.18%	12.49	0.04%	12.49	0.10%	0.00	%00.0	z
Total	27,220.91	100.00%	31,440.39	100.00%	12,866.45	100.00%	18,573.94	100.00%	
					Recycling Percentage	40.92%			
Monthly Average	2.268.41		2,620.03		1.072.20		1.547.83		
	00 00								

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not proposely categorized.

102.08

88.38 2,268.41

Daily Average

60.31

41.77

DPW/SWMD Waste Delivery Period: February 1, 2015 through January 15, 2016

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec.	Total Disposal %	% of Disposal	Include in the Model
Aluminum	0.00	0.00%	00.0	0.00%	0.00	%00.0	0.00	0.00%	z
Animal	85.00	0.29%	8.63	0.02%	0.00	%00'0	8.63	0.04%	۲
Backfill	708.00	2.39%	7,568.22	21.07%	7,568.22	52.20%	00.00	%00.0	Z
Battery	00.00	%00.0	00.00	0.00%	0.00	%00.0	00.00	%00'0	z
C&D	1,351.00	4.57%	1,988.21	5.54%	0.00	%00.0	1,988.21	9.28%	z
Cardboard	956.00	3.23%	286.56	0.80%	286.56	1.98%	0.00	%00.0	7
Garment Waste	0.00	0.00%	0.00	0.00%	0.00	%00'0	0.00	0.00%	z
Glass	83.00	0.28%	13.98	0.04%	13.98	0.10%	0.00	0.00%	z
Gov. C&D	45.00	0.15%	115.41	0.32%	0.00	%00.0	115.41	0.54%	z
Gov. Free-loads	2,825.00	9.55%	1,148.48	3.20%	0.00	%00.0	1,148.48	5.36%	z
Gov. Greenwaste ^(a)	647.00	2.19%	692.77	1.93%	692.77	4.78%	0.00	0.00%	7
Gov. Special Waste ^(b)	0.00	0.00%	00.0	0.00%	0.00	%00'0	00.00	0.00%	z
Gov. White Goods	13.00	0.04%	7.12	0.02%	7.12	0.05%	0.00	0.00%	z
Greenwaste Clean	2,984.00	10.09%	5,604.64	15.60%	5,604.64	38.65%	0.00	0.00%	¥
Greenwaste Mixed	223.00	0.75%	545.04	1.52%	0.00	%00.0	545.04	2.54%	¥
Metal	139.00	0.47%	61.97	0.17%	61.97	0.43%	0.00	0.00%	z
MSW	6,485.00	21.93%	15,964.79	44.45%	0.00	%00'0	15,964.79	74.53%	۲
Mixed Recycling	438.00	1.48%	35.86	0.10%	35.86	0.25%	0.00	0.00%	z
Garments Not for Recycle	0.00	0.00%	0.00	0.00%	0.00	%00.0	0.00	0.00%	z
Plastic Bottles	90.00	0.30%	5.33	0.01%	5.33	0.04%	0.00	0.00%	z
Newspaper	12.00	0.04%	3.87	0.01%	3.87	0.03%	0.00	0.00%	Y
Office Paper	149.00	0.50%	61.47	0.17%	40.53	0.28%	20.94	0.10%	۲
Recycle Garments	00.00	0.00%	0.00	%00.0	0.00	%00.0	0.00	0.00%	z
Rejected Garments	00.00	%00.0	0.00	%00.0	0.00	%00'0	00.00	%00'0	z
Resi. Batteries	00.00	0.00%	0.00	%00.0	0.00	%00'0	0.00	0.00%	z
Resi. Charged	668.00	2.26%	111.32	0.31%	0.00	%00'0	111.32	0.52%	×
Resi. Free ^(c)	11,072.00	37.45%	1,168.53	3.25%	0.00	%00'0	1,168.53	5.46%	z
Resi. Metal	120.00	0.41%	18.81	0.05%	18.81	0.13%	00.00	0.00%	z
Resi. White Goods	28.00	%60.0	4.18	0.01%	4.18	0.03%	00.00	0.00%	z
Special Waste	84.00	0.28%	315.75	0.88%	0.00	%00'0	315.75	1.47%	z
Tip Floor MSW	00'0	0.00%	0.00	0.00%	0.00	%00'0	00.00	0.00%	×
Tip Floor Waste	0.00	0.00%	0.00	%00.0	0.00	%00'0	00.00	0.00%	×
Tires	314.00	1.06%	178.35	0.50%	144.69	1.00%	33.66	0.16%	z
White Goods	47.00	0.16%	10.97	0.03%	10.97	0.08%	0.00	%00.0	z
Total	29,566.00	100.00%	35,920.26	100.00%	14,499.50	100.00%	21,420.76	100.00%	93.96%
					Recycling Percentage	40.37%			
Monthly Average	2.463.83		2.993.36		1 208 29		1.785.06		

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not proportly categorized. 69.55 47.08 116.62 95.99 Daily Average

> DPW/SWMD Waste Delivery Period: February 1, 2016 through January 31, 2017

(a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
(b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
(c) Waste that were not propoerly categorized.

DPW/SWMD Waste Delivery Period: February 1, 2017 through January 31, 2018

Total Vehicles % of Vehicles 0 0.00%
9 0.02%
656 1.42% 4,545.91
0.00%
3,216 6.98% 3,278.05
0.00%
6,143 13.33%
1,098 2.38% 2,967.59
0.24%
3.67% 5,0
0.02%
2.15%
56.43% 22,5
648 1.41% 39.58
0.04%
0 0.00%
0.01%
0 0.00%
0 0.00% 0.00
884 1.92% 369.25
0 0.00%
46,077 100.00% 40,892.30
3.840 3.408
*

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not propoerly categorized. 87.67 1,157.38 45.09 3,408 132.77 3,840 150 Daily Average

DPW/SWMD Waste Delivery Period: February 1, 2003 through January 31, 2018

	Total Vehicles	% of Vehicles	Total Delivered	% of total Waste	Diverted for Recycling	% of Rec. T	Total Disposal % of Disposal	of Disposal	Include in the Model
Aluminum	438.00	0.07%	50.52	0.01%	50.52	0.03%	0.00	0.00%	z
Animal	335.00	0.06%	48.52	0.01%	0.00	%00.0	48.52	0.01%	۲
Backfill	8,730.00	1.49%	92,080.16	16.64%	92,078.71	50.43%	1.45	%00'0	z
Battery	13.00	0.00%	3.34	%00.0	3.34	%00.0	00.00	%00.0	z
C&D	13,887.00	2.37%	17,023.98	3.08%	2,200.29	1.21%	14,823.69	4.00%	z
Cardboard	19,888.00	3.40%	10,231.53	1.85%	10,016.74	5.49%	214.79	0.06%	۲
Garment Waste	5,993.00	1.02%	12,758.01	2.31%	11,207.46	6.14%	1,550.55	0.42%	z
Glass	8,082.00	1.38%	477.01	0.09%	469.56	0.26%	7.45	0.00%	z
Gov. C&D	664.00	0.11%	1,135.00	0.21%	32.24	0.02%	1,102.76	0.30%	z
Gov. Free-loads	48,271.00	8.25%	24,494.02	4.43%	0.00	%00.0	24,494.02	6.61%	z
Gov. Greenwaste ^(a)	8,732.00	1.49%	13,365.79	2.42%	13,335.41	7.30%	30.38	0.01%	۲
Gov. Special Waste ^(b)	913.00	0.16%	8,175.31	1.48%	4,315.59	2.36%	3,859.72	1.04%	z
Gov. White Goods	529.00	%60.0	263.33	0.05%	263.33	0.14%	00.00	%00.0	z
Greenwaste Clean	49,209.00	8.41%	38,722.24	2.00%	38,722.14	21.21%	0.10	%00.0	۲
Greenwaste Mixed	1,289.00	0.22%	3,682.42	0.67%	0.00	%00.0	3,682.42	%66.0	۲
Metal	3,456.00	0.59%	1,088.75	0.20%	1,088.75	0.60%	00.00	0.00%	z
MSW	170,888.00	29.20%	276,631.65	50.00%	0.00	%00.0	276,631.65	74.63%	۲
Mixed Recycling	5,595.00	0.96%	608.68	0.11%	608.68	0.33%	00.0	%00.0	z
Garments Not for Recycle	2,943.00	0.50%	14,264.63	2.58%	0.00	%00.0	14,264.63	3.85%	z
Plastic Bottles	662.00	0.11%	71.89	0.01%	71.89	0.04%	00.00	0.00%	z
Newspaper	212.00	0.04%	55.86	0.01%	55.86	0.03%	00.00	%00.0	۲
Office Paper	2,504.00	0.43%	1,030.12	0.19%	1,009.18	0.55%	20.94	0.01%	۲
Recycle Garments	0.00	0.00%	0.00	%00.0	0.00	%00.0	00.00	0.00%	z
Rejected Garments	101.00	0.02%	158.55	0.03%	0.00	%00.0	158.55	0.04%	z
Resi. Batteries	49.00	0.01%	4.29	%00.0	4.29	%00.0	00.00	0.00%	z
Resi. Charged	17,315.00	2.96%	1,613.69	0.29%	0.00	%00.0	1,613.69	0.44%	۲
Resi. Free ^(c)	202,321.00	34.58%	23,583.41	4.26%	0.00	%00.0	23,583.41	6.36%	z
Resi, Metal	1,415.00	0.24%	3,604.52	0.65%	3,604.52	1.97%	00.00	0.00%	z
Resi. White Goods	1,352.91	0.23%	391.18	0.07%	280.55	0.15%	110.63	0.03%	z
Special Waste	2,860.00	0.49%	4,480.47	0.81%	61.90	0.03%	4,418.57	1.19%	z
Tip Floor MSW	0.00	0.00%	0.00	%00.0	0.00	%00.0	00.00	%00'0	۲
Tip Floor Waste	0.00	0.00%	0.00	%00.0	0.00	%00.0	00.0	%00.0	۲
Tires	5,569.00	0.95%	2,872.91	0.52%	2,839.25	1.55%	33.66	0.01%	z
White Goods	949.00	0.16%	274.50	0.05%	268.34	0.15%	6.16	%00.0	z
Total	585,164.91	100.00%	553,246.28	100.00%	182,588.54	100.00%	370,657.74	100.00%	
					Recycling Percentage	33.00%			
Annual Average	45,012.69		42,557.41		14,045.27		28,512.13		
Monthly Average	3,751.06		3,546.45		1,170.44		2,376.01		
Daily Average	146.15		138.17		45.60		92.57		

 Daily Average
 146.15
 92.57

 (a) Green waste is composed of organic waste that can be composted, i.e. refuse from gardens, grass clippings or leaves, and domestic or industrial kitchen wastes.
 92.57

 (b) Special waste is composed of industrial process waste, pollution control waste, or toxic waste, which may pose a threat to human health or the environment.
 (c) Waste that were not proposed.

Appendix B

Puerto Rico Dump Landfill Gas Sampling Results

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EA Engineering, Science, and Technology, Inc.

1001 Army Drive, Suite 103 Barrigada, Guam 96913-1402 Telephone: 671-646-5231 Fax: 671-646-5230

18 July 2011

James R. Stump CIP Contracting Officer Caller Box 10007 Saipan, MP 96950

RE: Puerto Rico Dump Landfill Gas Testing Method, Results and Recommendations

Dear Mr. Stump:

EA Engineering, Science, and Technology, Inc. is pleased to provide you with method, results and recommendations for Puerto Rico Dump (PRD) landfill gas (LFG) testing efforts that took place of the week of 13 June 2011.

Method:

Sixteen LFG sample probes were installed per the Tier II Testing Services for Puerto Rico Closure Work Plan. No unexploded ordinances (UXO) were encountered. Per USEPA Method 3C, samples may contain no more than 20% nitrogen. A total of five sample locations of sixteen met this requirement. Therefore, three additional sample probes were installed to obtain more samples meeting this criterion. None of the additional probes contained concentrations lower than 20% nitrogen see attached Location Map. Therefore, five samples are the basis of this LFG assessment. The presence of high nitrogen concentrations is indicative of air intrusion, which may be expected given the temporary and thin soil layer cover onsite.

Results:

Collected PRD LFG samples contain typical concentrations for methane, carbon dioxide, and nitrogen. However, non-methane organic compounds (NMOC) are lower than those typically observed in municipal landfills. PRD LFG testing results are summarized in Table 1 below.

	Sample Lo	cation			
Constituent (%, v/v)	LFG-05	LFG-06	LFG-11	LFG-12	LFG-15
Hydrogen (%, v/v)	ND	ND	ND	ND	ND
Argon (%, v/v)	3.42	3.22	1.28	2.94	2.39
Nitrogen (%, v/v)	12.1	11.5	5.78	10.4	12.4
Carbon Monoxide (%, v/v)	ND	ND	ND	ND	ND
Methane (%, v/v)	44.3	44.7	50.8	46.1	44.5
Carbon Dioxide (%, v/v)	40.2	40.6	42.1	40.6	40.7
Non-Methane Organic Compounds (ppmV)	11	8.9	22	20	19
ND=Compound was analyzed, but not detected abo	ve the laborat	ory reporting	limit.		

Table 1. Results of the PRD LFG testing services



1001 Army Drive, Suite 103 Barrigada, Guam 96913-1402 Telephone: 671-646-5231 Fax: 671-646-5230

EA Engineering, Science, and Technology, Inc.

Recommendations:

We recommend using this collected LFG data as a basis of design for future closed PRD uses. Original sample results are attached. No action with regard to LFG emissions is required. In particular, the threshold of applicability for the federal rule is as follows (40 CFR 60.33c): Only landfills with a permitted capacity over 2.5 million cubic meters are required to calculate NMOC, by either Tier 1 or Tier 2 methods; only when calculated NMOC exceed 50 megagrams per year is the site obligated to install an LFG emissions collection and control system. Given that the PRD is smaller than the federal threshold, at approximately 1.3 million cubic meters, and that observed NMOC are lower than typical concentrations, neither Tier I nor Tier II LandGEM analysis is required.

Please contact me at (671) 646-5231 or tword@eaest.com for questions or comments regarding this effort, or if additional information is required. Thanks so much for this opportunity and we look forward to continuing to work with you.

Sincerely,

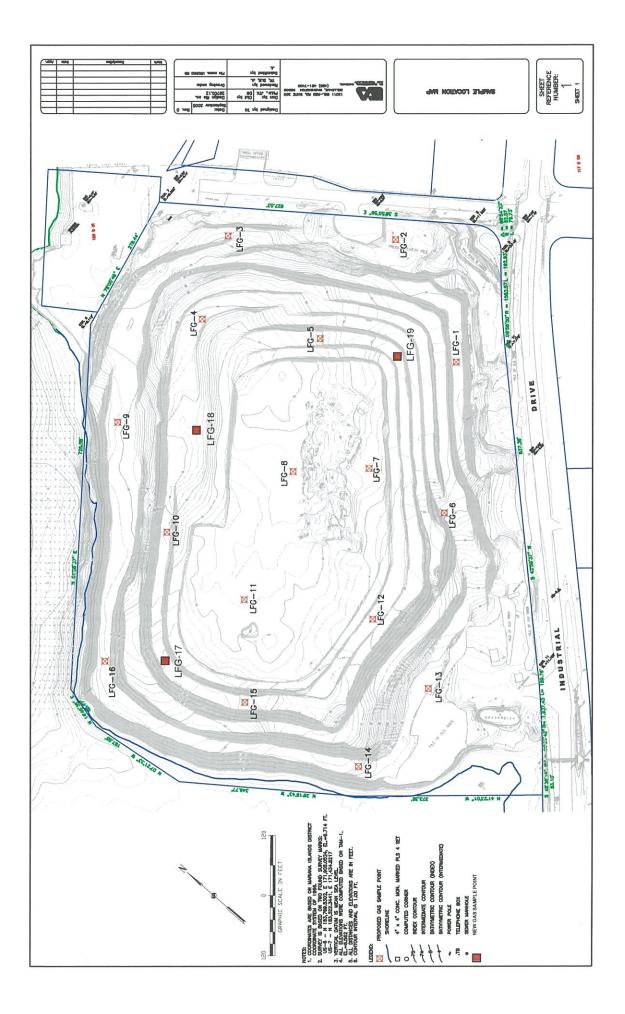
Tressie Word, PE Project Manager

Attachments:

PRD LFG Sample Location Map PRD LFG Sample Results

Cc:

Roy Reyes; Carl Castro (via email)





LABORATORY REPORT

July 12, 2011

Brenda Nuding EA Engineering, Science, and Technology 1221 Kapiolani Blvd. Suite 1030 Honolulu, HI 96814

RE: Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301

Dear Brenda:

Enclosed are the results of the samples submitted to our laboratory on June 27, 2011. For your reference, these analyses have been assigned our service request number P1102411.

All analyses were performed according to our laboratory's NELAP and DoD-ELAP-approved quality assurance program. The test results meet requirements of the current NELAP and DoD-ELAP standards, where applicable, and except as noted in the laboratory case narrative provided. For a specific list of NELAP and DoD-ELAP-accredited analytes, refer to the certifications section at www.caslab.com. Results are intended to be considered in their entirety and apply only to the samples analyzed and reported herein.

Columbia Analytical Services, Inc. is certified by the California Department of Health Services, NELAP Laboratory Certificate No. 02115CA; Arizona Department of Health Services, Certificate No. AZ0694; Florida Department of Health, NELAP Certification E871020; New Jersey Department of Environmental Protection, NELAP Laboratory Certification ID #CA009; New York State Department of Health, NELAP NY Lab ID No: 11221; Oregon Environmental Laboratory Accreditation Program, NELAP ID: CA20007; The American Industrial Hygiene Association, Laboratory #101661; United States Department of Defense Environmental Laboratory Accreditation Program (DoD-ELAP), Certificate No. L10-3-R1; Pennsylvania Registration No. 68-03307; TX Commission of Environmental Quality, NELAP ID T104704413-11-2; Minnesota Department of Health, NELAP Certificate No. 219474; Washington State Department of Ecology, ELAP Lab ID: C946. Each of the certifications listed above have an explicit Scope of Accreditation that applies to specific matrices/methods/analytes; therefore, please contact me for information corresponding to a particular certification.

If you have any questions, please call me at (805) 526-7161.

Respectfully submitted,

Columbia Analytical Services, Inc.

Sue Anderson Project Manager



2655 Park Center Drive, Suite A, Simi Valley, CA 93065 | 805.526.7161 | www.caslab.com

Client:EA Engineering, Science, and TechnologyCAS Project No:P1102411Project:Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301P1102411

CASE NARRATIVE

The samples were received intact under chain of custody on June 27, 2011 and were stored in accordance with the analytical method requirements. Please refer to the sample acceptance check form for additional information. The results reported herein are applicable only to the condition of the samples at the time of sample receipt.

Fixed Gases Analysis

The samples were analyzed for fixed gases (hydrogen, oxygen/argon, nitrogen, carbon monoxide, methane and carbon dioxide) according to EPA Method 3C (duplicate injection) using a gas chromatograph equipped with a thermal conductivity detector (TCD).

Total Gaseous Non-Methane Organics as Hexane Analysis

The samples were also analyzed for total gaseous non-methane organics as hexane according to EPA Method 25C. The analyses included a triplicate sample injection analyzed by gas chromatography using flame ionization detection/total combustion analysis.

The results of analyses are given in the attached laboratory report. All results are intended to be considered in their entirety, and Columbia Analytical Services, Inc. (CAS) is not responsible for utilization of less than the complete report.

Use of Columbia Analytical Services, Inc. (CAS) Name. Client shall not use CAS's name or trademark in any marketing or reporting materials, press releases or in any other manner ("Materials") whatsoever and shall not attribute to CAS any test result, tolerance or specification derived from CAS's data ("Attribution") without CAS's prior written consent, which may be withheld by CAS for any reason in its sole discretion. To request CAS's consent, Client shall provide copies of the proposed Materials or Attribution and describe in writing Client's proposed use of such Materials or Attribution. If CAS has not provided written approval of the Materials or Attribution within ten (10) days of receipt from Client, Client's request to use CAS's name or trademark in any Materials or Attribution shall be deemed denied. CAS may, in its discretion, reasonably charge Client for its time in reviewing Materials or Attribution requests. Client acknowledges and agrees that the unauthorized use of CAS's name or trademark may cause CAS to incur irreparable harm for which the recovery of money damages will be inadequate. Accordingly, Client acknowledges and agrees that a violation shall justify preliminary injunctive relief. For questions contact the laboratory.



			DE	ETAIL SUM	MARY REP	ORT						
Client:	EA Engineering	, Science,	and Techno	ology			Service Request: P1102411					
Project ID:	Landfill Gas Pu	erto Rico	Dump, (PRI	D) Saipan / 1	487301							
Date Received: Time Received:	6/27/2011 10:50								Fxd Gases Can 2X	TGNMO 3X Can		
			Date	Time	Container	Pi1	Pf1		1	L		
Client Sample ID	Lab Code	Matrix	Collected	Collected	ID	(psig)	(psig)		3C	25C		
LFG-00	P1102411-001	Air	6/20/2011	14:00	SC01065	-0.78	3.68		х	х		2
LFG-11	P1102411-002	Air	6/20/2011	15:46	SC00779	-0.22	3.80		х	х		
LFG-5	P1102411-003	Air	6/20/2011	16:16	SC00058	-0.45	3.55		Х	Х		
LFG-12	P1102411-004	Air	6/20/2011	16:51	SC00651	-0.41	3.85		х	х		
LFG-15	P1102411-005	Air	6/20/2011	17:20	SC00034	-0.61	3.70		Х	Х		
LFG-6	P1102411-006	Air	6/21/2011	10:43	SC00655	-0.58	4.27		х	х		

	Relinquished by: (Signature)	Tier I - Results (Default if not specified) Tier II (Results + QC Summaries)	Report Tier Levels - please select								0-0134		-16	151-17		151 11	Client Sample ID	bruding @ ecesti	1-808-256-8248 Email Address for Result Reporting	Brenda Nu	Project Manager	The try ine & numers (reporting intormation) 3 Washing in the Carter	Fax (805) 526-7270	2655 Park Center Drive, Suite A Simi Valley, California 93065
	huwww		-	ho'od	5.62	1.12	1.2		11.5	51.3-	0-0-6161	10 35 0-15	1-0.30 la	9/2018	20,14 6/	N0,66 61	Laboratory ID Number C	com/1	1-671-	Faxo	14 12550	normation) Le LTech		ž
	Date:	Tier III (R Tier IV (D							7		21/11/1043	20/11 1120	20/11 /651	120/11	11/02/	120/11	Date Time Collected Collected	tword cecrest.cum	646		0	1 Technology		Air- o
	11 Time: 150 10 21	Tier III (Results + QC & Calibration Summaries) Tier IV (Data Validation Package) 10% Surcharge						/	/		3 200655		1 500651		6 5060779		cted AC, SC, etc.)	oamp))	P.O. #/ Billing Information PO, # 9/6		Project Name Zy	Requested Tur 1 Day (100%) 2	Air - Chain of Custody Record & Analytical S
Nocencer by. (Signature		Summaries) % Surcharge									0400305	0400693	O A00353	S 0400270	0A00222	0400305	Flow Controller ID (Bar code # FC #)	bert Okon,		formation 9/60	1487301	ANDFILL GAS	Requested Turnaround Time in Business Days (Surcharges) please circle. 1 Day (100%) 2 Day (75%) 3 Day (50%) 4 Day (35%) 5 Day (25%) 10 Day-S	ly Record & A
(a)	perce										18	17	19	18	17	18	Canister Start Pressure "Hg	unski /				IP (PR)	ness Days (Surc %) 4 Day (35%)	nalytical Se
	E		Bo								1.0	2:0	1.0	10	1.5	0	Canister End Pressure "Hg/psig	un Olin	2			Saipan	5 Day (25%) 10 Day-Standard	ervice Request
Date:	Date:	EDD required								,	64 2	66 2	62 2	61 2	lot i	61 0	Sample Volume	E					Day-Standard	uest
Time:	h.	Yes / No					_		_		250 3	250 3	250 2	156 3	250 2	255 3						Analysis Method	CAS	Page
	O_1	Proj (MR									0	3 C	30	5 C	30	3C Q			The start insurance	845-1-1-1-1-1-1-1		ethod	S Project No.	
Cooler / Blank Temperature°C		Project Requirements (MRLs, QAPP)														Quote # 18532	9 8 1	specific instructions	e.g. Actual Preservative or	Commente		0	244	of



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Sample Acceptance Check Form

	Concerning of the second se	g, Science, and Techt	the second s			Work order:	P1102411			
	the second s	uerto Rico Dump, (PF	RD) Saipan / 1							
	(s) received on:				Date opened:		by:	MZAN		
Statement and Statement		amples received by CAS.			10 III III III III III III III III III I				cation of	
compliance	or nonconformity.	Thermal preservation and p	H will only be ev	aluated either at the	e request of the c	client and/or as require	ed by the method/	SOP. Yes	No	N/A
1	Were sample o	containers properly m	narked with cl	ient sample ID	?			X		
2	Container(s) su	upplied by CAS?						X		
3	Did sample co	ntainers arrive in goo	od condition?					\mathbf{X}		
4	Were chain-of	-custody papers used	and filled out	?				X		
5	Did sample co	ntainer labels and/or	tags agree w	ith custody pap	ers?			X		
6	Was sample ve	olume received adequ	ate for analys	is?				X		
7	Are samples w	ithin specified holdin	g times?					X		
8	Was proper ter	nperature (thermal p	reservation) of	of cooler at rec	eipt adhered	to?				X
	Co	oler Temperature		°C Blank T	emperature		°C			
9	Was a trip bla	nk received?							X	
10	Were custody	seals on outside of co	oler/Box?						X	
		Location of seal(s)?					Sealing Lid?			X
	Were signature	e and date included?								X
	Were seals inta	act?								X
	Were custody s	seals on outside of sam	nple containe	r?					X	
		Location of seal(s)?					Sealing Lid?			X
	Were signature	e and date included?								X
	Were seals inta	act?								X
11	Do containers	s have appropriate pr	eservation, ad	ccording to me	thod/SOP or	Client specified i	nformation?			X
	Is there a clier	nt indication that the s	ubmitted sam	ples are pH pr	eserved?					X
	Were VOA vi	als checked for present	nce/absence o	f air bubbles?						X
	Does the client	/method/SOP require	that the analy	st check the sa	mple pH and	l if necessary alte	er it?			X
12	Tubes:	Are the tubes cap	ped and intact	?						X
		Do they contain m	noisture?							X
13	Badges:	Are the badges pr	roperly cappe	d and intact?						X
		Are dual bed badg	ses separated a	and individuall	y capped and	intact?				X
Lab	Sample ID	Container	Required	Received	Adjusted	VOA Headspace	Receip	ot / Pres	ervation	

Container Description	Required pH *	Received pH	Adjusted pH	(Presence/Absence)	Receipt / Preservation Comments
6.0 L Source Can					
6.0 L Source Can					
6.0 L Source Can					
6.0 L Source Can					
6.0 L Source Can					
6.0 L Source Can					
		*			
	Description6.0 L Source Can6.0 L Source Can	DescriptionpH *6.0 L Source Can6.0 L Source Can	DescriptionpH *pH6.0 L Source Can	DescriptionpH *pHpH6.0 L Source Can6.0 L Source Can	DescriptionpH *pHpH(Presence/Absence)6.0 L Source Can </td

Explain any discrepancies: (include lab sample ID numbers):

Note: 13 of the 19 cans shipped were sent back not to be analyzed.

RSK - MEEPP, HCL (pH<2); RSK - CO2, (pH 5-8); Sulfur (pH>4)

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P1102411_EA Engineering, Science, and Technology_Landfill Gas Puerto Rico Dump, (PRD) Saipan_1487301.xls - Page 1 of 1 5 of 13



RESULTS OF ANALYSIS Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-00	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-001

Test Code:	EPA Method 3C	Date Collected: 6/2	20/11
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/27/11	
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/11	
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)
Test Notes:			
Container ID:	SC01065		

Canister Dilution Factor: 2.41

CAS #	Compound	Result	MRL	Data
-		%, v/v	%, v/v	Qualifier
1333-74-0	Hydrogen	ND	0.24	
7782-44-7	Oxygen +			
7440-37-1	Argon	2.87	0.24	
7727-37-9	Nitrogen	10.3	0.24	
630-08-0	Carbon Monoxide	ND	0.24	
74-82-8	Methane	45.5	0.24	
124-38-9	Carbon Dioxide	41.3	0.24	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



RESULTS OF ANALYSIS Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-11	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-002

Test Code:	EPA Method 3C	Date Collected: 6/20/11		
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/27/11		
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/11		
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)	
Test Notes:				
Container ID:	SC00779			

Canister Dilution Factor: 2.26

CAS #	Compound	Result %, v/v	MRL %, v/v	Data Qualifier
1333-74-0	Hydrogen	ND	0.23	
7782-44-7	Oxygen +			
7440-37-1	Argon	1.28	0.23	
7727-37-9	Nitrogen	5.78	0.23	
630-08-0	Carbon Monoxide	ND	0.23	
74-82-8	Methane	50.8	0.23	
124-38-9	Carbon Dioxide	42.1	0.23	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.

MRL = Method Reporting Limit - The minimum quantity of a target analyte that can be confidently determined by the referenced method.

3C_2X.XLT - Page No.:



RESULTS OF ANALYSIS Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-5	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-003

Test Code:	EPA Method 3C	Date Collected: 6/20	3/11
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/27/11	
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/11	
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)
Test Notes:			
Container ID:	SC00058		

Canister Dilution Factor: 2.30

CAS #	Compound	Result %, v/v	MRL %, v/v	Data Qualifier
1333-74-0	Hydrogen	ND	0.23	
7782-44-7	Oxygen +			
7440-37-1	Argon	3.42	0.23	
7727-37-9	Nitrogen	12.1	0.23	
630-08-0	Carbon Monoxide	ND	0.23	
74-82-8	Methane	44.3	0.23	
124-38-9	Carbon Dioxide	40.2	0.23	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



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RESULTS OF ANALYSIS

Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-12	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-004

Test Code:	EPA Method 3C	Date Collected: 6/2	20/11
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/2	27/11
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/3	0/11
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)
Test Notes:			
Container ID:	SC00651		

Canister Dilution Factor: 2.32

CAS #	Compound	Result %, v/v	MRL %, v/v	Data Qualifier
1333-74-0	Hydrogen	ND	0.23	Quuiniei
7782-44-7	Oxygen +			
7440-37-1	Argon	2.94	0.23	
7727-37-9	Nitrogen	10.4	0.23	
630-08-0	Carbon Monoxide	ND	0.23	
74-82-8	Methane	46.1	0.23	
124-38-9	Carbon Dioxide	40.6	0.23	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



RESULTS OF ANALYSIS

Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-15	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-005

Test Code:	EPA Method 3C	Date Collected: 6/20/11	
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/27/11	
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/11	
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed: 0.10 ml(s)	
Test Notes:			
Container ID:	SC00034		

Canister Dilution Factor: 2.36

CAS #	Compound	Result %, v/v	MRL %, v/v	Data Qualifier
1333-74-0	Hydrogen	ND	0.24	Quanner
7782-44-7	Oxygen +	,		
7440-37-1	Argon	2.39	0.24	
7727-37-9	Nitrogen	12.4	0.24	
630-08-0	Carbon Monoxide	ND	0.24	
74-82-8	Methane	44.5	0.24	
124-38-9	Carbon Dioxide	40.7	0.24	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



RESULTS OF ANALYSIS

Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	LFG-6	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P1102411-006

Test Code:	EPA Method 3C	Date Collected: 6/21	1/11
Instrument ID:	HP5890 II/GC1/TCD	Date Received: 6/27	7/11
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/11	
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)
Test Notes:			

Container ID: SC00655

Canister Dilution Factor: 2.43

CAS #	Compound	Result %, v/v	MRL %, v/v	Data Qualifier
1333-74-0	Hydrogen	ND	0.24	
7782-44-7	Oxygen +			
7440-37-1	Argon	3.22	0.24	
7727-37-9	Nitrogen	11.5	0.24	
630-08-0	Carbon Monoxide	ND	0.24	
74-82-8	Methane	44.7	0.24	
124-38-9	Carbon Dioxide	40.6	0.24	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



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RESULTS OF ANALYSIS

Page 1 of 1

Client:	EA Engineering, Science, and Technology	
Client Sample ID:	Method Blank	CAS Project ID: P1102411
Client Project ID:	Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301	CAS Sample ID: P110630-MB

Test Code:	EPA Method 3C	Date Collected: NA	
Instrument ID:	HP5890 II/GC1/TCD	Date Received: NA	
Analyst:	Dante Munoz-Castaneda	Date Analyzed: 6/30/	11
Sampling Media:	6.0 L Summa Canister	Volume(s) Analyzed:	0.10 ml(s)
Test Notes:			

CAS #	Compound	Result	MRL	Data
	100	%, v/v	%, v/v	Qualifier
1333-74-0	Hydrogen	ND	0.10	
7782-44-7	Oxygen +			
7440-37-1	Argon	ND	0.10	
7727-37-9	Nitrogen	ND	0.10	
630-08-0	Carbon Monoxide	ND	0.10	
74-82-8	Methane	ND	0.10	
124-38-9	Carbon Dioxide	ND	0.10	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.



RESULTS OF ANALYSIS Page 1 of 1

Client: EA Engineering, Science, and Technology Client Project ID: Landfill Gas Puerto Rico Dump, (PRD) Saipan / 1487301

CAS Project ID: P1102411

Total Gaseous Nonmethane Organics (TGNMO) as Hexane

Test Code:	EPA Method 25C	
Instrument ID:	HP5890 II/GC1/FID/TCA	Date(s) Collected: 6/20 - 6/21/11
Analyst:	Dante Munoz-Castaneda	Date Received: 6/27/11
Sampling Media:	6.0 L Summa Canister(s)	Date Analyzed: 6/29 - 6/30/11
Test Notes:		

Client Sample ID	CAS Sample ID	Canister Dilution Factor	Injection Volume ml(s)	Result ppmV	MRL! ppmV	Data Qualifier
LFG-00	P1102411-001	2.41	0.50	11	0.41	
LFG-11	P1102411-002	2.26	0.50	22	0.38	
LFG-5	P1102411-003	2.30	0.50	11	0.39	
LFG-12	P1102411-004	2.32	0.50	20	0.39	
LFG-15	P1102411-005	2.36	0.50	19	0.40	
LFG-6	P1102411-006	2.43	0.50	8.9	0.41	
Method Blank	P110629-MB	1.00	0.50	ND	0.17	
Method Blank	P110630-MB	1.00	0.50	ND	0.17	

ND = Compound was analyzed for, but not detected above the laboratory reporting limit.

MRL = Method Reporting Limit - The minimum quantity of a target analyte that can be confidently determined by the referenced method. ! = For consistency purposes, the actual MRL was divided by six and reported as Hexane.

Appendix C

Marpi Solid Waste Facility Landfill Gas Sampling Results

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September 5, 2018



LA Cert #04140 EPA Methods T03, T014A, T015, 25C/3C, RSK-175

> TX Cert T104704450-14-6 EPA Methods T014A, T015

UT Cert CA0133332015-3 EPA Methods TO3, TO14A, TO15, RSK-175

EA Engineering, Science & Technology ATTN: Jason Jaskowiak 1001 Army Dr., Suite 103 Barrigada, Guam 96913

LABORATORY TEST RESULTS

Project Reference: CNMI Landfill Gas Feasability Study; G330601 Lab Number: J082009-01/05

Enclosed are results for sample(s) received 8/20/18 by Air Technology Laboratories. Samples were received intact. Analyses were performed according to specifications on the chain of custody provided with the sample(s).

Report Narrative:

- Samples were received outside the laboratory-established 30-day holding time due to a USPS shipping error. Analyses were performed with client approval.
- Unless otherwise noted in the report, sample analyses were performed within method performance criteria and meet all requirements of the TNI Standards.
- The enclosed results relate only to the sample(s).

Preliminary results were e-mailed to Jason Jaskowiak on 9/04/18.

ATL appreciates the opportunity to provide testing services to your company. If you have any questions regarding these results, please call me at (626) 964-4032.

Sincerely,

Mark Johnson Operations Manager MJohnson@AirTechLabs.com

Note: The cover letter is an integral part of this analytical report.

			- Contraction		CHAIN OF	: CUSTODY		RECORD		
AITEC	TECHNOLOGY	18501 E. Gale Ave., Suite 130 City of Industry CA 91748	TURI	TURNAROUND TIME			ABLES	PAGE:	1 OF	1
A V V Labe	Laboratories, Inc.	Ph: 626-964-4032	Standard] 48 h	48 hours	EDD		Condition u	Condition upon receipt:	
	, in the second se	Fx: 626-964-5832	Same Day]. 72 H	72 hours	EDF			Sealed Yes	□ °N
Project No.: 63306	0001		24 hours] 96 F	96 hours	LEVEL 3			Intact Yes	No
Project Name: CNMI	LANDFILL GAS FEASABILITY	sinty Sturdy	Other: 10 -	-DAY	v	LEVEL 4			Chilled	deg C
Report To: JASCAN	JASKOWIAK			BILLING	-		AN	ALYSIS	ANALYSIS REQUEST	
Company: CA EA	ENGINEEDING, SA., & TA	TECH., PSC	P.O. No.: /	18034				~		
1001	ARMY DRIVE, SUITE 10	201	Bill to: JA	AU NOS	TASON JASKOUIAK		yani té terreter		0	
ate/Zip: 8	ARRIGEDA, GUAN 96	96913	700/ AR	ARMY DRIVE	VE					
	671-646-5231		STE 103			25		75		
	JJASKOWIAK @ EAEST. COM	W	BARRIGADA	A GUAN	96913	20		E (013	
LAB USE ONLY	SAMPLE IDENTIFI	DENTIFICATION	SAMPLE TAD	SAMPLE	ХІЯТАМ ЯЗИІАТИОС ЗЯҮТ	Jo#49W	JOWN	METHOS	HU , JO	
J082407-01	MARPI-15- 071018	018	0 31/0/to	WH IOLO	LFG 9	×	×	8	8	
70- 1, 1	140-45-192AM	0710180	31/01/FD	1203 AIR	Lf 6 SUMMA	×	×	8	×	
\$ ¹	MARPI-3A-071018	1018	CA/10/18	24C NO		×	×	×	×	K
do -	MARD - 44 - 071018	glot	et/10/18	an h2E	LEG SUMMA	×	×	×	×	
5	MARPI-58-0	Slotto	21/01/to	417 22H	LEG SUMA	X	×	×	XX	
/										
/		C .	Ì						the second	
/		\times							-	
										/
AUTHORIZATION TO PERFORM WORK	SCOULAR COMPANY	140	DATE/TIME 103	70/ CO	COMMENTS					
SAMPLED BY TIMOTHY CHARGUNIDS	C GHILLS COMPANY	Professo	DATE/TIME							
RELINQUISHED BY		HVF St	DATE/TIME	£						
RELINQUISHED BY MSPS	DATE/TIME	RECEIVED BY	DATE/TIME /9	AR A						
RELINQUISHED BY	DATE/TIME	-	re/Time	2						
METHOD OF TRANSPORT (circle one): Walk-In	(circle one): Walk-In FedEx	Ex UPS Courier ATLI Other	ler	-						
DISTRIBUTION: White & Ye	DISTRIBUTION: White & Yellow - Lab Copies / Pink - Customer Copy	omer Copy	Preservation: H=HCL N=None / Container: B=Bag C=Can V=VOA 0=Other	HCL N=	Vone / Contai	ner: B=Bag	C=Can	V=VOA		Rev. 03 - 5/7/09

Client:	EA Engineering
Attn:	Jason Jaskowiak
Project Name:	CNMI Landfill Gas Feasability Study
Project No.:	G330601
Date Received:	8/20/2018
Matrix:	Air

TNMOC by EPA METHOD 25C Fixed Gases by EPA METHOD 3C

	Lab No.:	J0820	09-01	J0820	09-02	J0820	09-03	J0820	09-04	
Client	Sample I.D.:	MARF 0710		MARF 0710		MARF 0710		MARF 0710		
Date/Ti	me Sampled:	7/10/18	8 9:01	7/10/18	12:03	7/10/18	12:46	7/10/18	13:24	
Date/Tin	ne Analyzed:	8/23/18	22:33	8/24/18	23:32	8/24/18	8 0:30	8/24/18	8 1:28	
QC Batch No.:		180823GC8A1		180823GC8A1		1808230	GC8A1	1808230	GC8A1	
Ana	lyst Initials:	A	AS		AS		AS		AS	
Dilu	tion Factor:	3.2		3.	0	3.2		3.2		
ANALYTE	(Units)	Result	RL	Result	RL	Result	RL	Result	RL	
TNMOC N2 corrected	(ppmv-C)	1,400	32	1,300	30	850	32	1,600	32	
TNMOC O2 corrected	(ppmv-C)	1,400	32	1,400	30	890	32	1,600	32	
TNMOC uncorrected	(ppmv-C)	1,300	32	660	30	440	32	1,500	32	
Nitrogen	(% v/v)	ND	3.2	37	3.0	35	3.2	ND	3.2	
Oxygen	(% v/v)	ND	1.6	10	1.5	10	1.6	ND	1.6	
Carbon Dioxide	(% v/v)	44	0.032	25	0.030	25	0.032	42	0.032	
Methane	(% v/v)	61	0.0032	36	0.0030	36	0.0032	59	0.0032	

RL = Reporting Limit

ND = Not detected at or above the RL.

TNMOC = Total Non-Methane Organic Compounds

ppmv-C = parts per million by volume as carbon

TNMOC N2 corrected (applicable if N2 < 20%)

TNMOC O2 corrected (applicable if N2 > 20% and O2 < 5%)

TNMOC uncorrected = not corrected for N2, O2 or moisture

NA = Nitrogen/oxygen/moisture correction causes division by zero.

Reviewed/Approved By:

Date 9/4/12

Mark Johnson Operations Manager

The cover letter is an integral part of this analytical report



- AITTECHNOLOGY Laboratories, Inc. -

J082009

18501 E. Gale Avenue, Suite 130 • City of Industry, CA 91748 • Ph: (626) 964-4032 • Fx: (626) 964-5832

Client:	EA Engineering
Attn:	Jason Jaskowiak
Project Name:	CNMI Landfill Gas Feasability Study
Project No.:	G330601
Date Received:	8/20/2018
Matrix:	Air

TNMOC by EPA METHOD 25C Fixed Gases by EPA METHOD 3C										
	Lab No.:	J08200)9-05			I				
Client Sample I.D.:		MARP 0710								
Date/Time Sampled:		7/10/18 14:22								
	e Analyzed:	8/24/18 2:27								
QC	Batch No.:	1808230	GC8A1	-						
Ana	lyst Initials:	AS	5							
Dilu	tion Factor:	3.()			<u> </u>		L		
ANALYTE	(Units)	Result	RL							
TNMOC N2 corrected	(ppmv-C)	1,400	30							
TNMOC O2 corrected	(ppmv-C)	1,400	30							
TNMOC uncorrected	(ppmv-C)	1,300	30							
Nitrogen	(% v/v)	5.9	3.0	-						
Oxygen	(% v/v)	1.6	1.5							
Carbon Dioxide	(% v/v)	39	0.030							
Methane	(% v/v)	61	0.0030							

RL = Reporting Limit

ND = Not detected at or above the RL.

TNMOC = Total Non-Methane Organic Compounds

ppmv-C = parts per million by volume as carbon

TNMOC N2 corrected (applicable if N2 < 20%)

TNMOC O2 corrected (applicable if N2 > 20% and O2 < 5%)

TNMOC uncorrected = not corrected for N2, O2 or moisture

NA = Nitrogen/oxygen/moisture correction causes division by zero.

Reviewed/Approved By:

Mark Johnson

Date 9/4/12

Operations Manager

The cover letter is an integral part of this analytical report

AirTECHNOLOGY Laboratories, Inc. -

71

Site: 5A Refusal @ 0.5' Site: 1A Refusal @ 1.5' Site: 1B SampleID: Marpi-1B-071018 Sample Date: 07/10/18 Location: 15.2723 N, 145.8168 E

Ν

Site: 5B SampleID: Marpi-5B-071018 Sample Date: 07/10/18 Location: 15.2721 N, 145.8165 E

Site: 2A Sample ID: Marpi-2A-071018 Sample Date:07/10/18 Location: 15.2719 N, 145.8164 E

Site: 3A SampleID: Marpi-3A-071018 Sample Date:07/10/18 Location: 15.2716 N, 145.8165 E Site: 4A SampleID: Marpi-4A-071018 Sample Date:07/10/18 Location: 15.2718 N, 145.8166 E

Legend

- Top of Cell 1
- Landfill Gas Sample Points

125	62.5	0	125 Feet



GC Raw Data Index General Information

Method: EPA 25C/3C

Lab Project No.: J082009

	Section	Page #
1.	Supporting Documents	6
2.	Sample Raw Data	17
3.	Initial Calibration	80
4.	Initial Calibration Verification	88
5.	Continuing Calibration	96
6.	Method Blank	121
7.	LCS/LCSD	na

Conventions and Conversions

1 ppbv = 0.001 ppmv = 0.0000001% v/v 1% v/v = 10,000 ppmv = 10,000,000 ppbv

 $1 \text{ ug/m}^3 = 1 \text{ ng/L} = \text{ppbv x MW/24.45}$ $1 \text{ ug/L} = 1 \text{ mg/m}^3 = \text{ppmv x MW/24.45}$

Where **MW** is the molecular weight of the compound and 24.45 is the molar volume of ideal gas at 1 atmosphere and 25° C.

> 1 atmosphere = 14.6 psia = 0 psig 30" Hg = 0 psia = -14.6 psig

Standard pressure is taken as 14.6 psia at Air Technology Labs' facility.

Form-15 Rev. 2 \VAIRTECH-SERVER\Shared Folders\Company\QA\Forms\GC Raw Data Pkg Dividers Rev2.doc QA Manager 10/2016

1. Supporting Documents

- a. Pressurization log (if applicable)
- b. ICAL run log
- c. CCAL/QC/Samples run log
- d. Miscellaneous documents

PRESSURIZATION LOGBOOK

))	Date	Sample ID	Can #	Initial Pressure	Final Pressure	Dilution Gas	Dilution Gas Lot #	Initials	ETR #	Client/ Comments	He Prefill
)) 1	8/21/13	J082105-01	3129	6"47	lopsig	He	165119188	Hog	8895	WEAVER	YES
2		-02		614	4	1	4	1	1	1	1
) 3	3/21/13	J882009-01	3143	S"U	BASIA	He	165113133	Am	8849	EANG	KT
4	<u> </u>	-02	1473	4"4							
5		-63	5435	5"4							
6		-04	5481	5"14							
) 7	1	1 -05	1468	4"H	-		1			1	4
8				,							
9											
10											
) 11											
112											
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15											
) 16											
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120	•										
1/21											
122											
23											
24			b								
25											
26											
27		N									
28											

Approved by/Date:_____

Air Technology Laboratories Inc.

Logbook #17

<u>AS</u> 071.592889	QC Batch	16071161341																			7
Chemist: Blank Lot #: <u>(</u>	Comments	FILS ICCY. NIMOC					7	FID ICCUL hinneoc						•							
	Status	2					_>	ch-					-;	ol				7	ck	<	-7
ook	Line #	_	R	3	4	5	0		2	3	4	- V.	0	0	8	0	10	đ	2	14	$\overline{\mathbf{X}}$
dgo-	ЦЦ	1-G			•																
GC Injection Logbook ک	Sample dilution	(_																		→
ic Inje	Press. Dilution	1										·	•								
	Sample Volume	STUCEP	ادمااد																2		
<u>veci_16071</u>	Client/ Std Code	0-00-12 111/12/0710	11/2110 21/21	·) Austrucci	() AWARDOG	(C),(C) AWRING	NSOH34	11 CA12/MV	OKULLIN	Awizierce	801.912114	ענייות ובירטר	ASCIU34	AWIZIUTIZ	SILAIZINS	MUZ 1102/	nsold 807	80%/n1054	1.5/1/2. 2001216/1	Div171671	2 NW12167
GC 8A	Lab Number/ Standard Type	D. March 2 CHARGIO	DRA U. (D) 5/0 (1 +41 () + () Hurane zik	O19, CHURDIN	7. 1 9.CHui/0, (()	P_S/CHAILUNCO	Hurlin (O)	1), (20017, CI-HUCUSIC AW 211071	(), (0) 1% (Hi/0)(0) AWININA	202 Or OI -6C.Hullop (6 Amirican	202 10, 14, C141 C0, 10 ANVENDOR	O'S' CHUILONCO NUMBER	1.0% CH4(CO, 10) ASC	Mo STACHUCOS	207 25% CHUCO	SOG CHUCU	100% 000	100%0144	5		194.412 1140029924/02/AW12167
GC 8A MMOCENER 10011 (1061)	Data File	CP In (0331	1	03510	10201	11/1	1114 001 C	00210	CORIC	1 1204 10	Das	0010	1 000	008	000	010	1101	1 012	103
	Time	020	1795	1/1/10	104	1119	1123	1152	2161	1929.	1251	11/21	12.20	1959	Uhll,	1426	1 h h l	ILSG	1S18	1523	134D
ତ୍ତି ଆଜାନା ID: Mitical Method: afile Directory:	Date	11/10																			

Page 67 of 202 GC8A Logbook #38

Air Technology Laboratories, Inc.

Approved by/Date:

		r					-				1	<u> </u>			r				 ĺ
. AS 071593139	QC Batch	160011GGAN								;									
Chemist: Blank Lot #,	Comments					incora stri NR	- - -												
ų.	Status	K				de		0	4	20									
ook	Line S #	2	=	ļ	2	8	57	6	<i>c</i> .	Q.									
odpo.	DF	0.								}								•	
GC Injection Logbook	Sample dilution	1		_												•			
C Inje	Press. Dilution	1											•						
00	Sample Volume	C1254																-	
1001-1000	Client/ Std Code	118	ALL -	PILAISIUM	110010357	02601211-112	Į.,	Asoluson	12081480c	1084121010									
190 8A 10111 (1001) MM2200/2002	Lab Number/ Standard Type	10% Hz	715 92400, 78% Nr	2.5% Ha	100% Nº	icu.	· 100	Commun (numer)	ICU TCD number here	IN FIDGRAMMECC AUTLIESOI									
0102/18/2018	Data File	112101011	UKS	910	017	018	100	122 121 CGA		1700 00 3 1 (N)									
): ≥thod: story:	Time	1600	(12)	1631	1646	1700	SICI	1122	1:28	8	Ţ								
ରୁ ଆୁମ୍ବାପୋ ID: ଅନୁମ୍ବାରେ Method: tafile Directory:	Date	(1116	-				;	12/16											

Pade 68 of 202 GC8A Logbook #38

Air Technology Laboratories, Inc.

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6 Approved by/Date:____

		41		1]]]]									38	Page 127 of 202	
Chemist: <u> </u>	QC Batch	1603121608/11	*1																			->	GC8A Logbook #38	Page 1	
Chemist: <u> </u>	Comments .	ceirlo NR		· ·	•			•		y -oz-kéw.netgan!	\sim	ine	ЧR	JPC .	JR			UR.				•			
gbook	F Line Status	0 10 0k.		2	14 1	is or	16 ck		JULION	742/11 ok	0 1 0 N	1. No 1	4 ck N	3 ck	· 110 01	->	16 ck	\$ 4. F	74310 OK	.0 3 ok		↑ _↑	lnc.		
GC Injection Logbook	Sample DF dilution	- 1.						5 3.15d	30													;	Air Technology Laboratories, Inc.		,
GC In	Sample Press. Volume Dilution	Cop 1						Sel		>	!								200 1051	۱ 		7	Air Technold		
·	Client/ Sa Std Code Vo	PENTICH FEBCE				TA	PEC	I muer		TA)	AWIZITICA.	PULLISHOP	givitatiole	(1	SILICIAN	えりったりっしいろ	L D L	DUITITICI	.LOILIZMA	I			
GC 8A ECILIBOTII OLDN AUG	Lab Number/ Standard Type	H061003-02	1 -02	MO-	20-	H081102-01	Hrande-Oi	10-2011201	CO- 1	H081201-01	(J2N2 CCU)	Oil s/CHUCOP(C) AWARDED		0.14/ (Hu/0,00	blank	Hank .	1% N2 LOQ		1202120-1)(),1%(141(Cl)n(())	CHU	OZN2 CC			
Gran 1201	Data File	13.0100/JA	2013	10	510	010	LIO:	018	blO	CNO	170	. 003	200	heo			Can	MAS 128			20	750. 1		ate:	
Monent ID: Material Method:	hate Time	3/16/11/14	11/28	2111	2101	12201	13 UG	1253	1312	1228	1251	6111.	1426	11111	9211	CISIO	153X	155	11008	11022	(59)	1 1452		0 Approved by/Date: 	125

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s Xs		QC Batch	18062761841																			
Chemist:	Blank Lot #	Comments	Ne			leaf .				file end	I ral.		P				1 nal/			IND& /		
	-	Status	K			5	<u>.</u> .		6.		or			ok						ol.		
ook		Line #			,	. 4			C				~							4		
Logb		DF	1.0																			
GC Injection Logbook		Sample dilution	ì																			
C Inje		Press. Dilution)																			
Ċ		Sample Volume	Std Loop																			
	0	Client/ Std Code	POSSOCIUM		- 0	AWIJOSSOG		1	AW1308802	-				RWIJCESEDS					-7	AWI308801		1
GC 8A	12018 / Jun	Lab Number/ Standard Type	5	-		30PPMV NUNOC		4 -	30(1) pam nucc			n		30 PAMU MIKC						999999999911 MMOC AWISCS801		>
0	nmochixed GC8A \2C	Data File	Mun 2011	0	00	014	OK	010	CID	018	019	030	Cal	2	C.9.3	Cay	CBS	Cab	60	035 99	039	1 030
i i		Time	11382	I.S.S.	207	1333	1236	1351	1305 I	1320	346	00h	1415	1432	Uh/1	ISSI	16 Clo	1621	SEPI	1050	inoui	1919
Instrument ID: J082009	Analytical Method: Datafile Directory:	Date	6 37 18	-																	-	

GC8A Logbook #44 Para 40 nf 200

Air Technology Laboratories, Inc.

Approved by/Date:

Batrument 1D:

GC 8A

GC Injection Logbook

Chemist: AS

1 - 1	· · · · · ·				 		 	 	 		 	 	 	-	-
Blank Lot #: Old 10800	QC Batch	1.411/0.11.1.841	11/07/01/00/01												
· Blank Lot #	Comments	101													
	Status	de													
	Line #	5													1
	DF	1.0		÷											
	Sample dilution	,													
	Press. Dilution	1				·.									
	Sample Volume	Stel													
	Client/ Std Code	PSC lugog													
180087 181 Jun	Lab Number/ Standard Type	3002Pmv nimoc													
000001/1001 - 1801027	Data File	1734 27 Jun 031	5							2.0					
	Time	1734													
Analytical Method: Datafile Directory:	Date	811160													

Page 43 of 202 GC8A Logbook #44

Air Technology Laboratories, Inc.

Approved by/Date:_

Chemist: AS	Blank Lot #: 610802	Comments QC Batch	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	180823GC8A1	Page of 200
lbook		Line Status	2-1 ok	2-2	2-3	2-4	2-4	2-4	2-5 de	2-5	2-6 NG 9/E	2-6 ch	2-7 OL :	2-8 dc	13 2-9 cL	73 2-10	73 2-11	i9 2-12 4	4, 0k	4,	4, 4	4,	
GC Injection Logbook		Sample DF dilution	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 1	None 2.973	None 2.973	None 2.973	None 3.159	None 1	None 1	None 1	None 1	ories, Inc.
SC Inje		Press. Dilution	None	None	None	None	None	None	None	None	None	None	None	None	see log	Air Technology Laboratories, Inc. GC 8A Log# 45							
0		Sample Volume	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Std Loop	Air Techno G
	18\Aug	Client/ Std Code	1	AW1309720	AW1309718	AS014909	AS014909	AS014909	AS014809	AS014809	ı	1	HALL	TA	FOTH	FOTH	FOTH	FOTH	scs	SCS	SCS	scs	
GC 8A	nmoc fixed_180627 WAIRTECH-SERVER/InsData\GC8A\2018\Aug	Lab Number/ Standard Type	02_N2_CCV	0.1%_CH4_CO2_CO	25%_CH4_CO2_7%_H2_AW1309718	300_PPMV_NMOC	300_PPMV_NMOC	300_PPMV_NMOC	R	LCSD	Method Blank	Method Blank	J082302-01	J082301-01	1082007-01	J082007-02	J082007-03	J082007-04	J082002-03	J082002-03	J082002-03	1082002-03	
	nmoc fixed_180627 \VAIRTECH-SERVE	Data File	13:47 ug\23aug	14:02 23aug001	14:17 23aug002	14:31 23aug003	14:46 23aug004	15:00 23aug005	15:15 23aug006	15:29 23aug007	15:44 23aug008	15:58 23aug009	16:13 23aug010	16:28 23aug011	16:42 23aug012	16:57 23aug013	17:11 23aug014	17:26 23aug015	17:41 23aug016	17:55 23aug017	18:10 23aug018	18:24 23aug019	
Ö	Method: rectory:	Time					-																Approved by/Date
Instrument ID:	Analytical Method: Datafile Directory:	Date	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	08/23/18	Approve
			r-1	2	3	4	S	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	

GC 8A Log# 45

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J082009

GC 8A

Instrument ID:

GC Injection Logbook

Chemist: AS

	Analytical Method:	ethod:	nmoc fixed 180627	1627								Blank Lot #:	#; 610802
-	Datafile Directory:	ctory:	WAIRTECH-SEF	NAIRTECH-SERVER/InsData/GC8A/2018/Aug	018\Aug								
	Date	Time	Data File	Lab Number/ Standard Type	Client/ Std Code	Sample Volume	Press. Dilution	Sample dilution	DF	Line #	Status	Comments	QC Batch
н Н	08/23/18	18:39	18:39 23aug020	J082002-04	scs	Std Loop	See Log	None	Ч	5,	20	RSD>S (Held)	180823GC8A1
7	08/23/18	18:54	18:54 23aug021	J082002-04	scs	Std Loop	See Log	None	H	5,			180823GC8A1
m	08/23/18	19:08	19:08 23aug022	J082002-04	scs	Std Loop	See Log	None	Ч	5,			180823GC8A1
4	08/23/18	19:23	19:23 23aug023	J082002-04	scs	Std Loop	See Log	None	1	5,			180823GC8A1
ы	08/23/18	19:38	19:38 23aug024	J082002-12	. SCS	Std Loop	See Log	None	1	13,	ok		180823GC8A1
0	08/23/18	19:52	19:52 23aug025	J082002-12	SCS	Std Loop	See Log	None	1	13,			180823GC8A1
~	08/23/18	20:07	20:07 23aug026	J082002-12	scs	Std Loop	See Log	None	1	13,			180823GC8A1
00	08/23/18	20:21	20:21 23aug027	J082002-12	scs	Std Loop	See Log	None	۲,	13,			180823GC8A1
ŋ	08/23/18	20:36	20:36 23aug028	J082002-13	scs	Std Loop	See Log	None	ц.	14,			180823GC8A1
10	08/23/18	20:51	20:51 23aug029	J082002-13	scs	Std Loop	See Log	None	Ч	14,			180823GC8A1
11	08/23/18	21:05	21:05 23aug030	J082002-13	scs	Std Loop	See Log	None	1	14,	_		180823GC8A1
12	08/23/18	21:20	21:20 23aug031	J082002-13	scs	Std Loop	See Log	None	Ч	14,			180823GC8A1
13	08/23/18	21:35	21:35 23aug032	J082002-14	scs	Std Loop	See Log	None	7	15,	No	RSD 25	180823GC8A1
14	08/23/18	21:49	21:49 23aug033	J082002-14	scs	Std Loop	See Log	None	t.	15,			180823GC8A1
15	08/23/18	22:04	22:04 23aug034	J082002-14	scs	Std Loop	See Log	None	1	15, .			180823GC8A1
16	08/23/18	22:19	22:19 23aug035	J082002-14	scs	Std Loop	See Log	None	1	15,			180823GC8A1
17	08/23/18	22:33	22:33 23aug036	1082009-01	EA	Std Loop	See Log	None	1	7,	or		180823GC8A1
18	08/23/18	22:48	22:48 23aug037	1082009-01	EA	Std Loop	See Log	None	H	7,			180823GC8A1
19	08/23/18	23:02	23:02 23aug038	1082009-01	EA	Std Loop	See Log	None	1	7,			180823GC8A1
20	08/23/18	23:17	23:17 23aug039	1082009-01	EA	Std Loop	See Log	None	-	7,			180823GC8A1
	Approved by/Date	by/Date		I		Air Technology Laboratories, Inc.	ology Laborat	itories, Inc.					Page of 200

nology Laboratories, Inc. GC 8A Log# 45

Chemist: AS

GC Injection Logbook

610802

nmoc fixed 180627

GC 8A

nstrument ID:

Date

2 3 4

8/24/18 QC Batch 180823GC8A1 R Blank Lot #: Comments Status 3 Line # 10, 10, 10, 11, 11, 11, 10, 11, ŝ ŝ ŝ ŝ s) 6 6 é, Ц 1 Ч -Ч L, 1 H -1 1 H 1 --1 T -Sample None See Log Press. Dilution See Log Std Loop Sample Volume Std Loop Client/ Std Code NAIRTECH-SERVER/InsData/GC8A/2018/Aug EA EA EA A EA Lab Number/ Standard Type J082009-03 1082009-05 J082009-05 1082009-03 J082009-04 J082009-04 J082009-04 J082009-05 J082009-05 J082009-02 1082009-02 1082009-02 1082009-03 J082009-03 1082009-04 J082009-02 Data File 0:59 23aug046 23aug055 0:45 23aug045 1:28 23aug048 1:43 23aug049 2:27 23aug052 23aug040 23:46 23aug041 23aug042 0:15 23aug043 0:30 23aug044 1:14 23aug047 23aug050 23aug051 2:41 23aug053 2:56 23aug054 1:58 2:12 3:11 23:32 0:01 Time Analytical Method: Datafile Directory: 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18 08/23/18 08/23/18 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18 08/24/18

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of 200

Page _____

Air Technology Laboratories, Inc. GC 8A Log# 45

Approved by/Date

-	Instrument ID:	ö		GC 8A		G	C Inje	GC Injection Logbook	dgo-	ook		Chemist: AS	: AS
A	Analytical Method:		nmoc fixed_180	nmoc fixed_180627, nmneoc fixed_160711bu	11bu							Blank Lot #:	610802
LL ,	Datafile Directory:	ctory:	WAIRTECH-SER	WAIRTECH-SERVERIInsData\GC8A\2018	A2018VAug								
	Date	Time	Data File	Lab Number/ Standard Type	Client/ Std Code	Sample Volume	Press. Dilution	Sample dilution	Ъ	Line #	Status	Comments	QC Batch
Ч	08/24/18	3:25	3:25 23aug056	02_N2_CCV	1	Std Loop	None	None	1	2-1	üle		180824GC8A1
7	08/24/18	3:40	3:40 23aug057	0.1%_CH4_CO2_CO	AW1309720	Std Loop	None	None	Ч	2-2			180824GC8A1
m	08/24/18	3:55	3:55 23aug058	25%_CH4_CO2_7%_H2	AW1309718	Std Loop	None	None	ч	2-3			180824GC8A1
4	08/24/18	4:09	4:09 23aug059	300_PPMV_NMOC	AS014909	Std Loop	None	None	н	2-4			180824GC8A1
5 N	08/24/18	4:24	4:24 23aug060	300_PPMV_NMOC	AS014909	Std Loop	None	None	H	2-4			180824GC8A1
9	08/24/18	4:38	4:38 23aug061	300_PPMV_NMOC	AS014909	Std Loop	None	None	Ч.	2-4			180824GC8A1
~	08/24/18	8:24	8:24 ug\24aug	0.1% CH4_CO2_CO+	AW1309720	Std Loop	None	None	Ч	7,			180824GC8A1
~~~	08/24/18	8:43	8:43 24aug001	LCS	AS014809	Std Loop	None	None	Ļ	2-5	ol		180824GC8A1
6	08/24/18	8:58	8:58 24aug002	LCSD	AS014809	Std Loop	None	None	ц.	2-5	_		180824GC8A1
10	08/24/18	9:13	9:13 24aug003	c2_LcS	AW1309810	Std Loop	None	None	Ч	2,			180824GC8A1
11	08/24/18	9:33	9:33 24aug004	c2_LCSD	AW1309810	Std Loop	None	None	Ч	2,			180824GC8A1
12	08/24/18	9:53	9:53 24aug005	METHOD	BLANK	Std Loop	None	None	Ч	6,	Nc	de	180824GC8A1
ц.	08/24/18	10:21	10:21 24aug006	METHOD	BLANK	Std Loop	None	None	1	6,	ok		180824GC8A1
14	08/24/18	10:51	10:51 24aug007	J081403-01	GOLDER	Std Loop	see log	None	2.295	ά	ok.		180824GC8A1
-51 -	08/24/18	11:10	11:10 24aug008	J081403-02	GOLDER	Std Loop	see log	None	2.295	10,			180824GC8A1
16	08/24/18	11:30	11:30 24aug009	J081403-03	GOLDER	Std Loop	see log	None	2.295	11,			180824GC8A1
11	08/24/18	11:49	11:49 24aug010	J081403-04	GOLDER	Std Loop	see log	None	2.407	12,			180824GC8A1
18	08/24/18	12:09	12:09 24aug011	J081403-05	GOLDER	Std Loop	see log	None	2.193	13,	_		180824GC8A1
19	08/24/18	12:28	12:28 24aug012	J081403-06	GOLDER	Std Loop	see log	None	2.193	14,	_		180824GC8A1
20	08/24/18	12:48	12:48 24aug013	J081403-07	GOLDER	Std Loop	see log	None	2.193	15,			180824GC8A1
	Approved by/Date	by/Date				Air Technology Laboratories, Inc. GC 8A Loø# 45	iology Laborato GC 8A Loe# 45	atories, Inc. 15					Page of 200

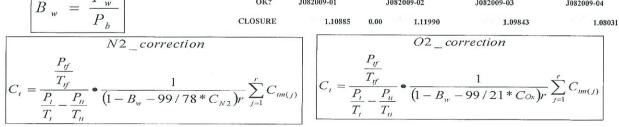
GC 8A Log# 45

J082009

## 2. Sample Raw Data

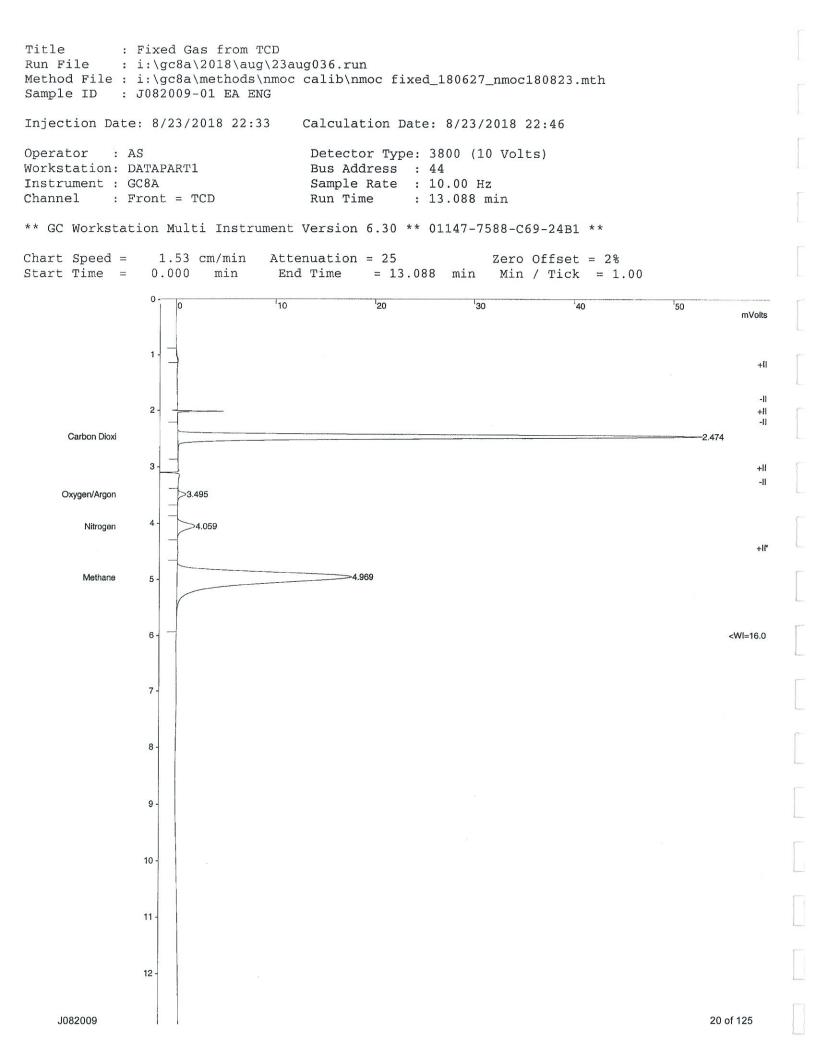
- a. Calculations (if applicable)
- b. Chromatograms/Results

CALCULATIONS										
	Normalized? NO	Variable								
			J082009-01	<b>J0</b> 8	82009-02		J082009-03		J082009-04	
<b>1</b>										
Moisture content, fraction		Bw	0.03123		0.03123		0.03123		0.03123	
Calculated NMOC N2 corr. concentration, ppmv C		C _t	1378.7	1311.4		850.6			1576.8	
Calculated NMOC O2 corr. concentration, p	opmv C	C,	1384.1		1385.3		894.5		1562.2	
Uncorr NMOC concentration, ppmv C Calculated N2 concentration, fraction		C _t	1288.2		657.5		441.2		1479.4	
Measured N2 concentration, fraction		C _{N2}	0.02708		0.36825		0.35460		0.02407	
Calculated O2 concentration, fraction		Cox	0.00838 0.00807		0.12109 0.10482		0.10974		0.00745	
Measured O2 concentration, fraction		Cox	0.00250		0.03447		0.10086 0.03121		0.00461 0.00143	
measured NMOC concentration, ppmv C		C _{tm1}	414.0		224.7		141.4		472.6	
measured NMOC concentration, ppmv C		C _{tm2}	411.3		223.0		141.5		472.7	
measured NMOC concentration, ppmv C		Ctm3	409.3		221.8		139.9		472.5	
barometric pressure, mm Hg		Pb	762.0		762.0		762.0		762.0	
gas sample tank pressure before sampling, m	m Hg	Pti	228.59		228.59		228.59		228.59	
gas sample tank pressure at completion of sa	and the second	P	634.98		660.38		634.98		634.98	
final gas sample tank pressure after pressuria		Ptr	1272.13		1272,13		1272.13		1272.13	
vapor pressure of H2O, mm Hg		Pw	23.8		23.8		23.8		23.8	
sample tank temperature before sampling, of	ç	T ₀	297.0		297.0		297.0		297.0	
sample tank temperature at completion of sa		T _t	297.0		297.0		297.0		297.0	
sample tank temperature after pressurization		Tu	297.0		297.0		297.0		297.0	
Sample tank temperature in field, oC	• 50%	- 0	25.0		25.0		25.0		25.0	
total number of analyzer injections		r	3		3		3		3	
barometric pressure, inches Hg			30		30		30		30	
sample temp in field before sampling, oF			75		75		75		75	
sample temp in field after sampling, oF			75		75		75		75	
Sample pressure prior to sampling, inches Hg			-21	1	-21		-21	/	-21	
Sample pressure after sampling, inches Hg			-5.0	/	-4.0	1	-5.0	/	-5.0	/
Sample pressure after pressurization, psia			24.6		24.6		24.6		24.6	÷.
Sample temp after pressurization, oF			75		75		75	0	75	
	NMOC RUN1		SAMPLE1	SA	MPLE2		SAMPLE3		SAMPLE4	
	NMOC RUN1		414.0		224.7		141.4		472.6	
	NMOC RUN2		411.3 409.3		223.0 221.8		141.5		472.7	
	NMOC DATAFILE1		409.5		221.0		139.9		472.5	
	NMOC DATAFILE2									
	NMOC DATAFILE3									
	NMOC TIME/DATE1	22:33	08/23/18	23:32 0	08/23/18	0:30	08/24/18	1:28	08/24/18	
	NMOC TIME/DATE2	22:48	08/23/18		08/23/18	0:45	08/24/18	1:43	08/24/18	
	NMOC TIME/DATE3	23:02	08/23/18		08/24/18	0:59	08/24/18	1:58	08/24/18	
	RESULT RSD		0.58	- 0.6		_	0.65	/	0.02	
			-			-				
	NITROGEN RUN1		0.839	12.1	119		10.986		0.749	
	NITROGEN RUN2		0.838	12.0	099		10.962		0.740	
	OXYGEN RUN1		0.251	3.4			3.125		0.143	
	OXYGEN RUN2		0.249	3.4	45		3.118		0.142	
	3C DATAFILE1									
	3C DATAFILE2 3C TIME/DATE	23:02	00/02/10	0.01	0/34/10	0.50	00/0///0		00/01/00	
	3C TIME/DATE	23:02	08/23/18 08/23/18		)8/24/18 )8/24/18	0:59 1:14	08/24/18 08/24/18	1:58	08/24/18	
	N2 RSD	25:17	0.12	0:15 0.1		1:14	08/24/18	2:12	08/24/18 1.18	
	O2 RSD		0.72	0.1			0.23		0.75	
				0.1			0.20		0.75 4	
	<b>Carbon Dioxide Run 1</b>		13,485	8.19	93		7.741		13.098	
	Carbon Dioxide Run 2		13.537	8.21	12		7.699		13.055	
	CO2 RSD		0.39	0.2	.3		0.55		0.33	
Manual CO2 and a distance				1						
Measured CO2 concentration fraction			0.13511		0.08202		0.07720		0.13076	
Calculated CO2 concentration, fraction	Mai D 1		0.43657		0.24944		0.24945		0.42253	
	Methane Run 1 Methane Run 2		18.773 18.729	11.7			11.032		18.308	
	CH4 RSD		0.23	11.8			11.008		18.257	
	CII4 KSD		0.25	0.1	4		0.22		0.28	
Measured CH4 concentration fraction			0.18751	0	0.11801		0.11020		0.18282	
Calculated CH4 concentration, fraction			0.60590		0.35889		0.35608		0.59076	
	Carbon Monoxide Run 1		0.0000370		005350		0.0004410		0.0000140	
	Carbon Monoxide Run 2		0.0000350		004940		0.0004400		0.0000150	
	CO RSD		5.56	7.9	7		0.23		6.90	
Measured CO concentration fraction			0.00000	0	0.00001		0.00000		0.00000	
Calculated CO concentration fraction			0.00000		.00002		0.00001		0.00000	
	Hydrogen Run 1		0		218306		0.188295		0.247941	
	Hydrogen Run 2		0		258007		0.19413		0.192255	
	H2 RSD		#DIV/0!	16.6	57		3.05		25.30	
Measured H2 concentration fraction			0.00000		00320		0.00101		0.00000	
Calculated H2 concentration fraction			0.00000 0.00000		0.00238		0.00191		0.00220	
concentration fraction			0.00000	0	0.00724		0.00618		0.00711	
·										
D										
$P = P_w$		ок? ј	082009-01	J082009-(	02	J082	009-03	J083	2009-04	
$B_w = \frac{T_w}{D}$	1. 1.		24.24							
	C	OCUDE	1 10007	0.00			4 000 10		<ul> <li>International contents</li> </ul>	



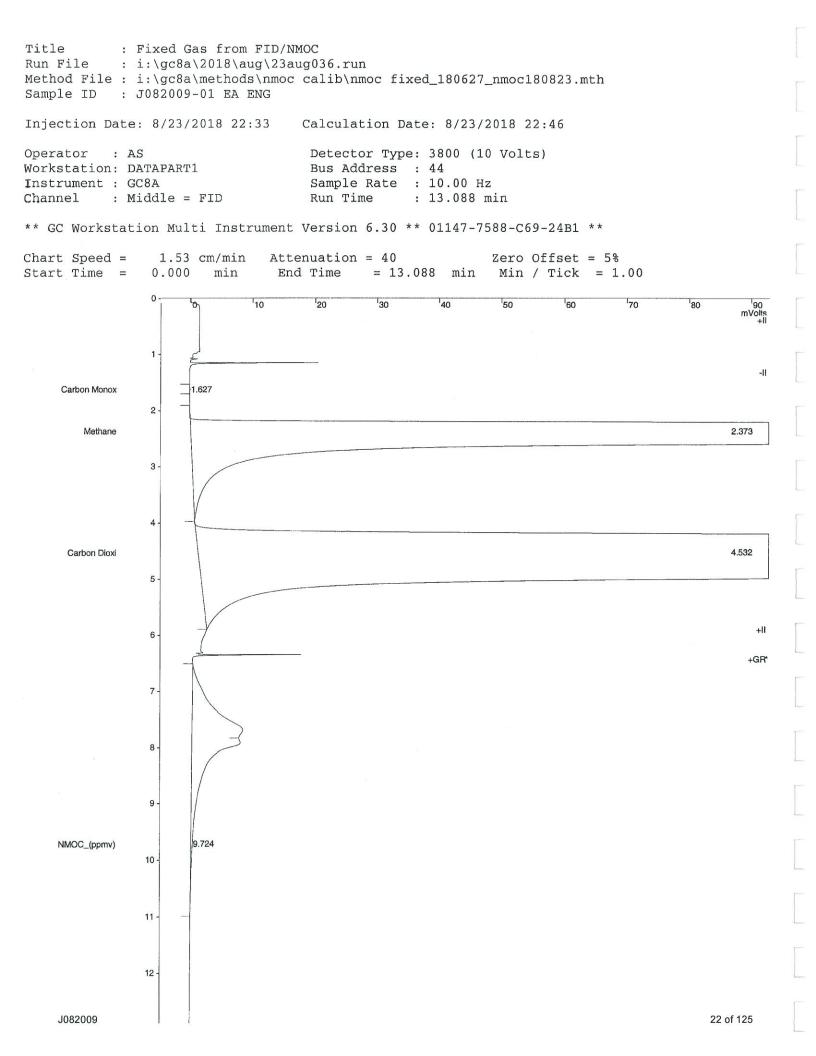
CALCULATIONS

CALCULATIONS						
Normalized? NO	Variable	J082009-05				
		3082009-05				
Moisture content, fraction	Bw	0.03123				
Calculated NMOC N2 corr. concentration, ppmv C	Ct	1427.9				
Calculated NMOC O2 corr. concentration, ppmv C	C,	1429.3				
Uncorr NMOC concentration, ppmv C	C,	1276.8				
Calculated N2 concentration, fraction Measured N2 concentration, fraction	C _{N2}	0.05881 0.01934				
Calculated O2 concentration, fraction	Cox	0.01601				
Measured O2 concentration, fraction	010000	0.00526				
measured NMOC concentration, ppmv C	Ctm1	433.9				
measured NMOC concentration, ppmv C	Ctm2	432.7				
measured NMOC concentration, ppmv C	Ctm3	433.5				
barometric pressure, mm Hg	Pb	762.0				
gas sample tank pressure before sampling, mm Hg gas sample tank pressure at completion of sampling, mm Hg	Pti	228.59 660.38				
final gas sample tank pressure after pressurization, mm Hg	P _t P _{tf}	1272.13				
vapor pressure of H2O, mm Hg	Pw	23.8				
sample tank temperature before sampling, oK	Tti	297.0	A			
sample tank temperature at completion of sampling, oK	T	297.0				
sample tank temperature after pressurization, oK	Ttf	297.0				
Sample tank temperature in field, oC		25.0				
total number of analyzer injections barometric pressure, inches Hg	r	3 30				
sample temp in field before sampling, oF		75				
sample temp in field after sampling, oF		75				
Sample pressure prior to sampling, inches Hg		-21				
Sample pressure after sampling, inches Hg Sample pressure after pressurization, psia		-4.0 24.6				
Sample pressure after pressurization, psia		24.6				
		SAMPLE1				
NMOC RUN1		433.9				
NMOC RUN2 NMOC RUN3		432.7 433.5				
NMOC DATAFILE1		433.5				
NMOC DATAFILE2						
NMOC DATAFILE3						
NMOC TIME/DATE1	2:27	08/24/18				
NMOC TIME/DATE2 NMOC TIME/DATE3	2:41 2:56	08/24/18 08/24/18				
RESULT RSD	2.50	0.14	2			
NITROGEN RUN1		1.983				
NITROGEN RUN2 OXYGEN RUN1		1.884 0.539				
OXYGEN RUNI OXYGEN RUN2		0.513				
3C DATAFILE1		0.010				
3C DATAFILE2						
3C TIME/DATE	2:41	08/24/18				
3C TIME/DATE	2:56	08/24/18				
N2 RSD O2 RSD		5.15				
		4.50				
Carbon Dioxide Run 1		13.194				
Carbon Dioxide Run 2		12.739				
CO2 RSD		3.51				
Measured CO2 concentration fraction		0.12967				
Calculated CO2 concentration, fraction		0.39435				
Methane Run 1		20.368				
Methane Run 2		19.651				
CH4 RSD		3.58				
Measured CH4 concentration fraction		0.20010				
Calculated CH4 concentration, fraction		0.60854				
Carbon Monoxide Run 1		0.0000700				
Carbon Monoxide Run 2 CO RSD		0.0000720				
CO RSD		2.82				
Measured CO concentration fraction		0.00000				
Calculated CO concentration fraction		0.00000				
Hydrogen Run 1		0.240271				
Hydrogen Run 2 H2 RSD		0 200.00				
12 850						
Measured H2 concentration fraction		0.00120				
Calculated H2 concentration fraction		0.00365				
D						
$B_{w} = \frac{P_{w}}{D}$	OK? JO	82009-05				
$D_w = -\frac{P}{P}$	LOSURE	1.11259				
	LOSURE	1.11259				
N2 correction			O2_correction			
N2_correction O2_correction						
$P_{tf}$		$P_{if}$				
$\frac{1}{T}$ 1	1 -					
$C_{t} = \frac{I_{tf}}{P P} \bullet \frac{1}{(1 P P)^{2}}$	$\Sigma C$	$C_i = \frac{c_i}{D}$	$\frac{P_{n}}{P_{n}} \bullet \frac{1}{(1 - B_{w} - 99 / 21 * C_{Ox})r} \sum_{j=1}^{r} C_{im(j)}$			
$C_{t} = \frac{\overline{T_{tt}}}{\underline{P_{t}} - \underline{P_{tt}}} \bullet \frac{1}{(1 - B_{w} - 99 / 78 * C_{N2})r}$	$\sum_{j=1}^{j} m(j)$	$\frac{P_1}{1} = \frac{1}{2}$	$(1 - B_{yr} - 99721 + Co_x)r_{j=1}$			
$\frac{1}{T_{i}} = \frac{1}{T_{ii}}$		T, T				
~/ *//						



Print Date: Thu Aug 23 22:46:42 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug036.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 22:33 Calculation Date: 8/23/2018 22:46 Detector Type: 3800 (10 Volts) : AS Operator Workstation: DATAPART1 Bus Address : 44 Instrument : GC8A Sample Rate : 10.00 Hz Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Time Width Result Ret. Time Offset Area Sep. 1/2 (min) (min) (counts) Code (sec) Peak Peak Status No. Name Codes ---- -----_____ 1.930 2.474 1 Hydrogen М 
 2 Carbon Dioxi
 13.532410
 2.474
 0.029

 3 Oxygen/Argon
 0.258808
 3.495
 -0.002
 251934 BB 4.5 3768 BB 3 Oxygen, .... 4 Nitrogen 0.8/2001 18.809752 4.3 0.872802 4.059 -0.007 18.809752 4.969 -0.028 13454 BB 7.4 BB 12.4 7.4 5 Methane 243057 --- -------- ========== ----33.473772 Totals: -0.008 512213 106% Status Codes: M - Missing peak Total Unidentified Counts : 0 counts Detected Peaks: 5 Rejected Peaks: 1 Identified Peaks: 5 Unidentified Peak Factor: 0 Multiplier: 1 Divisor: 1 Baseline Offset: 17 microVolts LSB: 1 microVolts Noise (used): 7 microVolts - monitored before this run Manual injection Revision Log: 8/23/2018 22:46: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 22:31:48 Original Notes: 

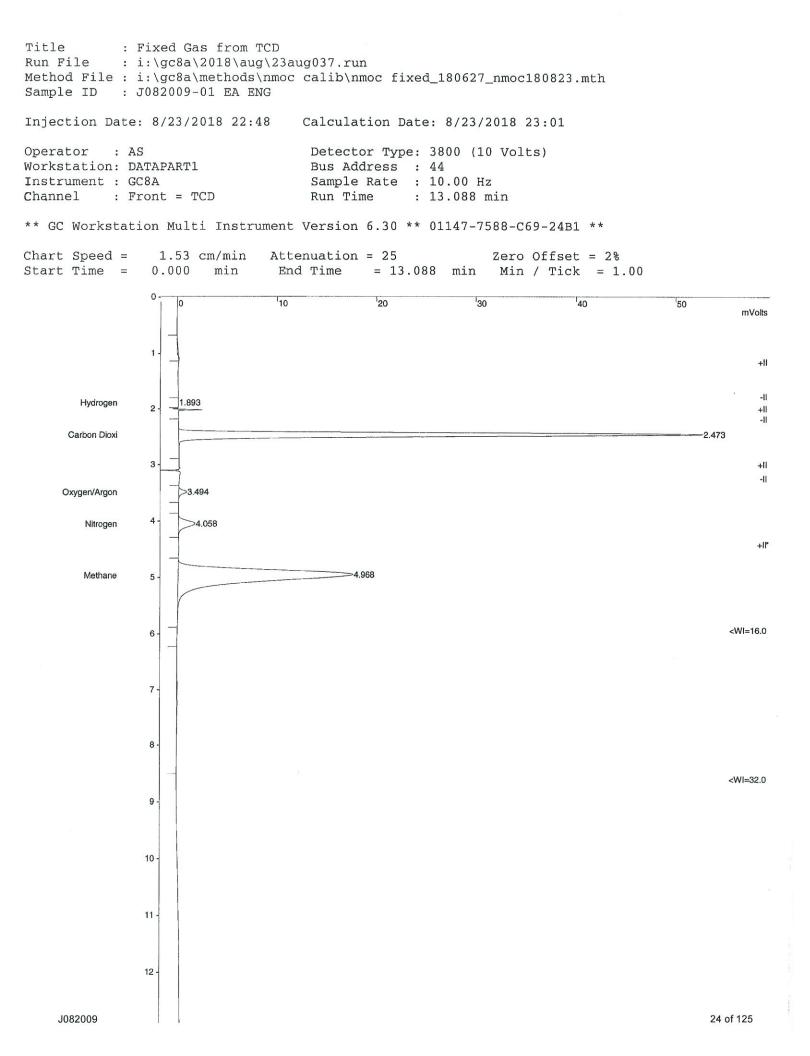


Print Date: Thu Aug 23 22:46:43 2018 Page 1 of 1 ] Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug036.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed 180627 nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 22:33 Calculation Date: 8/23/2018 22:46 Operator : AS Detector Type: 3800 (10 Volts) Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : Middle = FID Channel Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Time Width Ret Ret. Time Width Time Offset Area Sep. 1/2 Status (min) (min) (counts) Code (sec) Codes Peak Result Name (% v/v) Peak No. -- ---------_____ 
 1 Carbon Monox
 0.000031
 1.627
 0.049
 320

 2 Methane
 11.982968
 2.373
 0.001
 124053872

 3 Carbon Dioxi
 14.417774
 4.532
 -0.031
 148408720

 4 NMOC_(ppmv)
 413.998077
 9.724
 0.001
 492356
 320 BV 4.6 PP 11.6 C PB 18.6 C 4 NMOC_(ppmv) 413.998077 9.724 0.001 492356 GR 0.0 C ____ _ ____ Totals: 440.398850 0.020 272955268 Status Codes: C - Out of calibration range Total Unidentified Counts : 259 counts Detected Peaks: 6 Rejected Peaks: 0 Identified Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -89 microVolts LSB: 1 microVolts Noise (used): 10 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/23/2018 22:46: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 22:31:48 Original Notes: 



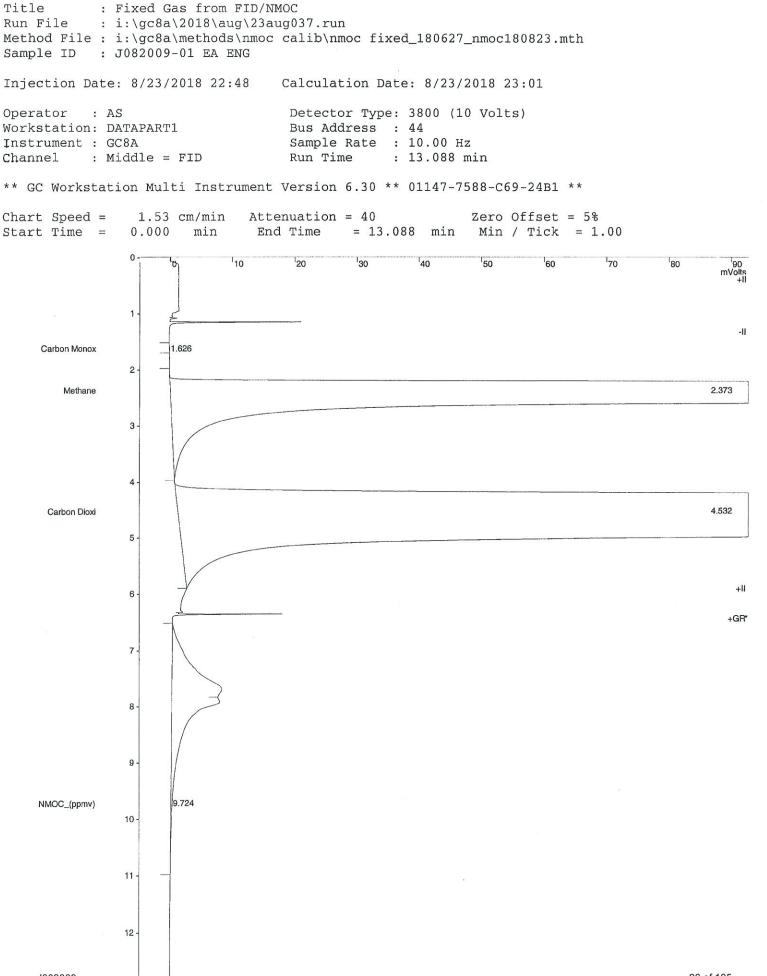
Print Date: Thu Aug 23 23:01:18 2018 Page 1 of 1 : Fixed Gas from TCD Title Run File : i:\gc8a\2018\aug\23aug037.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 22:48 Calculation Date: 8/23/2018 23:01 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : Front = TCD Run Time : 13.088 min Channel ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Width Ret. Time Time Offset Area sep. ... (min) (counts) Code (sec) Time Area Sep. 1/2 Result Status Peak Name Peak Codes No. (% v/v) (min) (-----0.037 48 BB 4.2 _____ ____ 
 0.200904
 1.893
 -0.037
 48

 13.485770
 2.473
 0.028
 251066

 0.253982
 3.494
 -0.003
 3698

 0.844585
 4.058
 -0.008
 13019

 18.747854
 4.968
 -0.029
 242258
 1 Hydrogen BB 4.5 2 Carbon Dioxi 13.485770 BB 4.3 3 Oxygen/Argon 0.253982 4 Nitrogen 0.844585 3 Oxygen 0.84400 4 Nitrogen 0.84400 18.747854 BB 7.3 BB 12.4 5 Methane _ _ _ _ _ _ _ _ _ -0.049 510089 Totals: 33.533095 4833 counts Total Unidentified Counts : Rejected Peaks: 1 Identified Peaks: 5 Detected Peaks: 7 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: 1 microVolts Baseline Offset: 14 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/23/2018 23:01: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 22:46:27 Original Notes: 



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Print Date: Thu Aug 23 23:01:19 2018 Page 1 of 1 : Fixed Gas from FID/NMOC : i:\gc8a\2018\aug\23aug037.run Title Run File Method File : i:\gc8a\methods\nmoc calib\nmoc fixed 180627 nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 22:48 Calculation Date: 8/23/2018 23:01 Operator : AS Detector Type: 3800 (10 Volts) Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 m Instrument : GC8A : Middle = FID Channel : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard 
 Ret.
 Time
 Width

 Peak
 Result
 Time
 Offset
 Area
 Sep. 1/2

 Name
 (% v/v)
 (min)
 (min)
 (counts)
 Code (sec)
 Ret. Time Width Peak Status No. Codes _ _ _ _ _ 

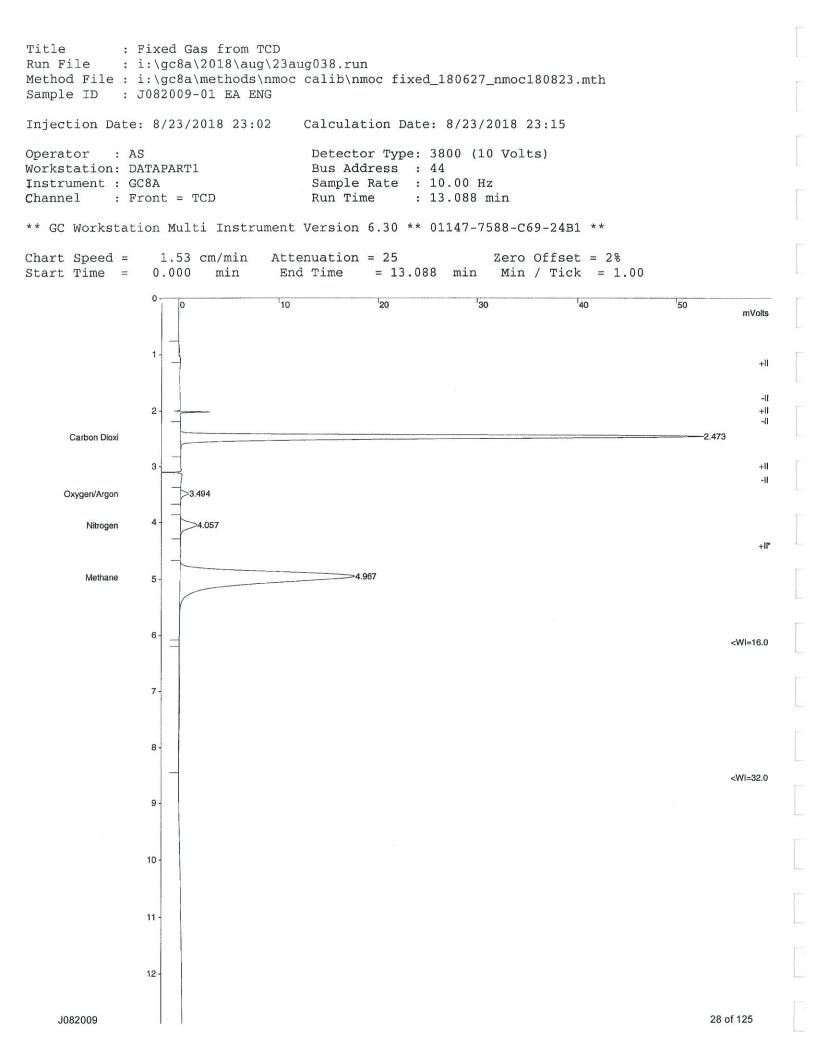
 1
 Carbon Monox
 0.000037
 1.626
 0.048
 383
 BV

 2
 Methane
 11.982177
 2.373
 0.001
 124045672
 PP

 3
 Carbon Dioxi
 14.416704
 4.532
 -0.031
 148397712
 PB

 4
 NMOC_(ppmv)
 411.321472
 9.724
 0.001
 489172
 GR

 4.5 PP 11.6 C PB 18.6 C 4 NMOC_(ppmv) 411.321472 GR 0.0 C ----- whereas whereas ---- -----Totals: 437.720390 0.019 272932939 Status Codes: C - Out of calibration range Total Unidentified Counts : 350 counts Detected Peaks: 6 Rejected Peaks: 0 Identified Peaks: 4 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: -93 microVolts LSB: 1 microVolts Noise (used): 8 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/23/2018 23:01: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 22:46:27 Original Notes: 



Print Date: Thu Aug 23 23:15:56 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug038.run Title Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 23:02 Calculation Date: 8/23/2018 23:15 Detector Type: 3800 (10 Volts) Operator : AS Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A : 13.088 min Channel : Front = TCD Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Time Offset Width Area Sep. 1/2 ----(counts) Code (sec) Codes Area Sep. 1/2 Result (% v/v) Peak Peak Status Name (min) (min) No. ----- ----- ----- -----1.930 1 Hydrogen M 

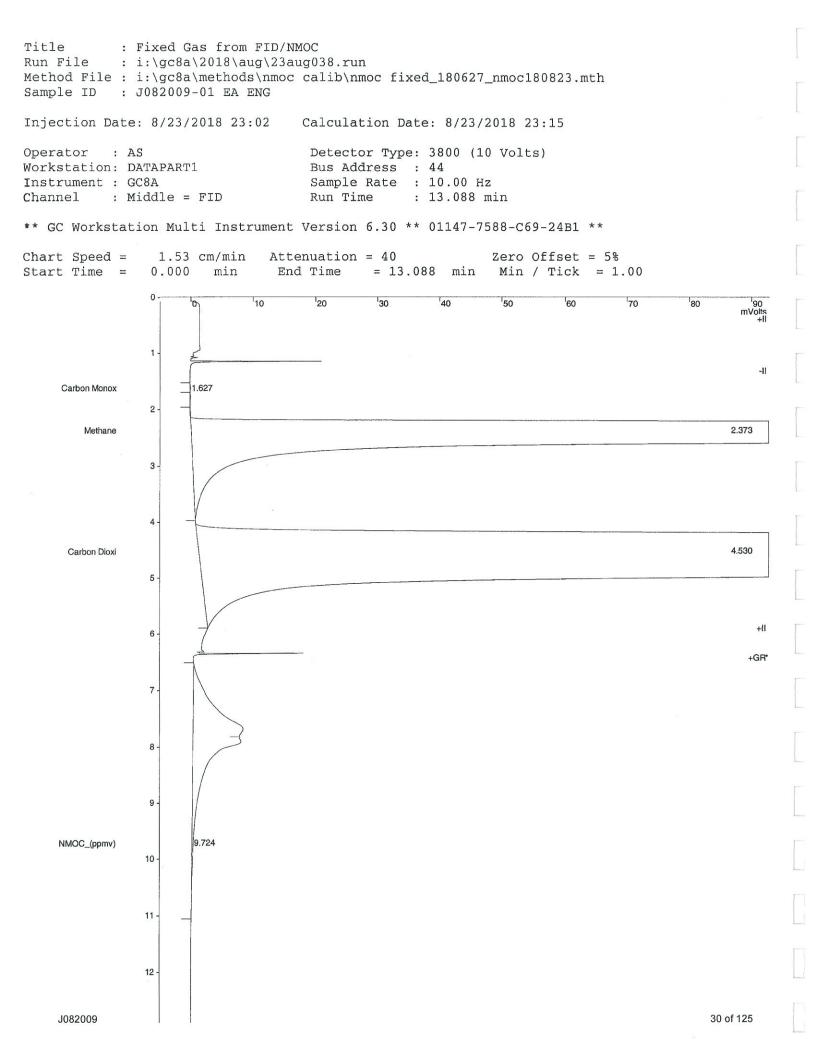
 2
 Carbon Dioxi
 13.484701
 2.473
 0.028
 251046
 BB
 4.5

 3
 Oxygen/Argon
 0.250594
 3.494
 -0.003
 3649
 BB
 4.3

 4
 Nitrogen
 0.838550
 4.057
 -0.009
 12926
 BB
 7.3

 5
 Methane
 18.772959
 4.967
 -0.030
 242582
 BB
 12.4

 _ _ _ _ _ _ 33.346804 -0.014 510203 Totals: Status Codes: M - Missing peak Total Unidentified Counts : 5021 counts Detected Peaks: 6 Rejected Peaks: 1 Identified Peaks: 5 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: 1 microVolts Baseline Offset: 10 microVolts Noise (used): 6 microVolts - monitored before this run Manual injection Revision Log: 8/23/2018 23:15: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 23:01:01 Original Notes: 



Print Date: Thu Aug 23 23:15:57 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug038.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-01 EA ENG Injection Date: 8/23/2018 23:02 Calculation Date: 8/23/2018 23:15 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A Channel : Middle = FID Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Width PeakResultTimeOffsetAreaSep. 1/2StatusName(% v/v)(min)(min)(counts)Code (sec)Codes Peak Peak Status NO. (miii) (cource, _____ ____ ___ _____ 

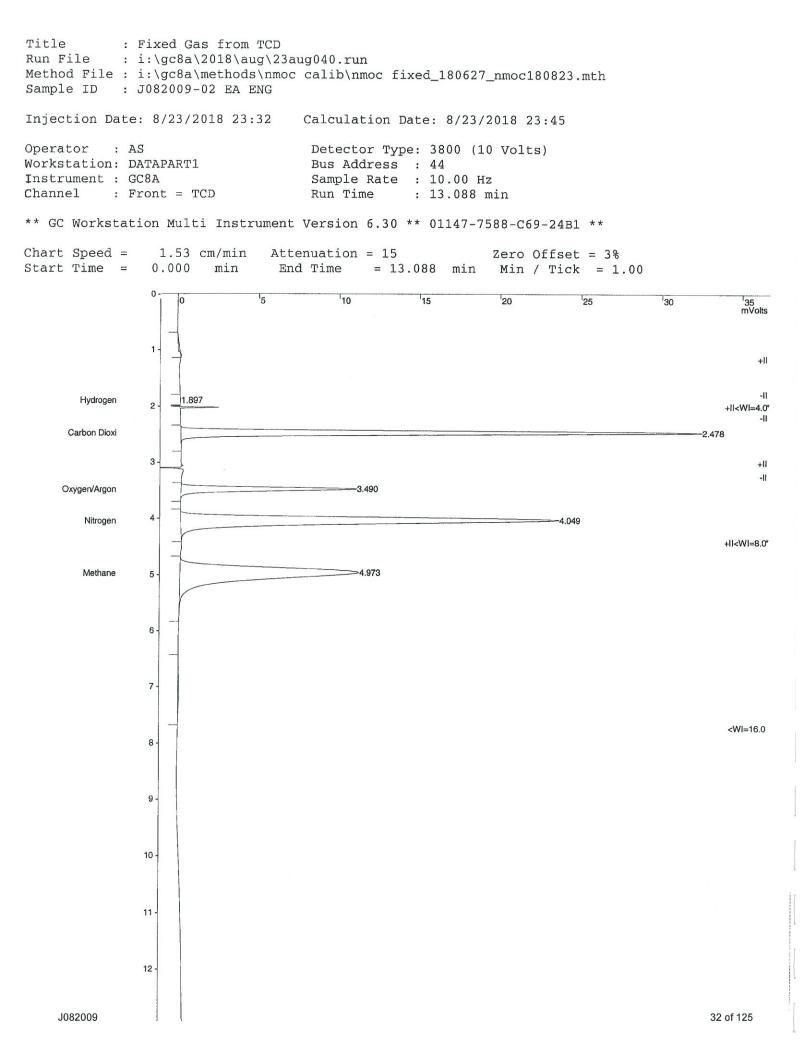
 1
 Carbon Monox
 0.000035
 1.627
 0.049
 362

 2
 Methane
 11.977551
 2.373
 0.001
 123997792

 3
 Carbon Dioxi
 14.423774
 4.530
 -0.034
 148470480

 4
 NMOC_(ppmv)
 409.278900
 9.724
 0.001
 486743

 BV 4.3 PP 11.6 C PB 18.6 C GR 0.0 C ___ ____ _ _ _ _ _ -----0.017 272955377 Totals: 435.680260 Status Codes: C - Out of calibration range Total Unidentified Counts : 350 counts Detected Peaks: 6 Rejected Peaks: 0 Identified Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 LSB: Baseline Offset: -12 microVolts 1 microVolts Noise (used): 7 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/23/2018 23:15: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 7, Advance Time: 23:01:01 Original Notes: 



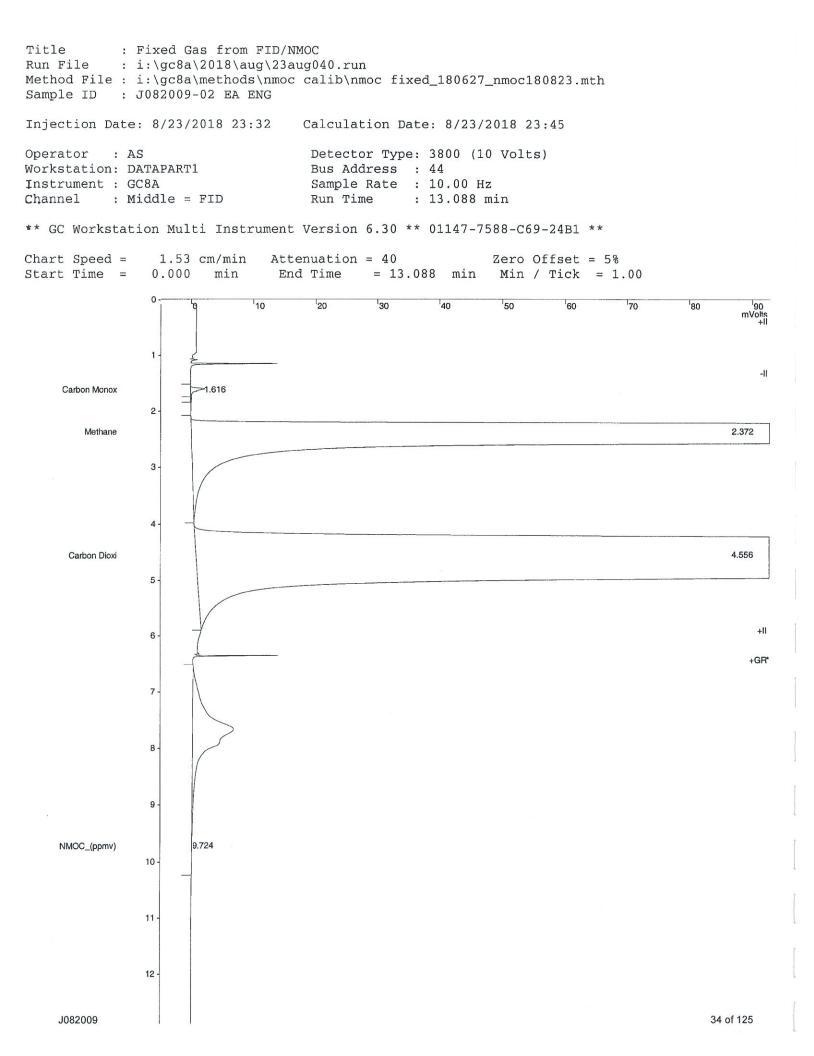
Print Date: Thu Aug 23 23:45:10 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug040.run Title Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/23/2018 23:32 Calculation Date: 8/23/2018 23:45 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis. Peak Measurement: Peak Area Calculation Type: External Standard Width Area Sep. 1/2 Area Sep. 1/2 (counts) Code (sec) Codes Peak Status No. (min) (min) ----- 
 1
 Hydrogen
 0.227996
 1.897
 -0.033

 2
 Carbon Dioxi
 8.209311
 2.478
 0.033

 3
 Oxygen/Argon
 3.449760
 3.490
 -0.007

 4
 Nitrogen
 12.121877
 4.049
 -0.017

 5
 Methane
 11.809709
 4.973
 -0.024
 BB 3.7 55 152834 BB 4.4 50231 4.3 186853 1553 BB 7.3 152604 BB 12.4 ____ ____ 542577 35.818653 -0.048 Totals: Total Unidentified Counts :  $\int \mathcal{J} \left( \begin{array}{c} \mathcal{J} \\ 2135 \end{array} \right)$  counts Rejected Peaks: 1 Identified Peaks: 5 Detected Peaks: 7 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: 8 microVolts LSB: 1 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/23/2018 23:45: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:30:17 Original Notes: 



Print Date: Thu Aug 23 23:45:10 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug040.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/23/2018 23:32 Calculation Date: 8/23/2018 23:45 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A Run Time : 13.088 min Channel : Middle = FID ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Result Time Offset Area Sep. 1/2 Status (min) (min) (counts) Code (sec) Codes Status Peak Result Name (% v/v) Peak No. 0.038 8897 _ _ _ _ _ _ _____ ____ ---- 

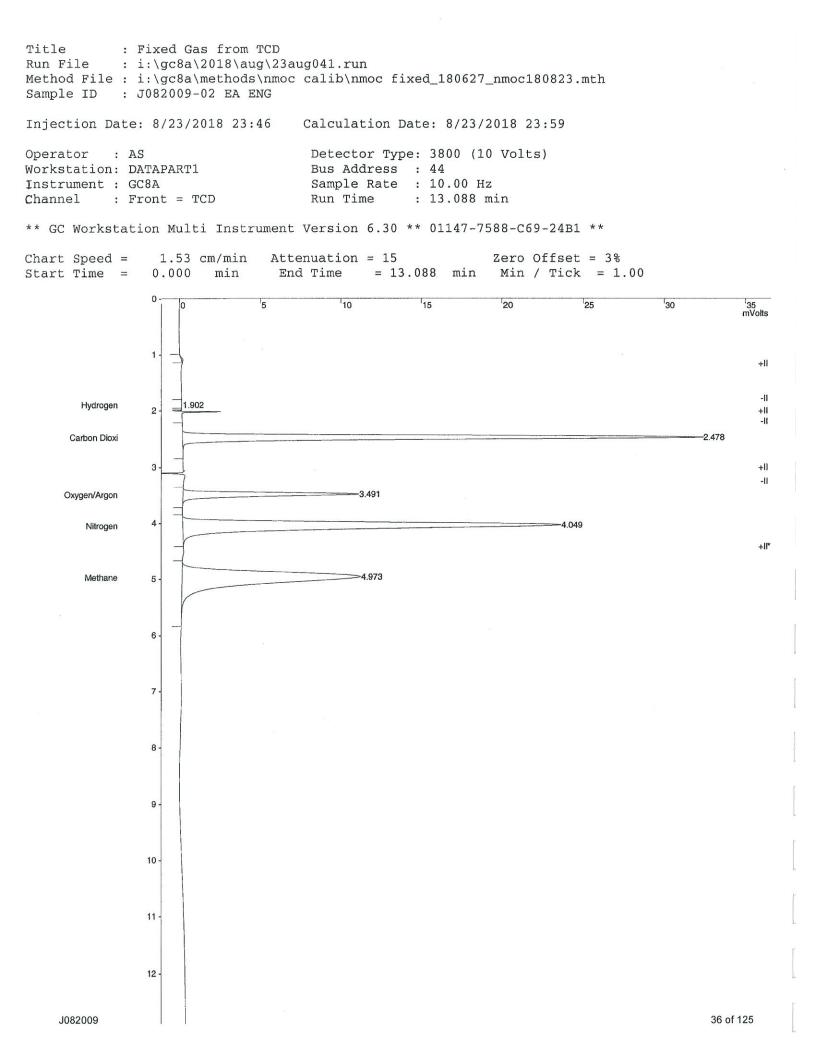
 1
 Carbon Monox
 0.000869
 1.616
 0.038
 8897

 2
 Methane
 10.037601
 2.372
 0.000
 103914424

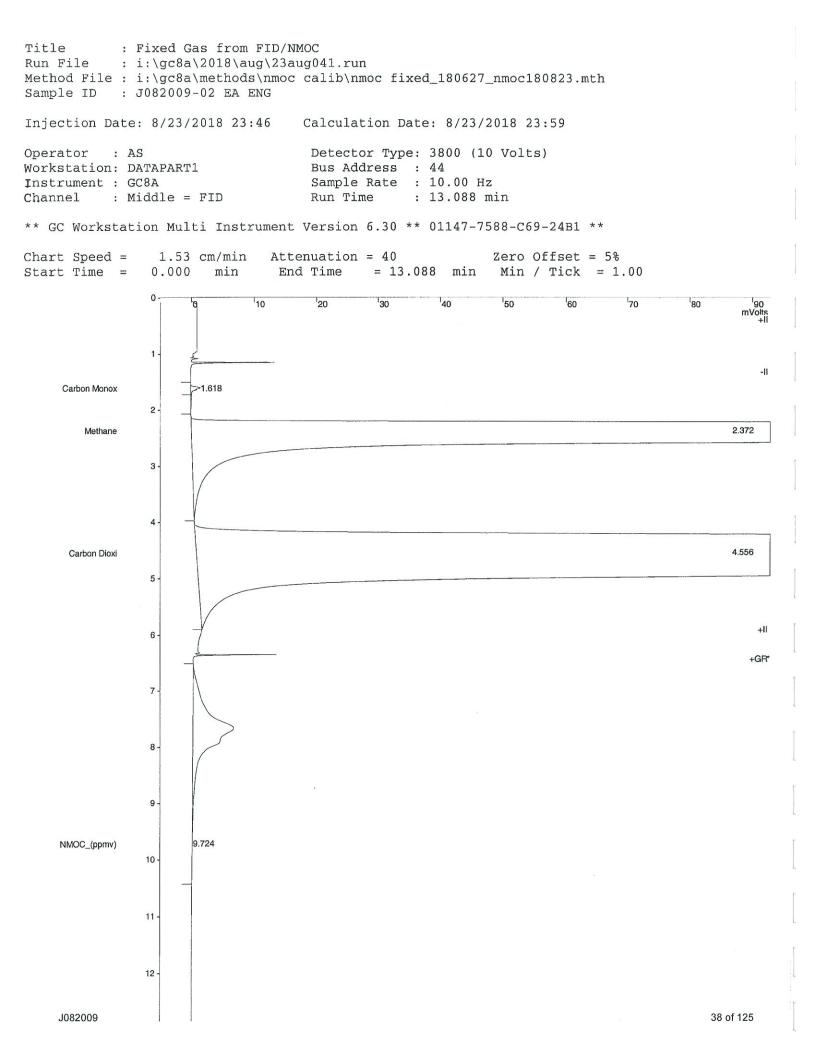
 3
 Carbon Dioxi
 8.876170
 4.556
 -0.007
 91366464

 4
 NMOC_(ppmv)
 224.653152
 9.724
 0.001
 267173

 BP 2.7 PP 9.6 PB 18.4 C C GR 0.0 ____ ____ 0.032 195556958 Totals: 243.567792 Status Codes: C - Out of calibration range Total Unidentified Counts : 110 counts Rejected Peaks: 0 Identified Peaks: 4 Detected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 Multiplier: 1 Baseline Offset: -7 microVolts LSB: 1 microVolts Noise (used): 8 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/23/2018 23:45: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:30:17 Original Notes: 



Print Date: Thu Aug 23 23:59:45 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug041.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/23/2018 23:46 Calculation Date: 8/23/2018 23:59 Operator : AS Detector Type: 3800 (10 Volts) Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : 13.088 min : Front = TCD Channel Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Time Offset Area Sep. ... (min) (counts) Code (sec) Ret. Time Width Peak Result Name (% v/v) Peak Status No. Codes ____ _____ 1 Hydrogen0.2616041.902-0.0282 Carbon Dioxi8.2105772.4780.0333 Oxygen/Argon3.4457663.491-0.0064 Nitrogen12.1053174.049-0.0175 Methane11.7948314.973-0.024 63 BV 6.1 152857 BB 4.4 50172 BB 4.3 7.3 BB 186598 152411 BB 12.4 ____ ____ ____ 35.818095 -0.042 542101 Totals: Total Unidentified Counts : 413 counts Rejected Peaks: 1 Identified Peaks: 5 Detected Peaks: 7 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: 10 microVolts LSB: 1 microVolts Noise (used): 7 microVolts - monitored before this run Manual injection Revision Log: 8/23/2018 23:59: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:44:53 Original Notes: *****



Print Date: Thu Aug 23 23:59:46 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug041.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/23/2018 23:46 Calculation Date: 8/23/2018 23:59 Detector Type: 3800 (10 Volts) Operator : AS Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Middle = FID Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Width Time Offset Area Sep. 1/2 Status (min) (min) (counts) Code (sec) Codes Area Sep. 1/2 Peak Result Name (% v/v) Peak Peak Status No. ____ ____ 

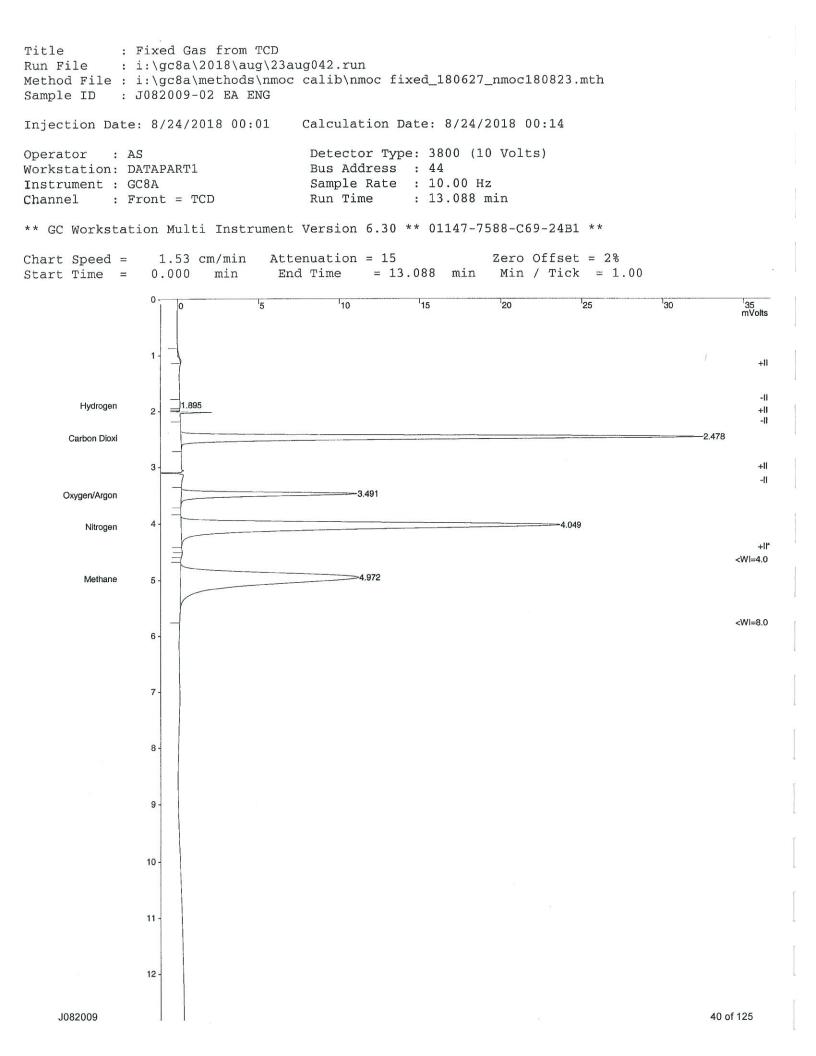
 1 Carbon Monox
 0.000535
 1.618
 0.040
 5477

 2 Methane
 10.037677
 2.372
 0.000
 103915208

 3 Carbon Dioxi
 8.875484
 4.556
 -0.008
 91359408

 4 NMOC_(ppmv)
 223.019501
 9.724
 0.001
 265230

 BV 3.7 PP 9.6 PB 18.4 C C GR 0.0 ---- ------------ ======== ____ ____ ____ 241.933197 0.033 195545323 Totals: Status Codes: C - Out of calibration range Total Unidentified Counts : 1001 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: 1 microVolts Baseline Offset: -3 microVolts Noise (used): 9 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/23/2018 23:59: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:44:53 Original Notes: 



Print Date: Fri Aug 24 00:14:21 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug042.run Title Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/24/2018 00:01 Calculation Date: 8/24/2018 00:14 Operator : AS Detector Type: 3800 (10 Volts) Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Front = TCD : 13.088 min Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret.TimeWidthPeakResultTimeOffsetAreaSep.1/2Name(% v/v)(min)(min)(counts)Code (sec) Peak Status No. Codes _____ _ _____ ------____ 

 1
 Hydrogen
 0.218306
 1.895
 -0.035
 52

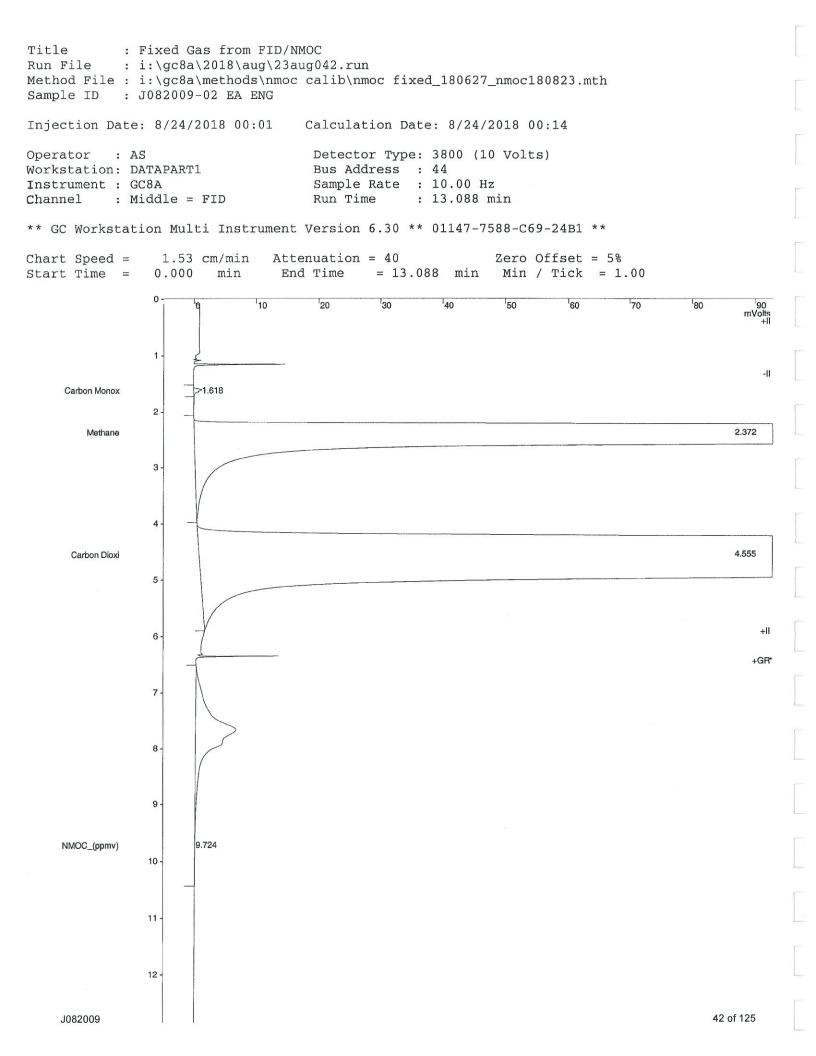
 2
 Carbon Dioxi
 8.192630
 2.478
 0.033
 152523

 3
 Oxygen/Argon
 3.448469
 3.491
 -0.006
 50212

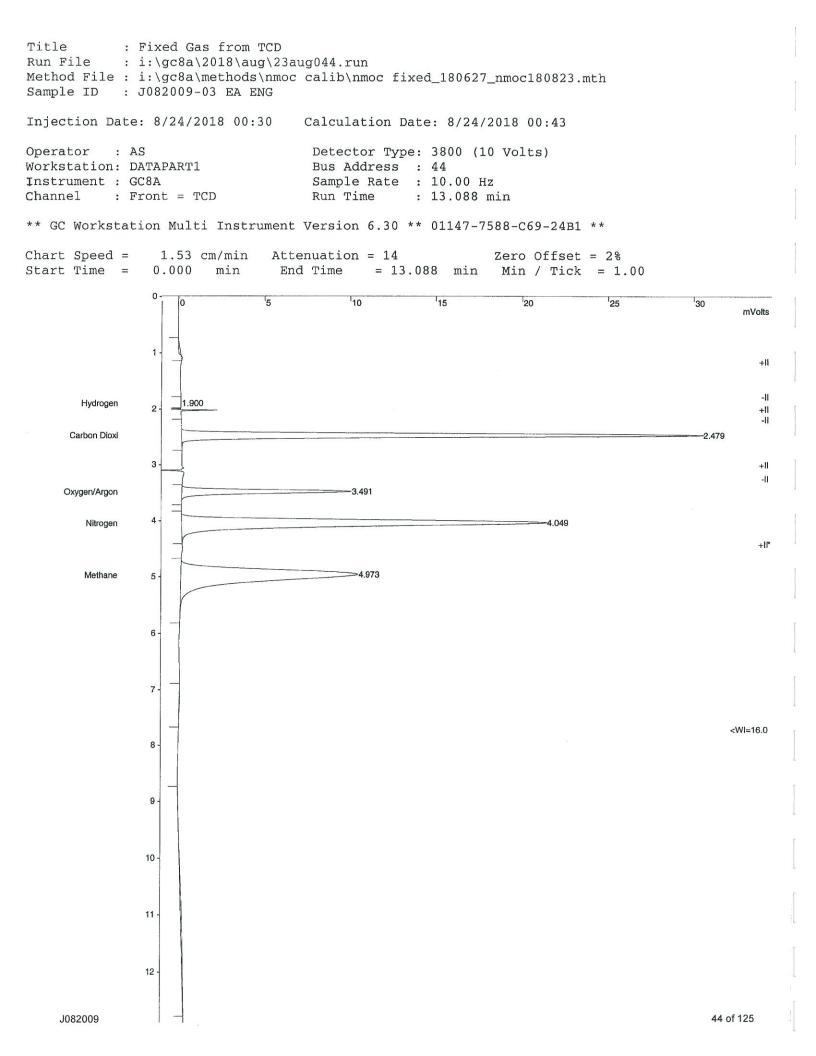
 4
 Nitrogen
 12.119019
 4.049
 -0.017
 186809

 5
 Methane
 11.794215
 4.972
 -0.025
 152403

 52 BP 5.8 152523 BB 4.4 BB 4.3 BB 7.3 BB 12.4 ____ ____ Totals: 35.772639 -0.050 541999 Total Unidentified Counts : 47 counts Rejected Peaks: 2 Identified Peaks: 5 Detected Peaks: 8 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: 5 microVolts LSB: 1 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 00:14: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:59:30 Original Notes: 



Print Date: Fri Aug 24 00:14:21 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Title : Fixed Gas From File, And Gas Run File : i:\gc8a\2018\aug\23aug042.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-02 EA ENG Injection Date: 8/24/2018 00:01 Calculation Date: 8/24/2018 00:14 Operator : AS Detector Type: 3800 (10 Volts) Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Middle = FID Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Time Offset Width Area Sep. 1/2 Peak Result Name (% v/v) Result Peak Status No. (min) (min) (counts) Code (sec) Codes ------____ ____ 1 Carbon Monox0.0004941.6180.04050542 Methane10.0393852.3720.0001039328883 Carbon Dioxi8.8811834.555-0.008914180644 NMOC_(ppmv)221.8197179.7240.001263804 BV 3.8 PP 9.6 C PB 18.4 C GR 0.0 ____ ____ ____ __ -----0.033 195619810 Totals: 240.740779 Status Codes: C - Out of calibration range Total Unidentified Counts : 1006 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -2 microVolts LSB: 1 microVolts Noise (used): 9 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 00:14: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 8, Advance Time: 23:59:30 Original Notes: ****



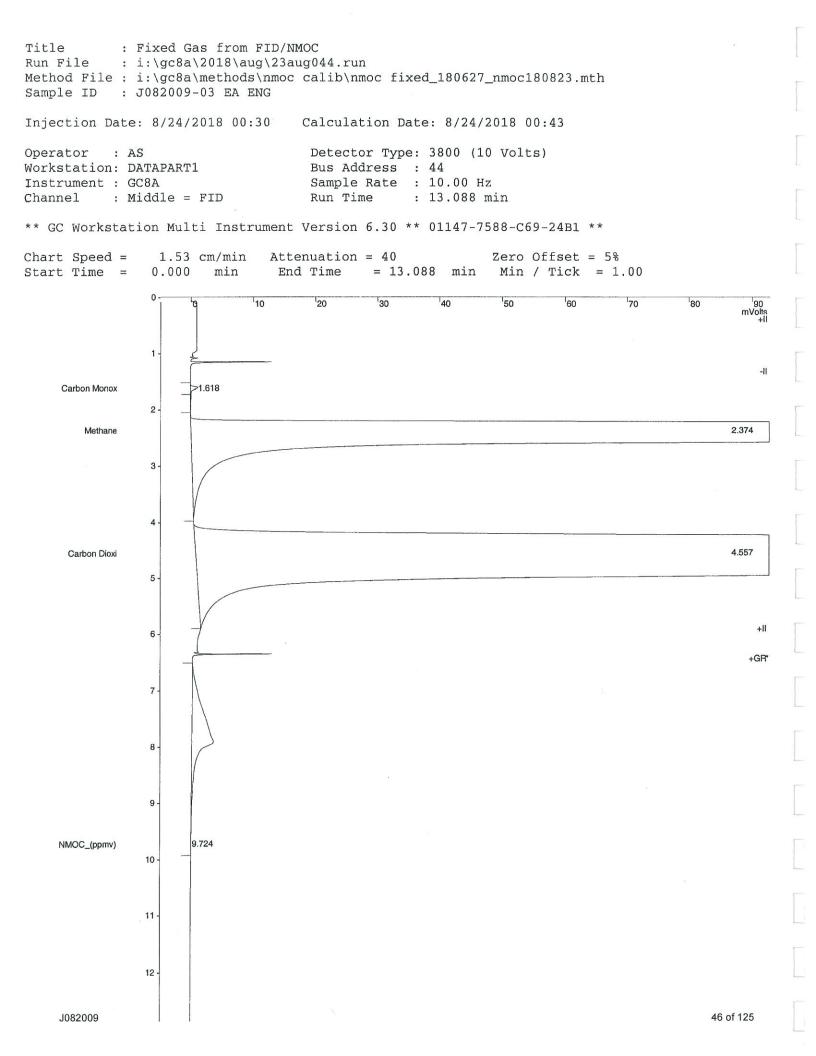
Print Date: Fri Aug 24 00:43:32 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug044.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:30 Calculation Date: 8/24/2018 00:43 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Workstation: DATAPART1 Instrument : GC8A Sample Rate : 10.00 Hz Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. III. Time Offset Area sep. ... (min) (counts) Code (sec) Ret. Time Peak Result Name (% v/v) Area Sep. 1/2 Status Peak No. Codes _____ ____ _____ ____ 
 1
 Hydrogen
 0.231331
 1.900
 -0.030
 56

 2
 Carbon Dioxi
 7.720663
 2.479
 0.034
 143736

 3
 Oxygen/Argon
 3.123269
 3.491
 -0.006
 45477

 4
 Nitrogen
 10.982498
 4.049
 -0.017
 169290

 5
 Methane
 11.035201
 4.973
 -0.024
 142596
 56 BB 4.4 143736 BB 4.4 4.3 BB BB 7.3 BB 12.4 ----- excess sesterant ____ ____ _____ 33.092962 -0.043 501155 Totals: Total Unidentified Counts : 105 (7290 counts Detected Peaks: 8 Rejected Peaks: 1 Identified Peaks: 5 Unidentified Peak Factor: 0 Multiplier: 1 Divisor: 1 LSB: Baseline Offset: 6 microVolts 1 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 00:43: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmog fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:28:40 Original Notes: 



Print Date: Fri Aug 24 00:43:32 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug044.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:30 Calculation Date: 8/24/2018 00:43 Operator : AS Detector Type: 3800 (10 Volts) Workstation: DATAPART1 Bus Address : 44 Instrument : GC8A Sample Rate : 10.00 Hz : Middle = FID Channel Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard 
 Ret.
 Iffee

 Peak
 Result
 Time
 Offset
 Area
 Sep. 1/2

 Name
 (% v/v)
 (min)
 (min)
 (counts)
 Code (sec)
 Ret. Time Width Width Area Sep. 1/2 Status Peak No. Codes ----_____ 

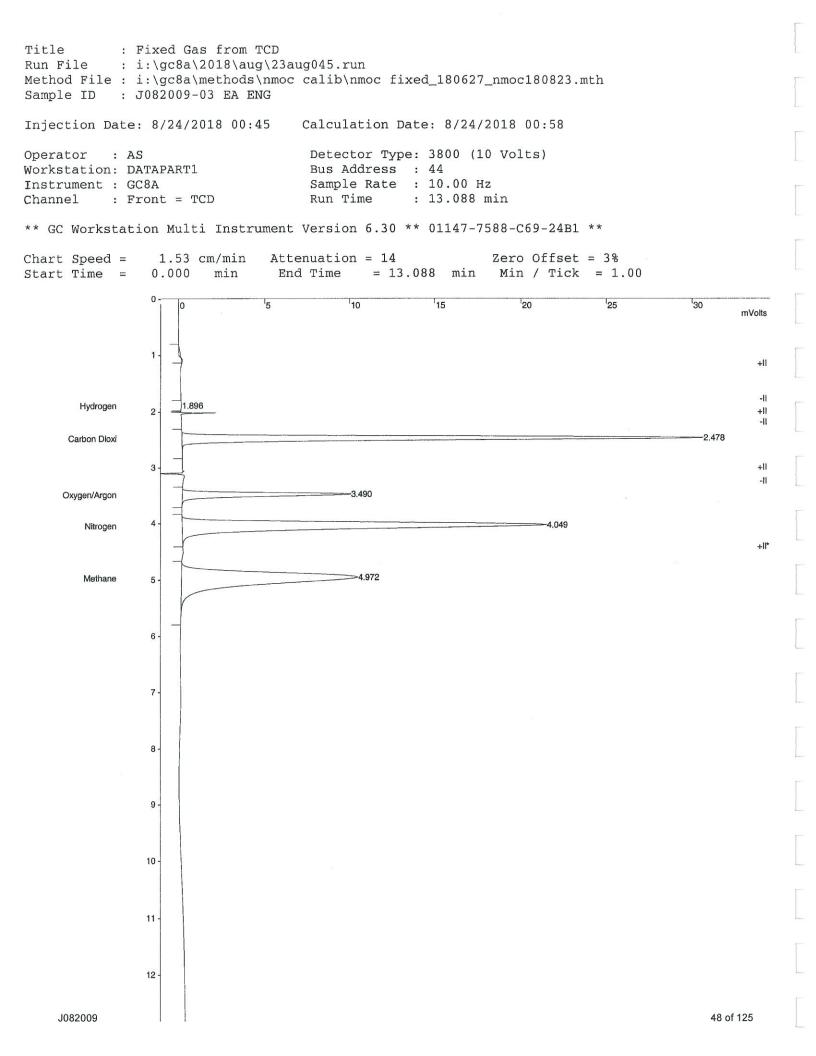
 1
 Carbon Monox
 0.000438
 1.618
 0.041
 4487

 2
 Methane
 9.720655
 2.374
 0.002
 100633240

 3
 Carbon Dioxi
 8.370328
 4.557
 -0.006
 86159600

 4
 NMOC_(ppmv)
 141.417023
 9.724
 0.001
 168183

 BV 3.8 PP 9.3 C PB 18.4 C GR 0.0 ____ ____ _____ Totals: 159.508444 0.038 186965510 Status Codes: C - Out of calibration range Total Unidentified Counts : 780 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: 2 microVolts LSB: 1 microVolts Noise (used): 8 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 00:43: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:28:40 Original Notes: 



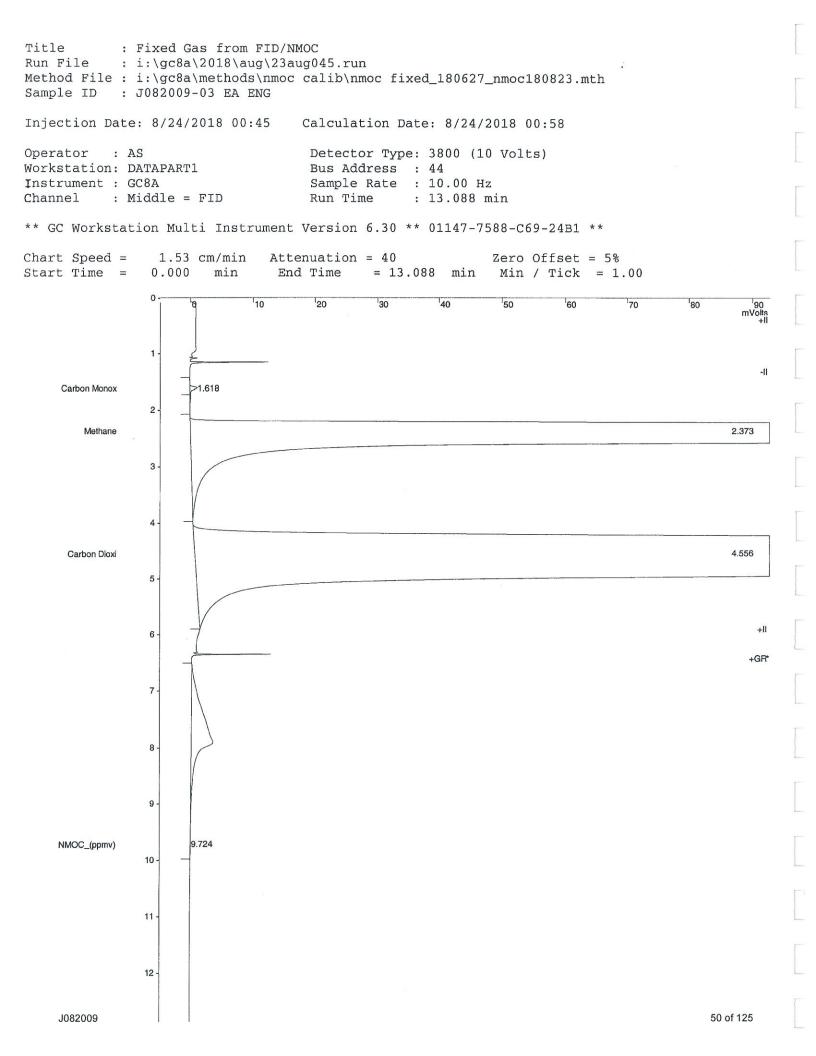
Print Date: Fri Aug 24 00:58:07 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug045.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:45 Calculation Date: 8/24/2018 00:58 Operator : AS Detector Type: 3800 (10 Volts) Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Time Offset Width Peak Result Name (% v/v) Area Sep. 1/2 Area sep. ... (counts) Code (sec) Peak Peak Status (min) (min) No. Codes _____ 
 1
 Hydrogen
 0.251859
 1.896
 -0.034

 2
 Carbon Dioxi
 7.716123
 2.478
 0.033

 3
 Oxygen/Argon
 3.125407
 3.490
 -0.007

 4
 Nitrogen
 10.991739
 4.049
 -0.017

 5
 Methane
 11.022758
 4.972
 -0.025
 60 BB 4.2 60 143652 BB 4.4 BB 4.3 ±3508 169433 7.3 BB 142435 BB 12.4 ____ ____ ----Totals: 33.107886 -0.050 501088 Total Unidentified Counts : 0 counts Detected Peaks: 6 Rejected Peaks: 1 Identified Peaks: 5 Divisor: 1 Multiplier: 1 Unidentified Peak Factor: 0 Baseline Offset: 4 microVolts LSB: 1 microVolts Noise (used): 6 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 00:58: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:43:15 Original Notes: 



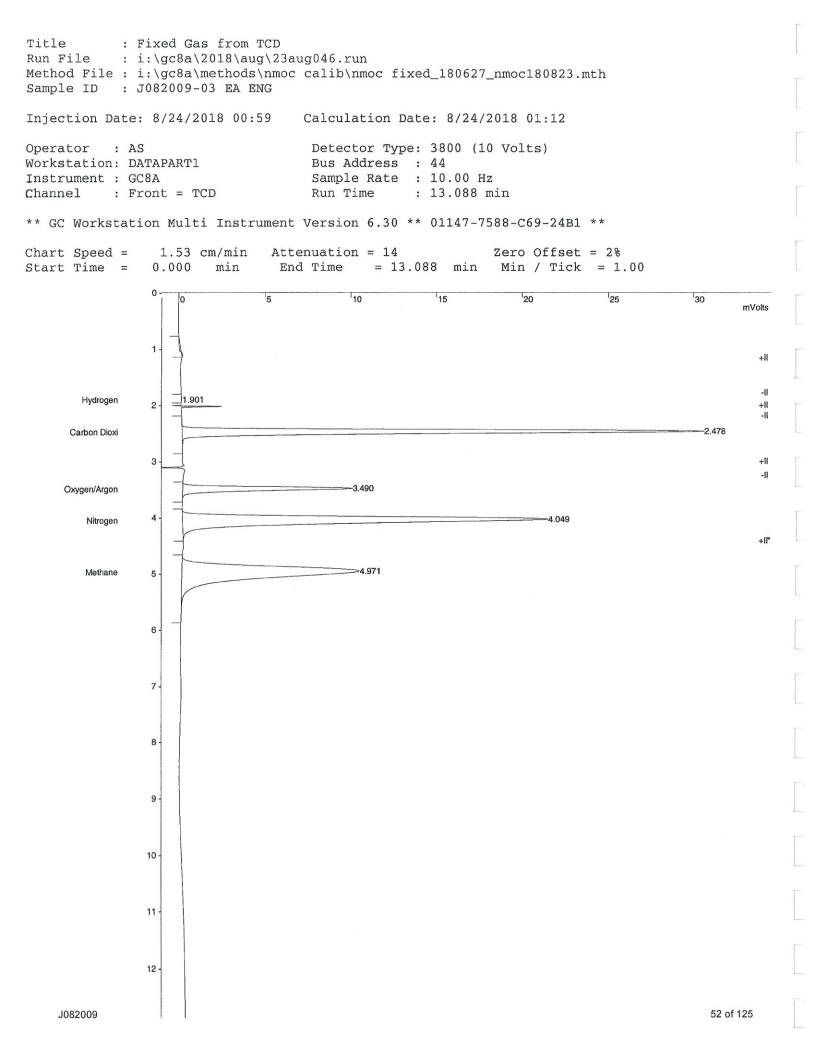
Print Date: Fri Aug 24 00:58:08 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gg?s\2012 Title : i:\gc8a\2018\aug\23aug045.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:45 Calculation Date: 8/24/2018 00:58 Operator : AS Detector Type: 3800 (10 Volts) Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Instrument : GC8A Channel : Middle = FID Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard 

 Ret.
 Time
 Width

 Peak
 Result
 Time
 Offset
 Area
 Sep.
 1/2
 Status

 Name
 (% v/v)
 (min)
 (min)
 (counts)
 Code
 Codes

 Peak Status NO. ____ ____ _____ 1 Carbon Monox0.0004411.6180.04045142 Methane9.7187142.3730.0011006131443 Carbon Dioxi8.3728044.556-0.007861850884 NMOC_(ppmv)141.5370189.7240.001168326 BV 3.7 PP 9.3 C PB 18.4 GR 0.0 18.4 C ____ _____ Totals: 159.628977 0.035 186971072 Status Codes: C - Out of calibration range Total Unidentified Counts : 854 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: Baseline Offset: 2 microVolts 1 microVolts Noise (used): 10 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 00:58: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:43:15 Original Notes: 



Print Date: Fri Aug 24 01:12:47 2018 Page 1 of 1 : Fixed Gas from TCD Title Run File : i:\gc8a\2018\aug\23aug046.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:59 Calculation Date: 8/24/2018 01:12 Operator : AS Detector Type: 3800 (10 Volts) Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A Channel : Front = TCD ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret.TimeWidthResultTimeOffsetAreaSep.1/2(% v/v)(min)(min)(counts)Code(sec) Peak Peak Status Name Codes No. -----1 Hydrogen 0.188295 1.901 -0.029 2 Carbon Dioxi 7.741359 2.478 0.033 45 BB 4.9 45 BB 4.9 144122 BB 4.4 

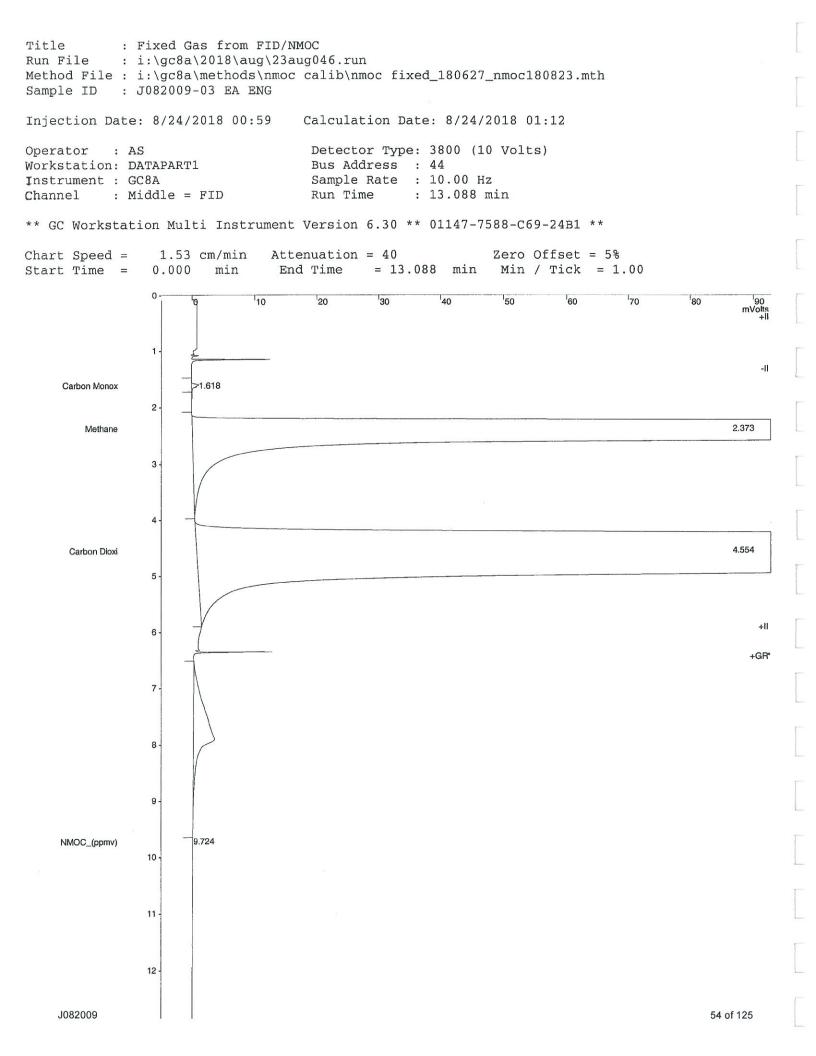
 2 Carbon Dioxi
 7.741333

 3 Oxygen/Argon
 3.124997

 4 Nitrogen
 10.986366

 5 Methane
 11.031891

 4555 169350 2553 BB 4.3 BB 7.3 45502 BB 12.4 142553 --------- ======================= -----33.072908 -0.046 501572 Totals: Total Unidentified Counts : 0 counts Rejected Peaks: 1 Detected Peaks: 6 Identified Peaks: 5 Multiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 Baseline Offset: 0 microVolts LSB: 1 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 01:12: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:57:51 Original Notes: 



Print Date: Fri Aug 24 01:12:48 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC : i:\gc8a\2018\aug\23aug046.run Run File Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-03 EA ENG Injection Date: 8/24/2018 00:59 Calculation Date: 8/24/2018 01:12 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : 13.088 min : Middle = FID Channel Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Width Time Ret. Area Sep. 1/2 Status (counts) Code (sec) Codes Result (% v/v) Time Offset (min) (min) Status Peak Peak (% v/v) No. Name ____ __ _____ ___ ____ 

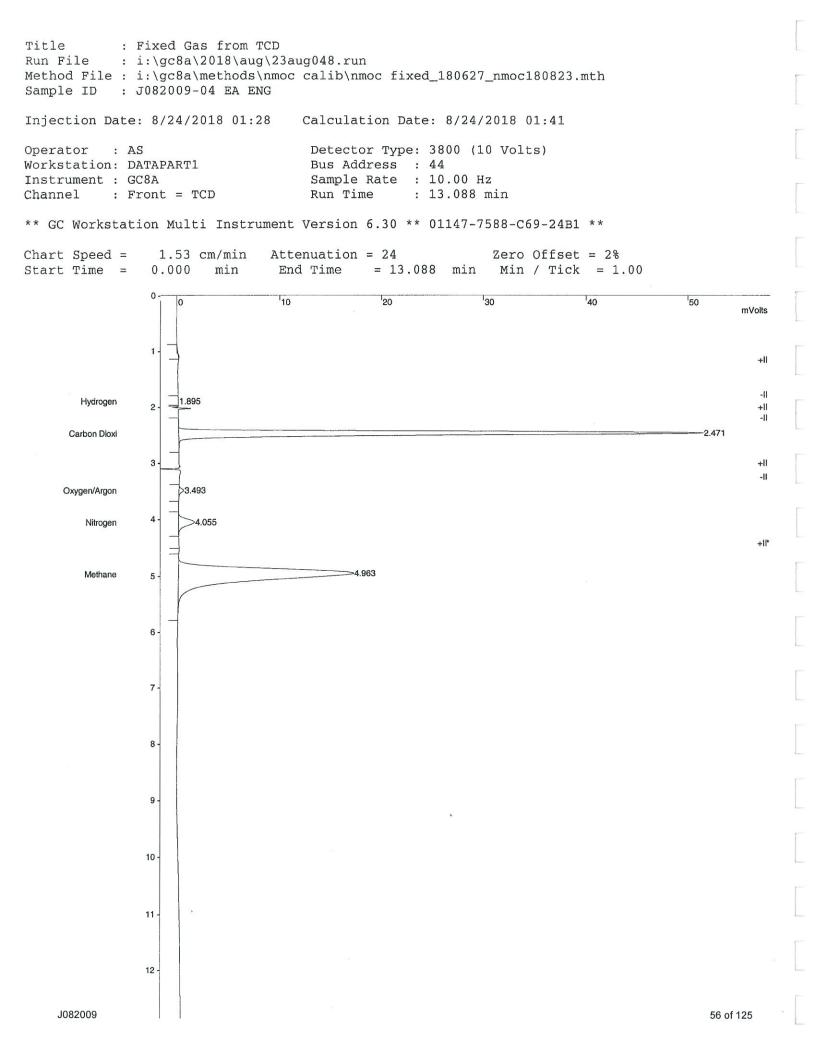
 1.618
 0.040
 4500

 2.373
 0.001
 100647480

 4.554
 -0.009
 86205808

 9.724
 0.001
 166380

 1 Carbon Monox 0.000440 2 Methane 9.722031 BV 3.7 PP 9.3 C 3 Carbon Dioxi 8.374817 PB 18.4 C 4 NMOC_(ppmv) 139.900681 GR 0.0 ---- -----_____ 0.033 187024168 Totals: 157.997969 Status Codes: C - Out of calibration range 837 counts Total Unidentified Counts : Rejected Peaks: 0 Identified Peaks: 4 Detected Peaks: 5 Unidentified Peak Factor: 0 Multiplier: 1 Divisor: 1 LSB: 1 microVolts Baseline Offset: 5 microVolts Noise (used): 8 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 01:12: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 9, Advance Time: 00:57:51 Original Notes: 



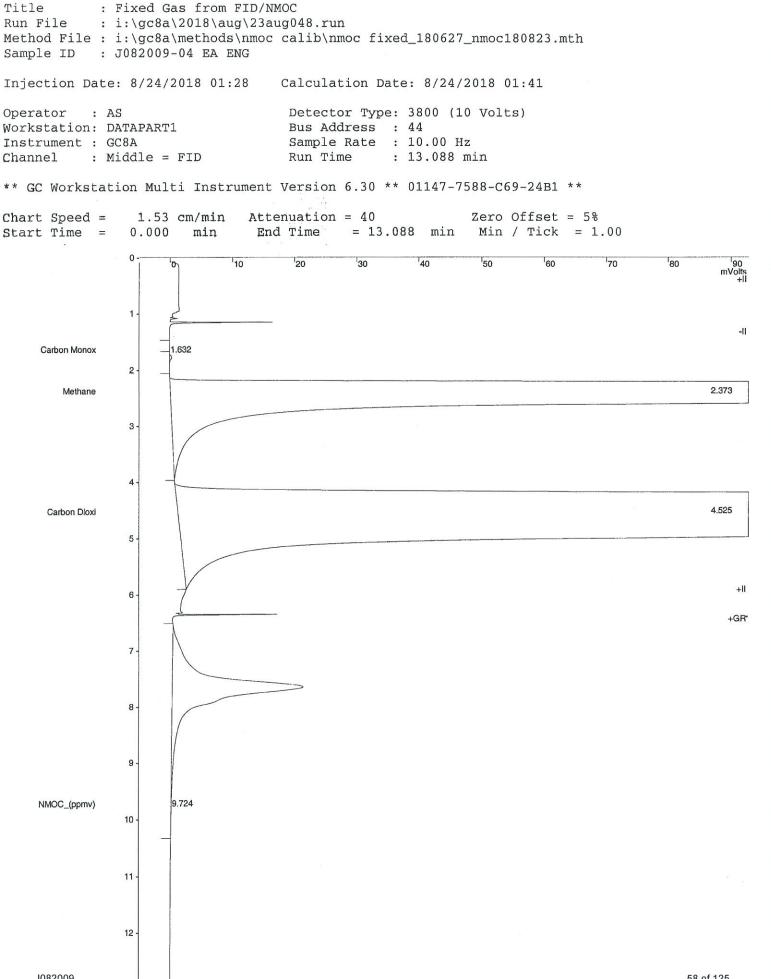
Print Date: Fri Aug 24 01:41:59 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug048.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-04 EA ENG Injection Date: 8/24/2018 01:28 Calculation Date: 8/24/2018 01:41 Detector Type: 3800 (10 Volts) Operator : AS Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Width Time Ret. Ret.TimeWidthPeakResultTimeOffsetAreaSep.1/2Name(% v/v)(min)(min)(counts)Code (sec) Status Peak Peak Codes NO. _____ ____ _ _____ 
 1 Hydrogen
 0.268219
 1.895
 -0.035
 64

 2 Carbon Dioxi
 13.127443
 2.471
 0.026
 244395

 3 Oxygen/Argon
 0.149376
 3.493
 -0.004
 2175

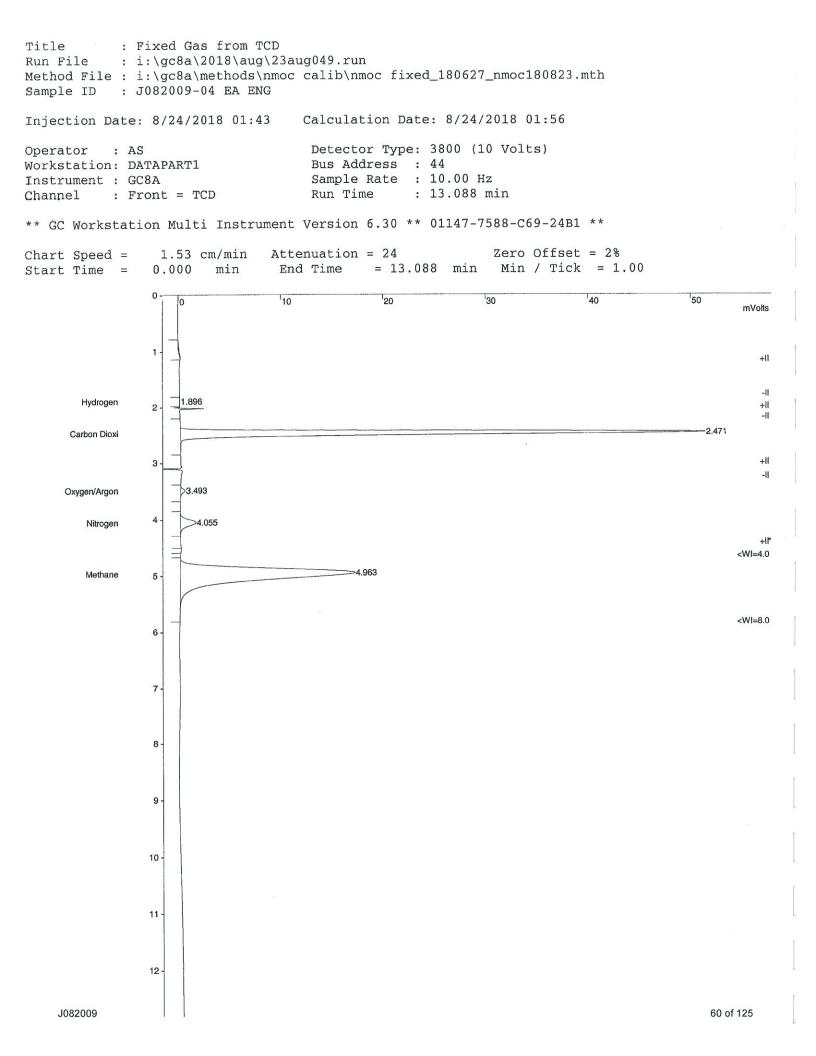
 4 Nitrogen
 0.771755
 4.055
 -0.011
 11896

 5 Methane
 18.307541
 4.963
 -0.034
 236568
 BP 5.5 BB 4.5 BB 4.3 BB 7.3 PB 12.4 _____ ____ ___ Totals: 32.624334 -0.058 495098 27 counts Total Unidentified Counts : Identified Peaks: 5 Rejected Peaks: 2 Detected Peaks: 8 Unidentified Peak Factor: 0 Divisor: 1 Multiplier: 1 Baseline Offset: 6 microVolts LSB: 1 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 01:41: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:27:07 Original Notes: 

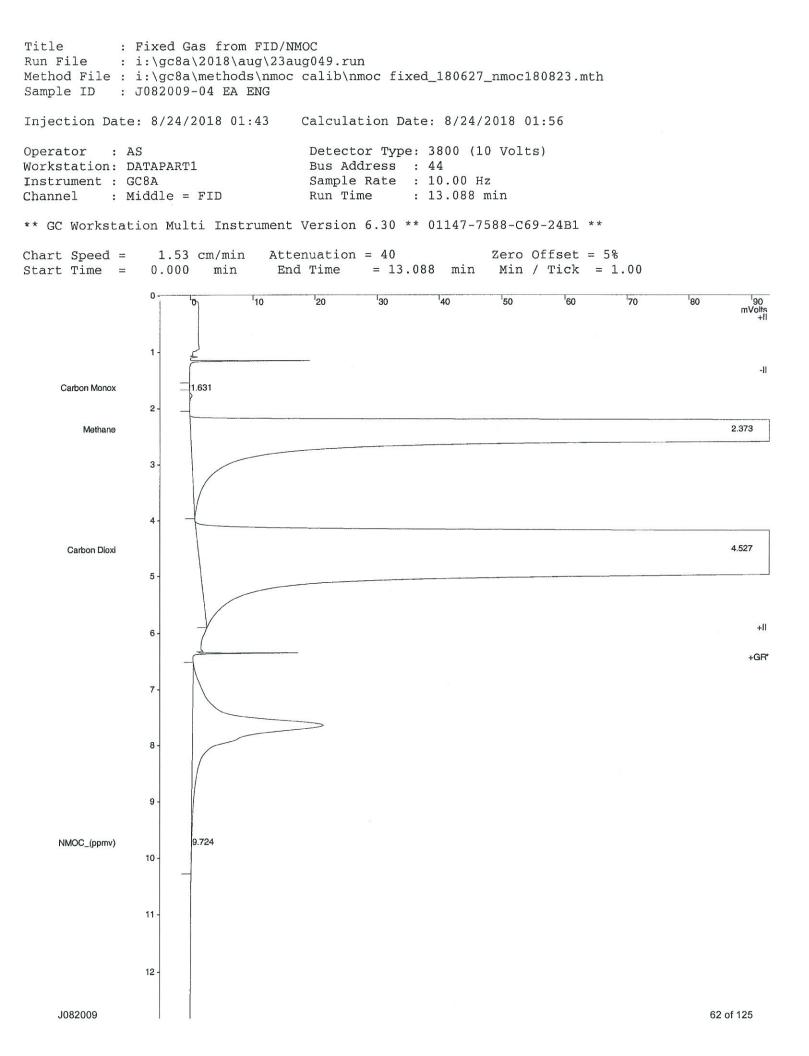


J082009

Print Date: Fri Aug 24 01:41:59 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8c\2010 : i:\gc8a\2018\aug\23aug048.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-04 EA ENG Injection Date: 8/24/2018 01:28 Calculation Date: 8/24/2018 01:41 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A Channel : Middle = FID ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Width Result Time Offset Area Sep. 1/2 Status (% v/v) (min) (min) (counts) Code (sec) Codes Width Status Peak Peak Name NO. 1 632 0 054 151 BV 5 2 ____ _____ 1 Carbon Monox0.0000151.6320.0541512 Methane11.8901012.3730.0011230924643 Carbon Dioxi14.0798674.525-0.0381449304964 NMOC_(ppmv)472.6101389.7240.001562061 BV 5.2 PP 11.5 C PB 18.5 C GR 0.0 C ____ ____ -------_ _ _ _ _ _ 498.580121 0.018 268585172 Totals: Status Codes: C - Out of calibration range Total Unidentified Counts : 1921 counts Rejected Peaks: 0 Identified Peaks: 4 Detected Peaks: 5 Unidentified Peak Factor: 0 Multiplier: 1 Divisor: 1 Baseline Offset: 4 microVolts LSB: 1 microVolts Noise (used): 9 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 01:41: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:27:07 Original Notes: 



Print Date: Fri Aug 24 01:56:34 2018 Page 1 of 1 Title : Fixed Gas from TCD : i:\gc8a\2018\aug\23aug049.run Run File Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-04 EA ENG Injection Date: 8/24/2018 01:43 Calculation Date: 8/24/2018 01:56 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A : Front = TCD Channel ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Width Time Ret. Ret. Time Width Peak Peak Result Time Offset Area Sep. 1/2 Status No. Name (% v/v) (min) (min) (counts) Code (sec) Codes Status Peak 1 Hydrogen0.1971521.896-0.03447BB4.12 Carbon Dioxi13.0821822.4710.026243552BB4.53 Oxygen/Argon0.1435593.493-0.0042090BB4.34 Nitrogen0.7526074.055-0.01111601BB7.45 Methane18.2831124.963-0.034236252BB12.4 4 Nitrogen 0.752607 5 Mothane 18.283112 ____ ____ -----Totals: 32.458612 -0.057 493542 Total Unidentified Counts : / J7/-43 counts Identified Peaks: 5 Rejected Peaks: 1 Detected Peaks: 7 Unidentified Peak Factor: 0 Divisor: 1 Multiplier: 1 1 microVolts Baseline Offset: -1 microVolts LSB: Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 01:56: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:41:44 Original Notes: 



Print Date: Fri Aug 24 01:56:35 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug049.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-04 EA ENG Injection Date: 8/24/2018 01:43 Calculation Date: 8/24/2018 01:56 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : Middle = FID Run Time : 13.088 min Channel ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. Time Peak Result Name (% v/v) Time Offset Area Sep. 1/2 Status (min) (min) (counts) Code (sec) Codes Area Sep. 1/2 Status Peak No. _____ ____ -----_ _ _ _ _ _ ---------- 

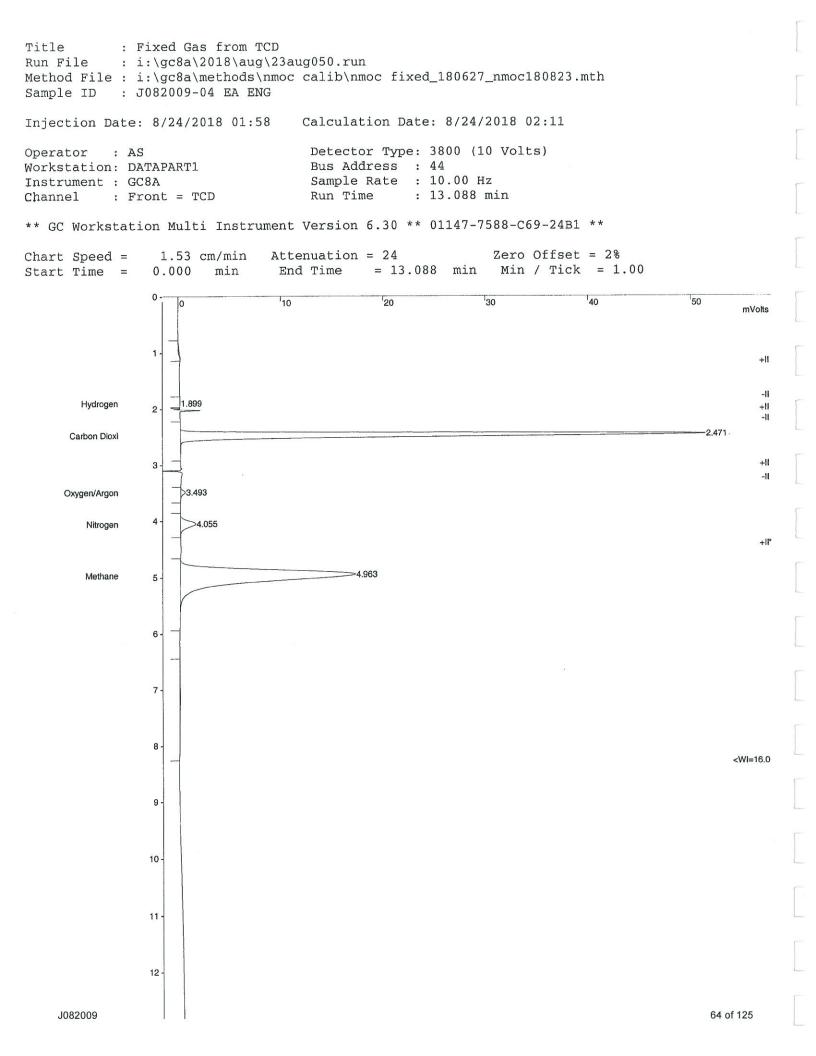
 1 Carbon Monox
 0.000014
 1.631
 0.053
 139

 2 Methane
 11.889049
 2.373
 0.001
 123081568

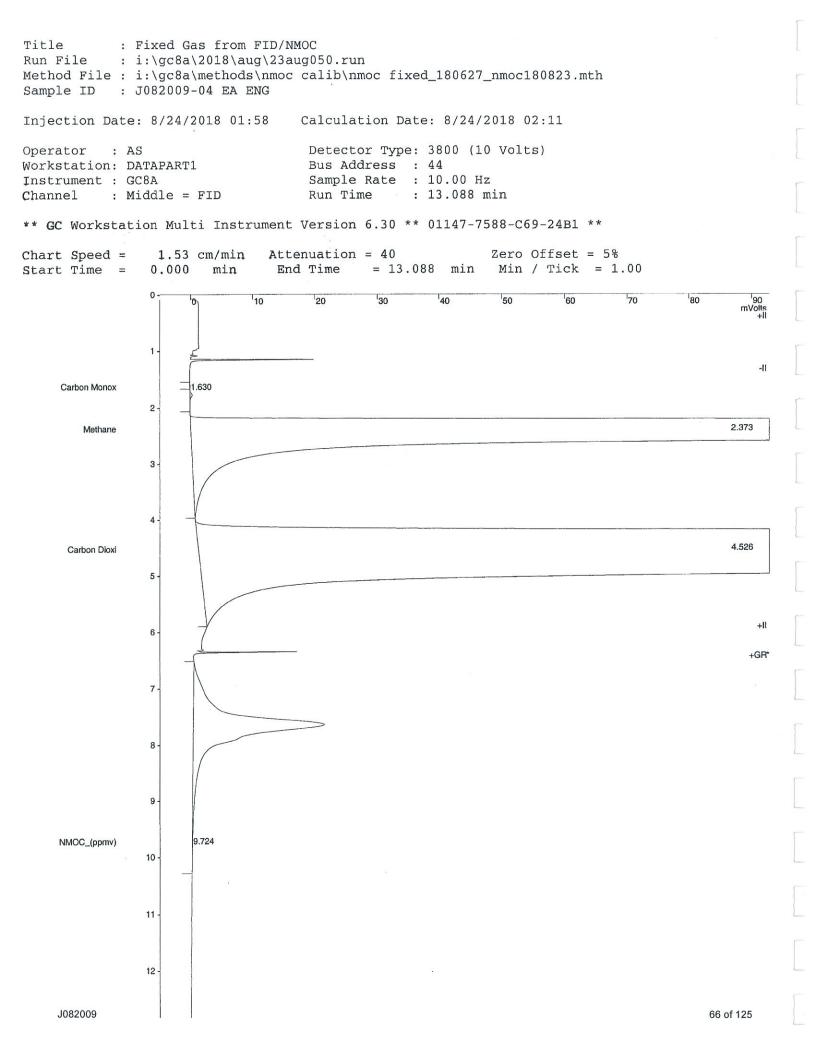
 3 Carbon Dioxi
 14.078229
 4.527
 -0.036
 144913632

 4 NMOC_(ppmv)
 472.710205
 9.724
 0.001
 562180

 BV 4.5 PP 11.5 C PB 18.5 C GR 0.0 C ----____ ----- =========== ____ Totals: 498.677497 0.019 268557519 Status Codes: C - Out of calibration range Total Unidentified Counts : 1928 counts Identified Peaks: 4 Detected Peaks: 5 Rejected Peaks: 0 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 LSB: 1 microVolts Baseline Offset: -3 microVolts Noise (used): 11 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 01:56: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:41:44 Original Notes: 



Print Date: Fri Aug 24 02:11:10 2018 Page 1 of 1 : Fixed Gas from TCD Title Run File : i:\gc8a\2018\aug\23aug050.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth : J082009-04 EA ENG Sample ID Injection Date: 8/24/2018 01:58 Calculation Date: 8/24/2018 02:11 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A Channel : Front = TCD Run Time ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. Time Width Peak Result Time Offset Area Sep. 1/2 Status Name (% v/v) (min) (min) (counts) Code (sec) Codes Status Peak NO. _____ ____ 1 Hydrogen0.2479411.899-0.03159BP4.42 Carbon Dioxi13.0976722.4710.026243841BB4.53 Oxygen/Argon0.1431363.493-0.0042084BB4.34 Nitrogen0.7492634.055-0.01111550BB7.35 Methane18.3083294.963-0.034236578BB12.4 ----____ ____ _ _ _ _ _ _ 494112 Totals: 32.546341 -0.054 3660 counts Total Unidentified Counts : Identified Peaks: 5 Rejected Peaks: 2 Detected Peaks: 8 Unidentified Peak Factor: 0 Divisor: 1 Multiplier: 1 LSB: 1 microVolts Baseline Offset: 0 microVolts Noise (used): 5 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 02:11: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:56:19 Original Notes: 



Print Date: Fri Aug 24 02:11:10 2018 Page 1 of 1 : Fixed Gas from FID/NMOC Title Run File : i:\gc8a\2018\aug\23aug050.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-04 EA ENG Injection Date: 8/24/2018 01:58 Calculation Date: 8/24/2018 02:11 Detector Type: 3800 (10 Volts) : AS Operator Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Instrument : GC8A Run Time Channel : Middle = FID ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Width 

 Ket.
 Time
 Width

 Peak
 Result
 Time
 Offset
 Area
 Sep.
 1/2
 Status

 Name
 (% v/v)
 (min)
 (min)
 (counts)
 Code
 Codes

 Shon
 Monox
 0.000015
 1.000
 Code
 Codes

 Status Peak No. ____ _______ 

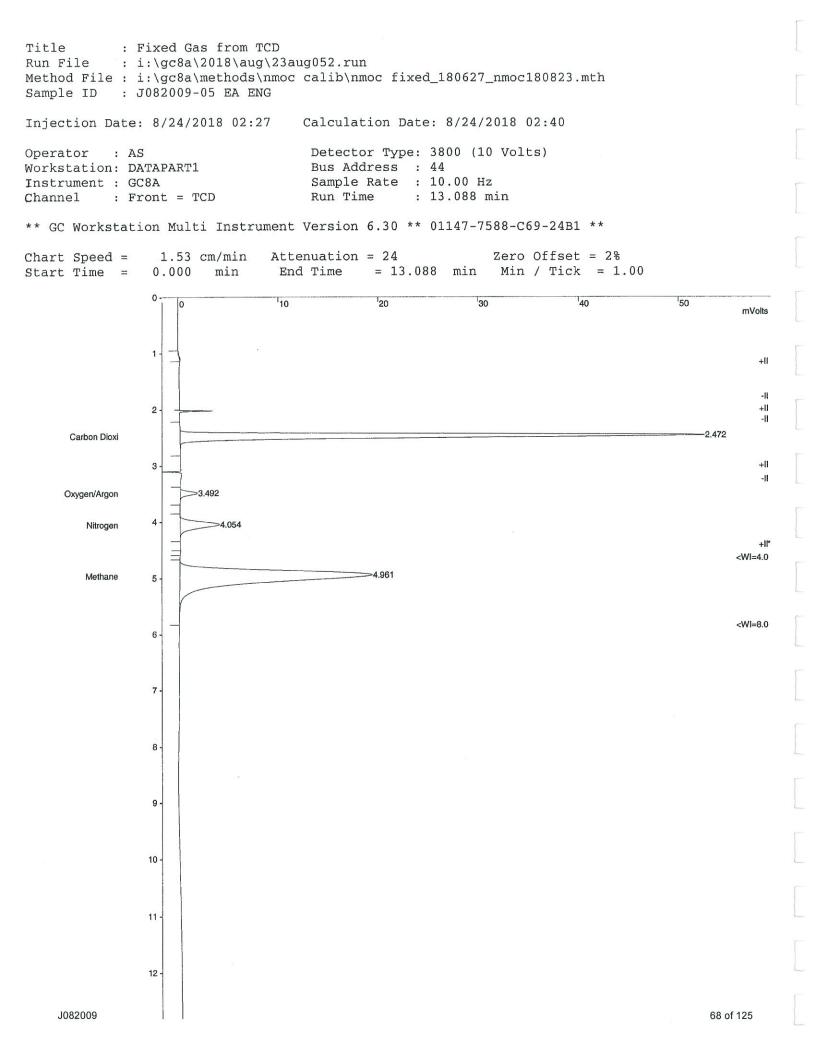
 1
 Carbon Monox
 0.000015
 1.630
 0.052
 153

 2
 Methane
 11.894177
 2.373
 0.001
 123134664

 3
 Carbon Dioxi
 14.086224
 4.526
 -0.037
 144995920

 4
 NMOC_(ppmv)
 472.500244
 9.724
 0.001
 561930

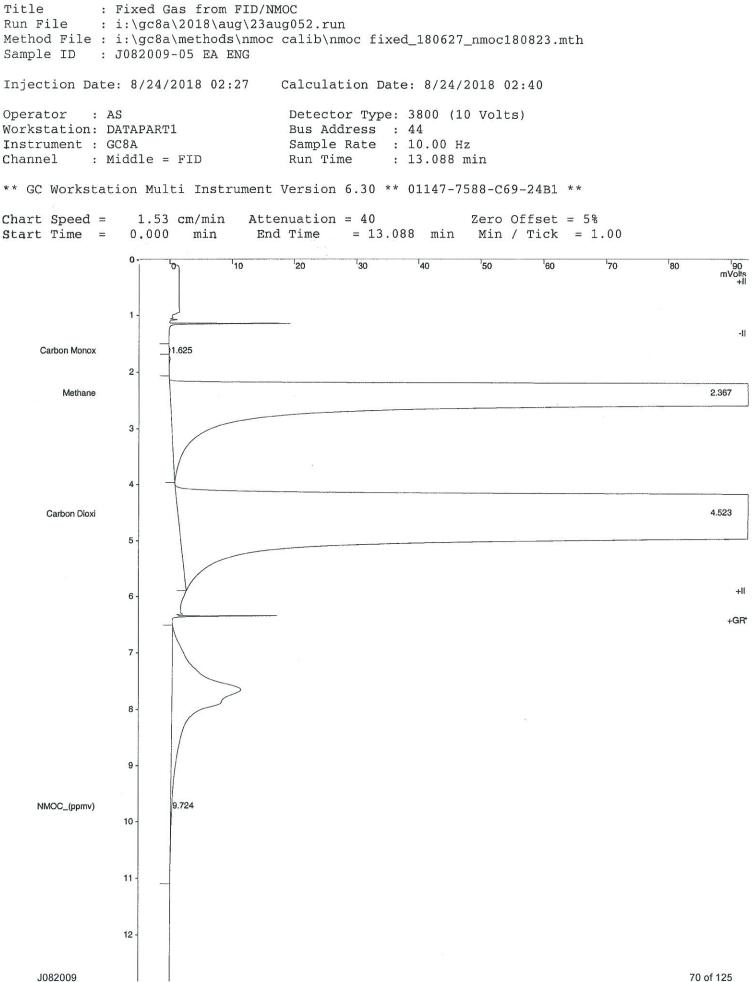
 BV 4.5 PP 11.5 C PB 18.5 C GR 0.0 C ____ _ ____ 498.480660 0.017 268692667 Totals: Status Codes: C - Out of calibration range Total Unidentified Counts : 1913 counts Rejected Peaks: 0 Identified Peaks: 4 Detected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 Multiplier: 1 LSB: 1 microVolts Baseline Offset: -7 microVolts Noise (used): 10 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 02:11: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 10, Advance Time: 01:56:19 Original Notes: 



Print Date: Fri Aug 24 02:40:21 2018 Page 1 of 1 Title : Fixed Gas from TCD : i:\gc8a\2018\aug\23aug052.run Run File Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-05 EA ENG Injection Date: 8/24/2018 02:27 Calculation Date: 8/24/2018 02:40 Detector Type: 3800 (10 Volts) : AS Operator Bus Address : 44 Workstation: DATAPART1 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Front = TCD Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Time Width Ret. Area Sep. 1/2 Offset Peak Result Time Status Peak (counts) Code (sec) No. Name (8 v/v) (min) (min) Codes ___ _____ -----____ ____ ____ 1.930 1 Hydrogen М 2 Carbon Dioxi 13.393999 3 Oxygen/Argon 0.553435 2.472 0.027 249357 BB 4.5 8058 3.492 -0.005 BB 4.3 
 3 Uxygen.

 4 Nitrogen
 2.035.1

 20.614388
 4.054 -0.012 4.961 -0.036 2.033714 31349 BB 7.3 BB 12.4 266377 ----- -----____ ___ Totals: 36.595536 -0.026 555141 129 Status Codes: M - Missing peak 282 counts Total Unidentified Counts : Detected Peaks: 6 Rejected Peaks: 0 Identified Peaks: 5 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -1 microVolts LSB: 1 microVolts Noise (used): 7 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 02:40: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:25:30 Original Notes: 



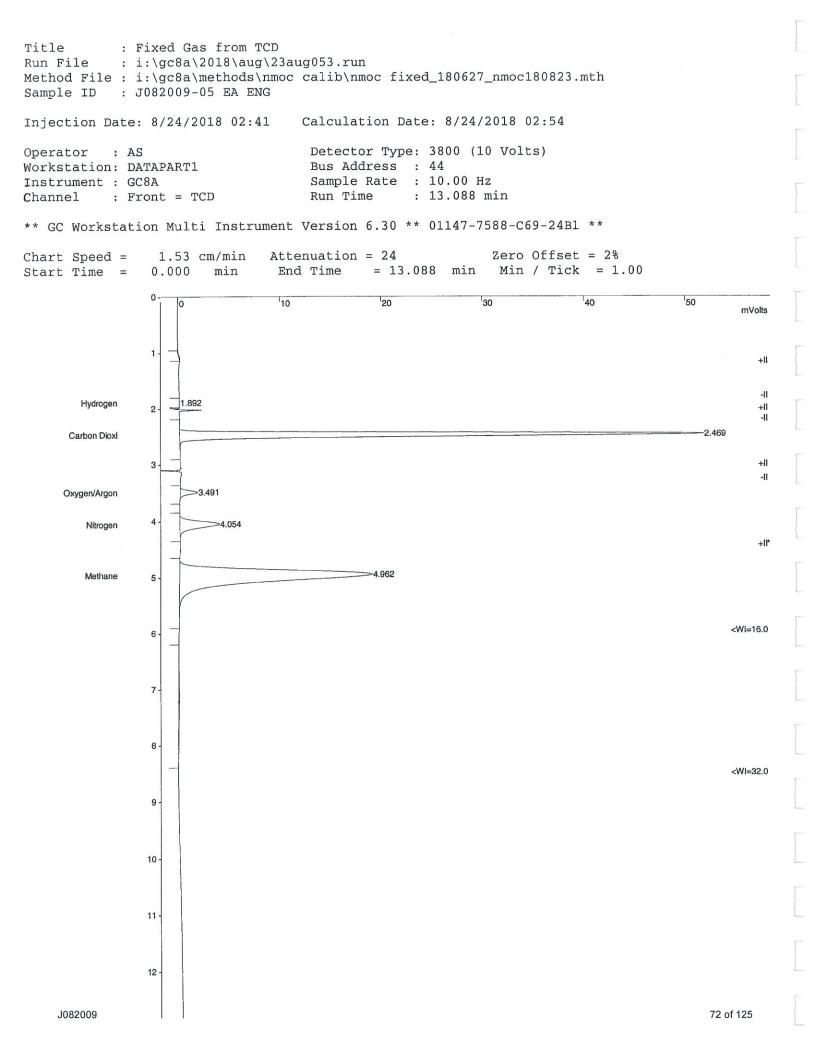
⁷⁰ of 125

Print Date: Fri Aug 24 02:40:22 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug052.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-05 EA ENG Injection Date: 8/24/2018 02:27 Calculation Date: 8/24/2018 02:40 : AS Detector Type: 3800 (10 Volts) Operator Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A Channel : Middle = FID Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Width Ret. Time Width Peak Result Time Offset Area Sep. 1/2 Name (% v/v) (min) (min) (counts) Code (sec) Status Peak Codes No. ---------____ ____ ____ 
 1
 Carbon Monox
 0.000066
 1.625
 0.047
 672

 2
 Methane
 12.357107
 2.367
 -0.005
 127927152

 3
 Carbon Dioxi
 14.399894
 4.523
 -0.041
 148224672

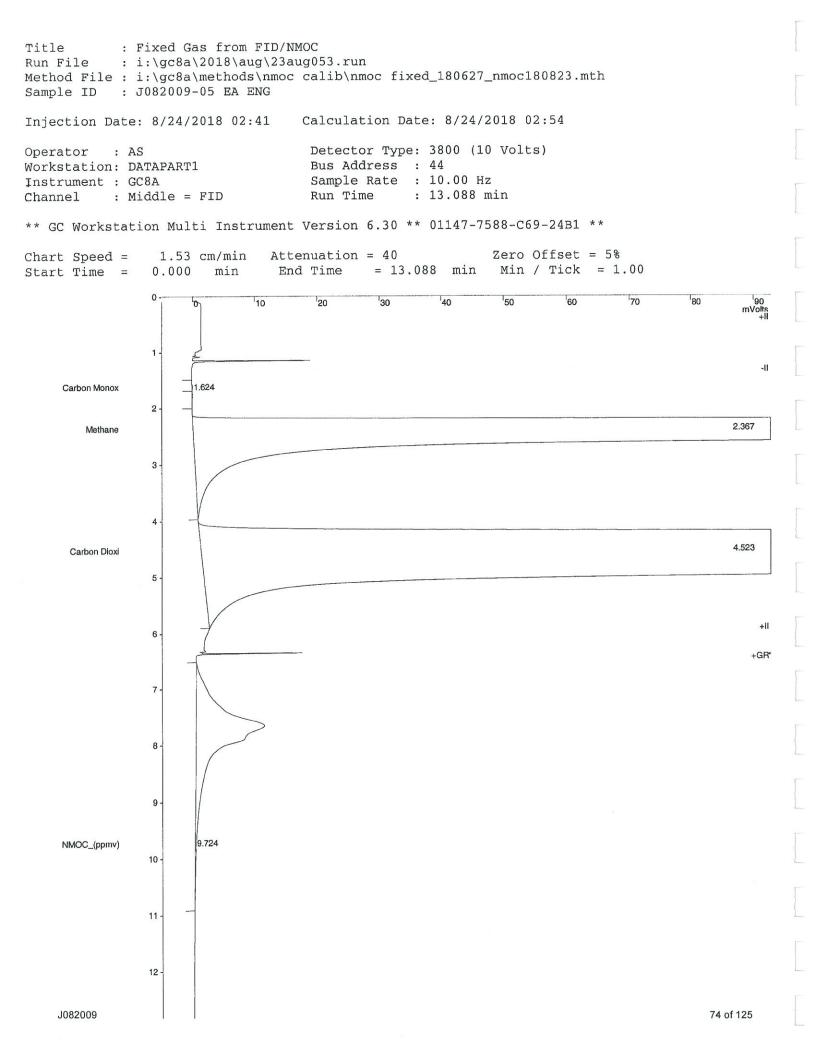
 4
 NMOC_(ppmv)
 433.891449
 9.724
 0.001
 516014
 BV 3.8 PP 12.0 C PB 18.6 C 4 NMOC_(ppmv) 433.891449 9.724 0.001 516014 GR 0.0 C _____ Totals: 460.648516 0.002 276668510 Status Codes: C - Out of calibration range Total Unidentified Counts : 971 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -6 microVolts LSB: 1 microVolts Noise (used): 11 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 02:40: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:25:30 Original Notes: 



Print Date: Fri Aug 24 02:54:57 2018 Page 1 of 1 : Fixed Gas from TCD Title Run File : i:\gc8a\2018\aug\23aug053.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-05 EA ENG Injection Date: 8/24/2018 02:41 Calculation Date: 8/24/2018 02:54 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A : Front = TCDChannel ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Ret. Time Width Ret. Time Width Result Time Offset Area Sep. 1/2 Status (% v/v) (min) (min) (counts) Code (sec) Codes Status Peak Peak No. Name 1 Hydrogen 0.240271 1.892 -0.038 2 Carbon Dioxi 13.194273 2.469 0.024 BP 4.6 BB 4.5 58 245639 
 3
 Oxygen/Argon
 0.539498
 3.491
 -0.006
 7855

 4
 Nitrogen
 1.983487
 4.054
 -0.012
 30575

 5
 Methane
 20.368279
 4.962
 -0.036
 263197
 BB 4.3 BB 7.3 BB 12.4 ----- ----- ----- -----547324 -0.068 Totals: 36.325808 Total Unidentified Counts : 4818 counts Rejected Peaks: 1 Identified Peaks: 5 Detected Peaks: 8 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 LSB: 1 microVolts Baseline Offset: 0 microVolts Noise (used): 6 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 02:54: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:40:06 Original Notes: 

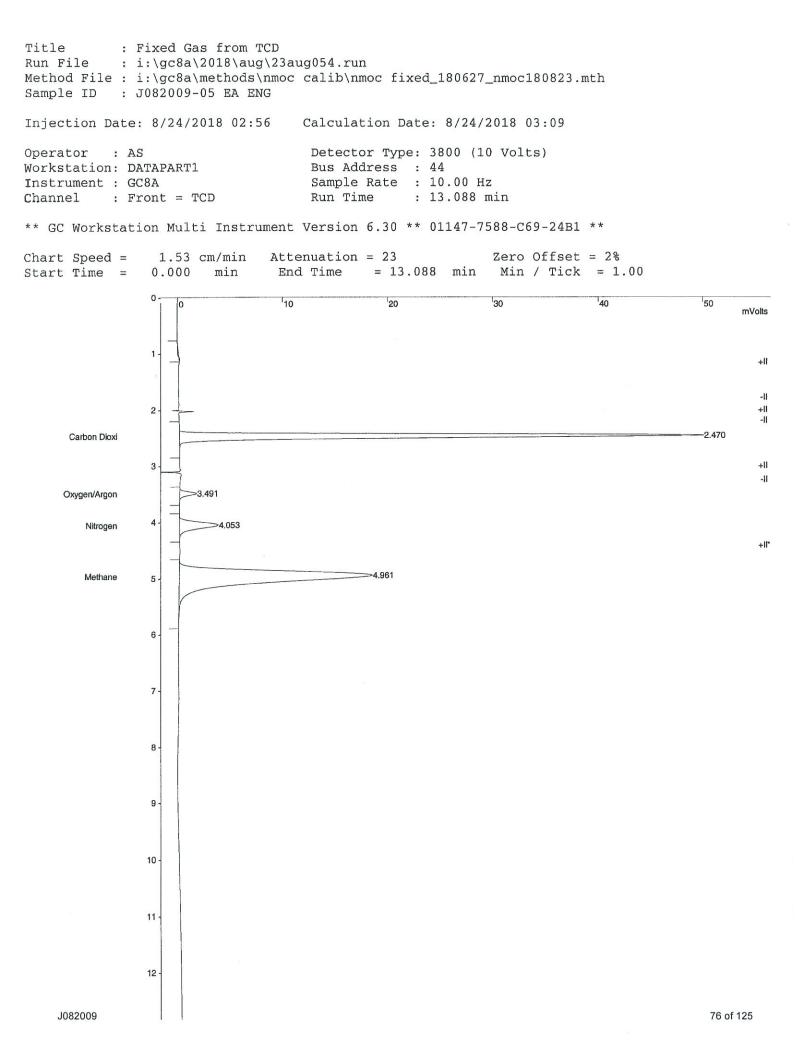


Print Date: Fri Aug 24 02:54:58 2018 Page 1 of 1 Title : Fixed Gas from FID/NMOC Run File : i:\gc8a\2018\aug\23aug053.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-05 EA ENG Injection Date: 8/24/2018 02:41 Calculation Date: 8/24/2018 02:54 Detector Type: 3800 (10 Volts) Operator : AS Workstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz Instrument : GC8A : Middle = FID Run Time : 13.088 min Channel ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis Run Mode Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. Time Time Offset Area Sep. 1/2 (min) (min) (counts) Code (sec) Area Sep. 1/2 Peak Result Name (% v/v) Result Status Peak Codes No. ____ ___ ____ ____ _____ 
 1 Carbon Monox
 0.000070
 1.624
 0.046
 712

 2 Methane
 12.349093
 2.367
 -0.005
 127844192

 3 Carbon Dioxi
 14.379933
 4.523
 -0.040
 148019216

 4 NMOC_(ppmv)
 432.666901
 9.724
 0.001
 514558
 BV 712 3.8 PP 12.0 C PB 18.6 C 514558 GR 0.0 C _____ _ _ _ _ _ _ Totals: 459.395997 0.002 276378678 Status Codes: C - Out of calibration range Total Unidentified Counts : 886 counts Detected Peaks: 5 Rejected Peaks: 0 Identified Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -8 microVolts LSB: 1 microVolts Noise (used): 8 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 02:54: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:40:06 Original Notes: 



Print Date: Fri Aug 24 03:09:32 2018 Page 1 of 1 Title : Fixed Gas from TCD Run File : i:\gc8a\2018\aug\23aug054.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth : J082009-05 EA ENG Sample ID Injection Date: 8/24/2018 02:56 Calculation Date: 8/24/2018 03:09 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Workstation: DATAPART1 Instrument : GC8A : Front = TCD Channel Run Time : 13.088 min ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. Time Result Time Offset Area Sep. 1/2 (% v/v) (min) (min) (counts) Code (sec) Area Sep. 1/2 Status Peak Peak Codes (% v/v) No. Name 1.930 M 1 Hydrogen 

 1 Hydrogen
 2.173

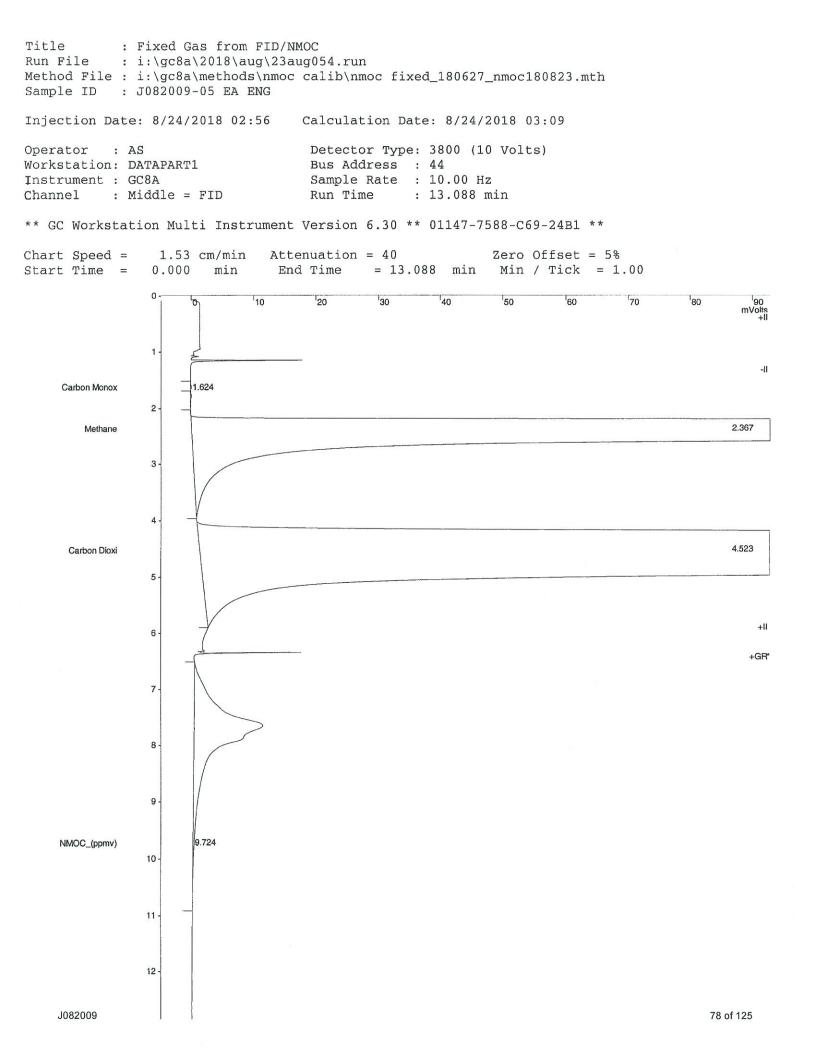
 2 Carbon Dioxi
 12.739395
 2.470
 0.025
 237171

 3 Oxygen/Argon
 0.513296
 3.491
 -0.006
 7474

 4 Nitrogen
 1.883909
 4.053
 -0.013
 29040

 5 Methane
 19.651237
 4.961
 -0.036
 253931

 BB 4.5 BB 4.3 BB 7.3 BB 12.4 ____ ___ -----34.787837 -0.030 527616 Totals: Status Codes: M - Missing peak 0 counts Total Unidentified Counts : Rejected Peaks: 1 Identified Peaks: 5 Detected Peaks: 5 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 LSB: 1 microVolts Baseline Offset: -2 microVolts Noise (used): 6 microVolts - monitored before this run Manual injection Revision Log: 8/24/2018 03:09: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:54:41 Original Notes: 



Print Date: Fri Aug 24 03:09:33 2018 Page 1 of 1 : Fixed Gas from FID/NMOC Title Run File : i:\gc8a\2018\aug\23aug054.run Method File : i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth Sample ID : J082009-05 EA ENG Injection Date: 8/24/2018 02:56 Calculation Date: 8/24/2018 03:09 Detector Type: 3800 (10 Volts) Operator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min Workstation: DATAPART1 Instrument : GC8A Channel : Middle = FID ** GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Run Mode : Analysis Peak Measurement: Peak Area Calculation Type: External Standard Width Ret. Time Ret. Time Width Result Time Offset Area Sep. 1/2 Status (% v/v) (min) (min) (counts) Code (sec) Codes Status Peak Peak No. Name 1 Carbon Monox0.0000721.6240.0467392 Methane12.3492532.367-0.0051278458323 Carbon Dioxi14.3646014.523-0.0401478613924 NMOC_(ppmv)433.5094609.7240.001515560 BV 3.9 PP 12.0 C PB 18.6 С GR 0.0 C ____ ____ _____ ____ _ 460.223386 0.002 276223523 Totals: Status Codes: C - Out of calibration range 938 counts Total Unidentified Counts : Rejected Peaks: 0 Identified Peaks: 4 Detected Peaks: 5 Divisor: 1 Unidentified Peak Factor: 0 Multiplier: 1 Baseline Offset: -10 microVolts LSB: 1 microVolts Noise (used): 6 microVolts - monitored before this run Manual injection Calib. out of range; No Recovery Action Specified Revision Log: 8/24/2018 03:09: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc calib\nmoc fixed_180627_nmoc180823.mth' Stream: 11, Advance Time: 02:54:41 Original Notes: 

## 3. Initial Calibration

a. ICAL Summaryb. Chromatograms/Results

Form-15 Rev. 2 \\AIRTECH-SERVER\Shared Folders\Company\QA\Forms\GC Raw Data Pkg Dividers Rev2.doc

QA Manager 10/2016

				Edit Codes						
08:53:08				Cal. No. of Range Points	ked ked ked ked					
Page 1 05 Jul 2018 08:53:08	3800 GC 44 Front	8/29/2016 14:10		لا	+9.9632e-001 +9.9999e-001 +9.9999e-001 +9.9999e-001 +9.9999e-001					
		•		O	<ul> <li>4.0.0000</li> <li>4.0.0000</li> <li>4.0.0000</li> <li>4.0.0000</li> <li>4.0.0000</li> <li>4.0.000</li> <li>4.0.000<!--</td--><td></td><td>r.</td><td>б</td><td>ũ</td><td>σ</td></li></ul>		r.	б	ũ	σ
ъt	Method Detector Type Method Bus Address Method Channel	Last Recalculation Date	*****	×	+2.3992e+002 +1.8617e+004 +1.4561e+004 +1.5415e+004 +1.2922e+004		Peak Measurement: Area Curve\Origin: 1 F Std. Dev. 5 # 1 # 8 # 1 # 4 #	Peak Measurement: Area Curve\Origin: 1 F Std. Dev. 4 # 8 # 8 # 8 # 8	Peak Measurement: Area Curve\Origin: 1 F Std. Dev. 6 # 8 # 8 # 8 #	Peak Measurement: Area Curve\Origin: 1 F \$td. Dev. 0 # 8 #
Calibration Block Report Nairtech-servervinsdata\gc8a\methods\nmoc fixed_180627.mth 7/5/2018 08:22			J0***********************	X²		Edit Codes 	Avg. Response 295. 1 1359 1918. 8 2585 5822	Avg. Response 8929. 85990. 910185. 1872540.	Avg. Response 7781. 32431. 158696. 318801.	Avg. Response 29017. 122900.
Calibration Block Report Nairtech-servervinsdata\gc8a\meth 7/5/2018 08:22	linear force External Standard Analysis	3 15:28	****************Version 6.3	×3		n Codes 	Locked Response 295 1359 1919 2585 5822	Locked Response 8929 85991 464867 910186 1872541	Locked Response 7782 32432 158697 318802	Locked Response 29017 122901
: Calibration Bloc : Nairtech-server : 7/5/2018 08:22	: linear : force : External S	: 8/12/2016 15:28	n Multi Instrument****	Curve\ Origin	<u> </u>	Origin Codes  I include IG ignore F force	Replicate No.	Replicate No.	Replicate No.	Replicate No. 1
Rood File 3000 File 3000 Time	utested Curve Type quested Origin ibration Type	Ibration Dates st Injection Date	*******************GC Workstation Multi Instrument************************************	tention Peak ne (min) Name	<ol> <li>930 Hydrogen</li> <li>445 Carbon Dioxide</li> <li>456 Oxygen/Argon</li> <li>933 Nitrogen</li> <li>997 Methane</li> </ol>	Curve Codes 	t. Time: 1.930 min. ak Name: Hydrogen vel Amount 1 1. 000000 2 7. 000000 3 7. 000000 4 10. 000000 5 25. 000000	tt. Time: 2.445 min. ak Name: Carbon Dioxide vel Amount 0. 500000 2 5. 000000 3 25. 000000 4 50. 000000 6 100. 000000	it. Time: 3.456 min. iak Name: Oxygen/Argon vel Amount 0.438000 2.190000 3.10.900000 4.21.900000	1. Time: 3.933 min. 2월k Name: Nitrogen 오테 Amount 1. 560000 전 7. 810000 t Date: 05 Jul 2018 08:53:09

* * * *	rement: Area :: 1 F Std. Dev. # # #	
604517.1 1202734.9 1541320.4 19878.5	Peak Measurement: Area Curve\Origin: 1 F Curve\Origin: 1 F Std. Dev. 6182. 6 60995. 7 321422. 2 639578. 3 1296034. 5 #	
604517 1202735 1541320 19879	Locked Response 6183 60996 321422 639578 1296035	
* = = =	Replicate No.	
39.099998 78.099998 100.000000	Time: 4.997 min. k Name: Methane el Amount 1 0. 500000 2 5. 000000 3 25. 000000 4 50. 000000 5 100. 000000 5 Too few points to calculate.	
പക്ടമാന്ത	. Time: 4.997 min. ik Name: Methane el Amour 1 0 0. 2 5 5 3 25 4 50 0 5 1000. Too few points to c	

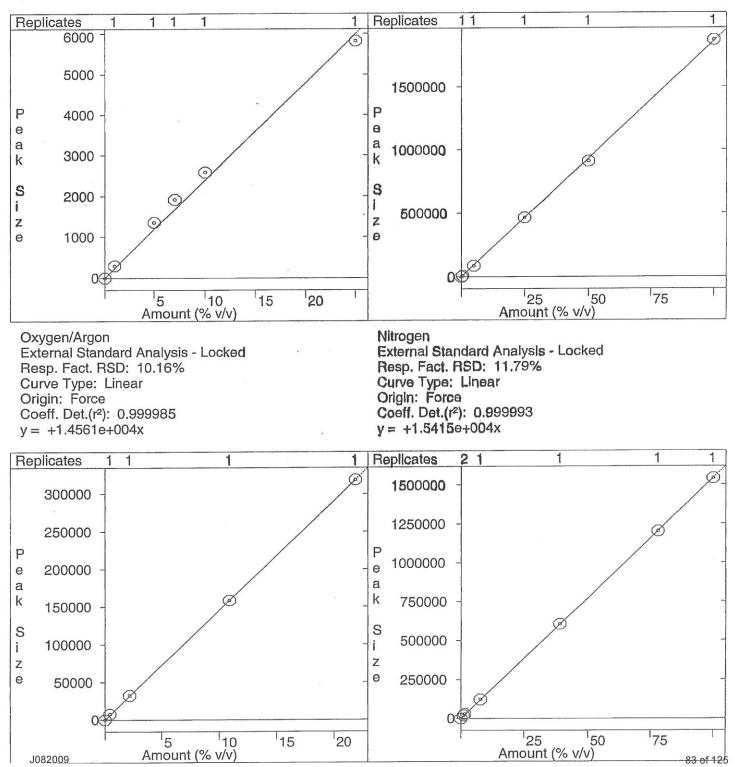
5 100.00000	-	F	1296035 12	1296034.5 #	
Too few points to calculate.					
ak Name	Level	Rep.	Injection Date Time	Run Files	
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ingen	ן - כ	- •			
	ZL	-	CC1 01 07/11/1		
	3 L	-	7/11/2016 15:47	c:\temp gc\gc8a\2016\jul\11jul013.run	
	4 L	-	7/11/2016 16:02	c:\temp gc\gc8a\2016\jul\11jul014.run	
	5 L		7/11/2016 16:31	c:\temp gc\gc8a\2016\jul\11jul016.run	
rbon Dioxide	11	-	7/11/2016 13:11	c:\temp gc\gc8a\2016\jul\11jul004.run	
	2 L	-	7/11/2016 13:57	c:\temp gc\gc8a\2016\jul\11jul006.run	
	3 L	-	7/11/2016 14:12	c:\temp gc\gc8a\2016\jul\11jul007.run	
	4 L	<b>,</b>	7/11/2016 14:26	c:\temp gc\gc8a\2016\jul\11jul008.run	
	5 L	-	7/11/2016 14:41	c:\temp gc\gc8a\2016\jul\11jul009.run	
ygen/Argon		-	7/11/2016 15:18	c:\temp gc\gc8a\2016\jul\11jul011.run	
	2 L	÷	7/11/2016 15:33	c:\temp gc\gc8a\2016\jul\11jul012.run	
	3 L		7/11/2016 15:47	c:\temp gc\gc8a\2016\jul\11jul013.run	
	4 L	-	7/11/2016 16:17	c:\temp gc\gc8a\2016\ju\\11jul015.run	
rogen	1 L	-	7/11/2016 15:18	c:\temp gc\gc8a\2016\jul\11jul011.run	
	2 L	-	7/11/2016 15:33	c:\temp gc\gc8a\2016\jul\11jul012.run	
	3 L	-	7/11/2016 15:47	c: temp gc/gc8a/2016/jul/11jul013.run	
	4 L	-	7/11/2016 16:17	c: temp gc/gc8a/2016/jul/11jul015.run	
	5 L		7/11/2016 16:46	c:\temp gc\gc8a\2016\jul\11jul017.run	
	6 L	-	8/12/2016 15:28	c:\temp gc\gc8a\2016\aug\12aug027.run	
thane	1 L	-	7/11/2016 13:11	c:\temp gc\gc8a\2016\jul\11jul004.run	
	2 L	-	7/11/2016 13:57	c:\temp gc\gc8a\2016\jul\11jul006.run	
121	3 L	-	7/11/2016 14:12	c:\temp gc\gc8a\2016\jul\11jul007.run	
	4 L	•	7/11/2016 14:26	c:\temp gc\gc8a\2016\jul\11jul008.run	
	5 L	-	7/11/2016 14:56	c:\temp gc\gc8a\2016\jul\11jul010.run	
. I acked Coefficients					

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: Locked Coefficients

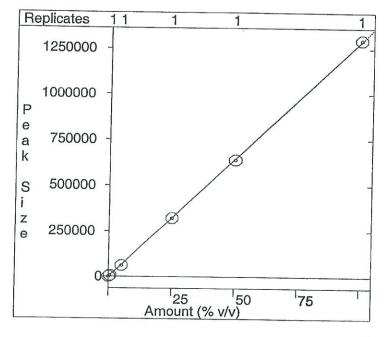
Print Date: 05 Jul 2018 08:53:10 Calibration Curves Report - Page 1 File: \\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth Detector: 3800 GC, Address: 44, Channel ID: Front

Hydrogen External Standard Analysis - Locked Resp. Fact. RSD: 8.632% Curve Type: Linear Origin: Force Coeff. Det.( $r^2$ ): 0.996320 y = +2.3992e+002x Carbon Dioxide External Standard Analysis - Locked Resp. Fact. RSD: 3.399%Curve Type: Linear Origin: Force Coeff. Det.( $r^2$ ): 0.999813y = +1.8617e+004x



Print Date: 05 Jul 2018 08:53:10 Calibration Curves Report - Page 2 File: \\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth Detector: 3800 GC, Address: 44, Channel ID: Front

Methane External Standard Analysis - Locked Resp. Fact. RSD: 2.632% Curve Type: Linear Origin: Force Coeff. Det.( $r^2$ ): 0.999958 y = +1.2922e+004x



				Edit Codes	1				
18:53:10				Cal. No. of Range Points	 Locked Locked Locked				
Page 1 05 Jul 2018 08:53:10	3800 GC 44 Middle	6/28/2018 09:16		ષ્ટ	+9.9984e-001 +9.9982e-001 +9.9980e-001 +9.9947e-001				
	۰۰ ۳۰۰۰			O	+0.00000000000000000000000000000000000				
th	Method Detector Type Method Bus Address Method Channel	Last Recalculation Date		×	+1.0233e+007 +1.0353e+007 +1.0293e+007 +1.1439e+003		Peak Measurement: Area Curve\Origin: 1 F Std. Dev. 3 # # 3 # # 7 # # 0 #	Peak Measurement: Area Curve\Drigin: 1 F Std: Dev. 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Peak Measurement: Area Curve\Origin: 1 F 4 # * * * * * * * * * * * * * * * * * *
Calibration Block Report \\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth 7/5/2018 08:22			.30****************	Xz		Edit Codes 	Para Para Para Para Para Para Para Para	Avg. Response 246. 8 9268. 2 96590. 7 996839. 0 5060043. 0	Avg. Response 4550. 4 12437. 1 96521. 4 991482. 9 5025025. 0 10358155. 0
Calibration Block Report \\airtech-server\insdata\gc8a\me 7/5/2018 08:22	linear force External Standard Analysis	6/27/2018 17:19	**GC Workstation Multi Instrument*************Version 6.30***********************	e\ X³ in		Origin Codes	Locked - Response 1449 9544 985214 5006934 10291208	Locked Response 247 9268 96591 996839 5060043 10414535	Locked Response 4550 12437 96521 991483 5025025 10358155
: Calit : Nairt : 7/5/2	: linear : force : Exterr	: 6/27	n Multi Instrumen	j. i	<u>т</u> ттт т	О ^{гіді} 2 п	Replicate No.	Replicate No.	Replicate No.
ad File Method Time	Gested Curve Type uested Origin bration Type	bration Dates t Injection Date	**********************GC Workstation		<ol> <li>768 Carbon Monoxide</li> <li>369 Methane</li> <li>558 Carbon Dioxide</li> <li>723 NMOC_(ppmv)</li> </ol>	Curve Codes  1 linear 2 quadratic 3 cubic	. Time: 1.768 min. k Name: Carbon Monoxide el Amount 0. 0001000 2 0. 010000 3 0. 100000 4 0. 100000 5 0. 500000 6 1. 000000	. Time: 2.369 min. k Name: Methane el Amount 0. 0001000 2 0. 010000 3 0. 100000 4 0. 100000 5 0. 500000 6 1. 000000	. Time: 4.558 min. ik Name: Carbon Dioxide el Amount 1 0.0001000 2 0.010000 3 0.010000 5 0.100000 5 0.100000 5 11.000000 5 0.500000 5 11.000000 5 11.000000 5 0.500000 5 0.500000 5 0.500000 5 0.5000000 5 0.5000000 5 0.5000000 5 0.50000000000000000000000000000000000

Page 1 05 Jul 2018 08:53:10

Date: 05 Jul 2018 08:53:10

Page 2 05 Jul 2018 08:33:																																									
Peak Measurement: Area	curve/Origin: I F Std. Dev.	4 E 0 7 0			1043.51		36222.67		1	25867.82			c-temp ochoc8a/20146/irif\08irif031 run	c. termo octocea 2016/jul/08/jul/08/julo	c:\temp gc\gc8a\2016\jul\08jul033.run	c:\temp gc\gc8a\2016\jul\08jul034.run	c:\temp gc\gc8a\2016\jul\08jul035.run	c:\temp gc\gc8a\2016\jul\08jul036.run	c:\temp gc\gc8a\2016\jul\08jul031.run	c:\temp gc\gc8a\2016\jul\08jul032.run	c:\temp gc\gc8a\2016\ull\08jul033.run	c:\temp gc\gc8a\2016\ull\08jul\034.run	ctiventip gorgcoated toyutwojutucostan	community generation of a second state of the second second second second second second second second second se	c:\temp gc\gcc8a\2016\iul\08iul032.run	c:\temp gc\gc8a\2016\jul\08jul033.nn	c:\temp gc\gc8a\2016\jul\08jul034.run	c:\temp gc\gc8a\2016\jul\08jul035.nn	c:\temp gc\gc8a\2016\jul\08jul036.nm	:\gc8a\2018\jun\27jun025.run	:\gc8a\2018\jun\27jun026.run	:\gc8a\2018\jun\27jun027.run	:\gc8a\2018\jun\27jun014.run	:\gc8a\2018\un\27jun015.run	:\gc8a\z018yun\z/jun016.run	:)gc8a\z018\un\z/junu19.run \rcsa\2018\iiiv\27iiin020 rija	Noc8a/2018/iun/27iun021.nu	:\dc8a\2018\jun\27jun028.run	:\gc8a\2018\jun\27jun029.run	:\gc8a\2018\jun\27jun030.run	
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Locked	Response 38062	38743	390338	388535	388525	3642229	3640684	11394963	11345066	11358176		Ē	7/11/2016 10:20	7/11/2016 10:25	7/11/2016 10:49	7/11/2016 11:04	7/11/2016 11:19	7/11/2016 11:33	7/11/2016 10:20	7/11/2016 10:35	7/11/2016 10:49	401102/11//	20-11 010711//	2/11/2/14/14/2/	7/11/2016 10:35	7/11/2016 10:49	7/11/2016 11:04	7/11/2016 11:19	7/11/2016 11:33	6/27/2018 16:05	6/27/2018 16:21	6/27/2018 16:35	6/27/2018 12:22	6/27/2018 12:36	LC:21 8102//2/9	6/2//2018 13:46 6/97/9018 14-00	6/27/2018 14-15	6/27/2018 16:50	6/27/2018 17:04	6/27/2018 17:19	
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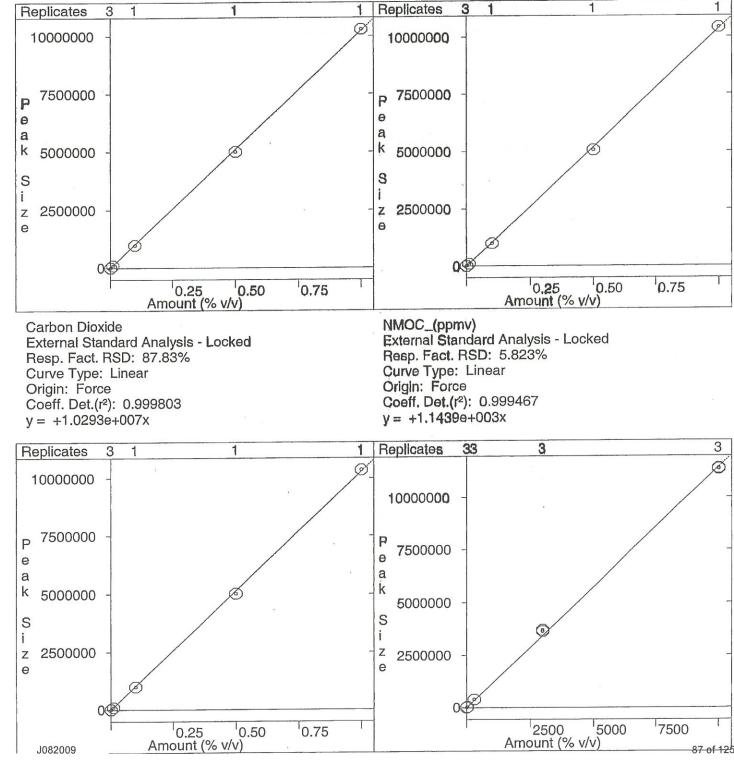
99 1521 Jo 3018 08:53:10 1521 Date: 05 Jul 2018 08:53:10

7

Locked Coefficients

Print Date: 05 Jul 2018 08:53:10 Calibration Curves Report File: \\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth Detector: 3800 GC, Address: 44, Channel ID: Middle

Methane **Carbon Monoxide** External Standard Analysis - Locked External Standard Analysis - Locked Resp. Fact. RSD: 35.30% Resp. Fact. RSD: 17.98% Curve Type: Linear Curve Type: Linear Origin: Force Origin: Force Coeff. Det.(r2): 0.999825 Coeff. Det.(r2): 0.999839 v = +1.0353e + 007xy = +1.0233e+007x1 Replicates 3 1 1



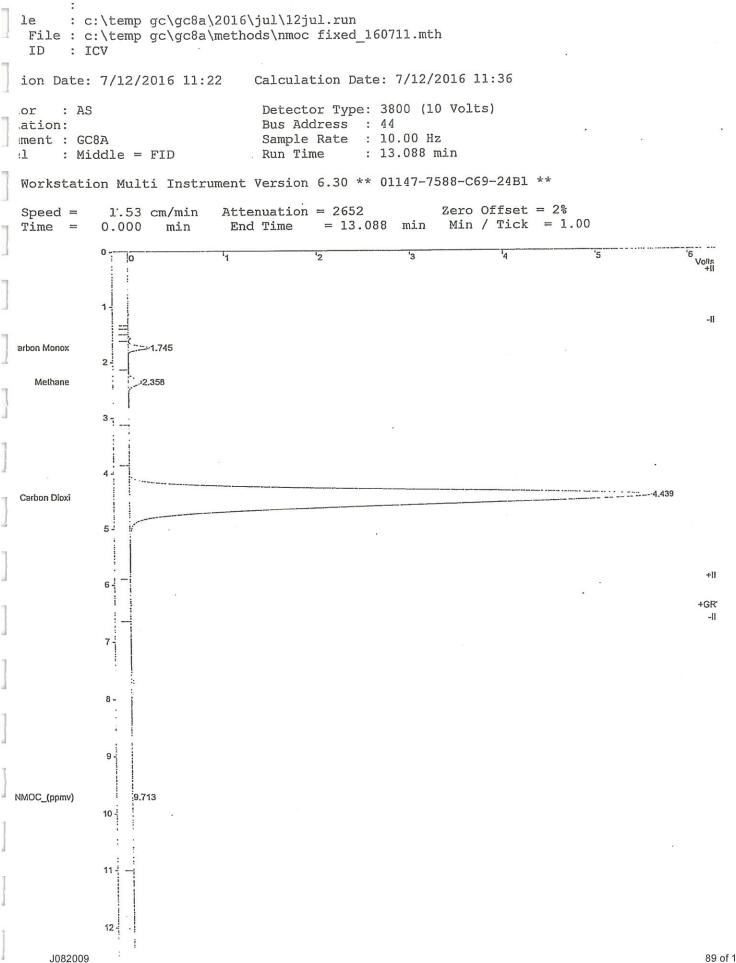
## 4. Initial Calibration Verification

a. ICV Summary

b. Chromatograms/Results

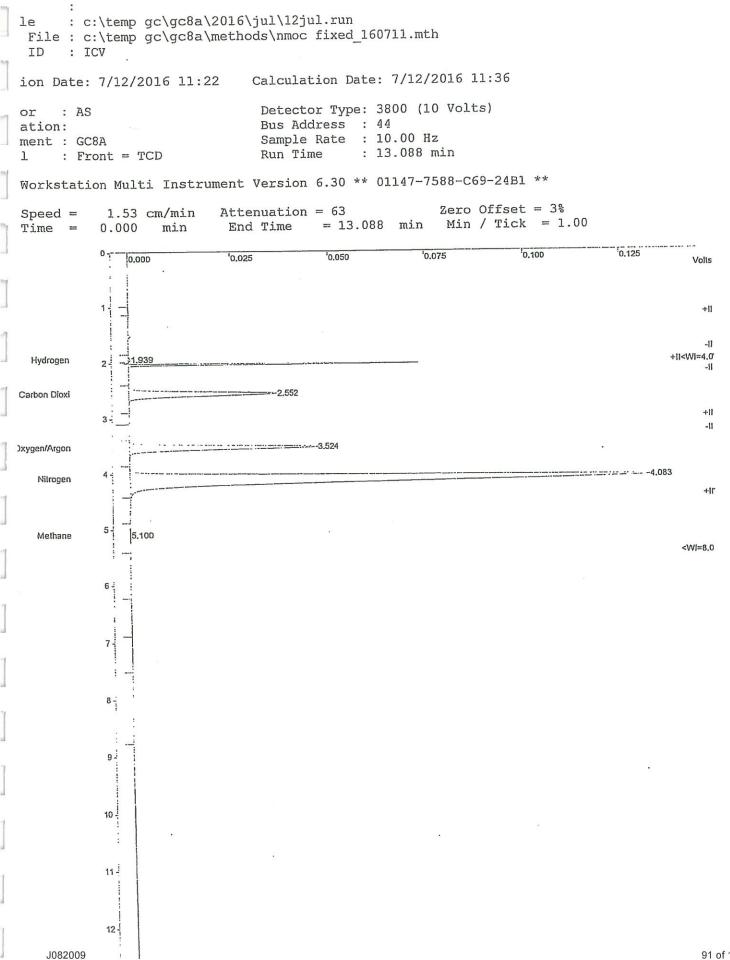
**Continuing Calibration Criteria:** 

Form-15 Rev. 2 \\AIRTECH-SERVER\Shared Folders\Company\QA\Forms\GC Raw Data Pkg Dividers Rev2.doc QA Manager 10/2016



'eam: 3, Advance Time: 17:13:44 7/12/2016 11:36: Calculated results from channel Middle using method: 'c:\temp gc\gcBa\methods\nmoc fixed_160711.mth' Status Codes ** υ 4 0 ** 01147-7588-C69-24B1 Width 1/2 (sec) 4.5 7.5 17.8 0.0 Unidentified Peak Factor: Identified Peaks: Calculation Date: 7/12/2016 11:36 3800 (10 Volts) Sep. Code UB GR GR 22 1 44 10.00 Hz 13.088 min microVolts c:\temp gc\gc8a\2016\jul\12jul.run c:\temp gc\gc8a\methods\nmoc fixed_160711.mth ICV 1080566 1075471 106895968 694536 109746541 (counts) nur Area Analysis - Subtract Blank Baseline Peak Area External Standard this Detector Type: : Bus Address : { Sample Rate : : Run Time : : Ч range; No Recovery Action Specified 3C Workstation Multi Instrument Version 6.30 0.003 before -0.060 Offset (min) Rejected Peaks: 0 62269 counts LSB: Time monitored 1.745 2.358 4.439 9.713 (uin) Ret. Time Ч Divisor: ale ID : ICV 88 82tion Date: 7/12/2016 11:22 6 microVolts 1 0.105600 0.103885 10.384848 1239.40222 1249.99655 Out of calibration range se (used): 10 microVolts Result (% v/v) .. Counts : GC8A : Middle = FID 56 al Unidentified 111 Carbon Monox Carbon Dioxi v sulation Type: •• c Measurement: NMOC (ppmv) eline Offset: ual injection ected Peaks: AS Peak ib. out of Name :ision Log: Methane ... •• Totals: ч tus Codes: ••• •• e File 10d File :ator :
cstation: tiplier: rument 1111 e ID Mode HNMA ak o. 1 1

90 of 125



Status Codes ** C Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ហ 2.5 4.8 4.4 7.7 1/2 (sec) Width 1111 Calculation Date: 7/12/2016 11:36 Identified Peaks: 3800 (10 Volts) sep. Code д д д д д д д д д д д 44 10.00 Hz 13.088 min c:\temp gc\gc8a\2016\jul\12jul.run c:\temp gc\gc8a\methods\nmoc fixed_160711.mth ICV 1346 188407 225156 1094118 1196 . Area (counts) 1510223 Detector Type: 5 Bus Address : 4 Sample Rate : 1 Run Time : 1 100.000 100.0046 100.0046 10000 10000 10000 10000 0.101 Rejected Feaks: 0 Offset counts (nim) Time 111 1.833 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 10647 1111 (uiu) Ret. Time External Standard He ID : ICV Stion Date: 7/12/2016 11:22 ator : AS 5.608941 10.120130 15.463351 70.980759 0.092556 102.265737 Result (% v/v) •• Analysis Peak Area Counts HCD HCD 1 11 Oxygen/Argon Nitrogen Methane Front Unidentified Carbon Dioxi ••• Measurement: ulation Type: σ GC8A cted Peaks: Name Peak Hydrogen .. Totals: File od File Le ID station: rument Mode nel Ч 1400401 х .

al injection

- monitored before this run

0

Unidentified Peak Factor:

Ч

Divisor:

-33 microVolts

iline Offset:

iiplier: 1

ie (used): 4 microVolts

1 microVolts

LSB:

sion Log:

iam: 3, Advance Time: 17:13:44 7/12/2016 11:36: Calculated results from channel Front using method: 'c:\temp gc\gc8a\methods\nmoc fixed_160711.mth'

: Fixed Gas from FID/NMOC itle in File : i:\gc8a\2018\jun\27jun031.run sthod File : \\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth imple ID : 300 PPMV NMOC ICV Calculation Date: 6/28/2018 09:17 ijection Date: 6/27/2018 17:34 Detector Type: 3800 (10 Volts) perator : AS Bus Address : 44 orkstation: Sample Rate : 10.00 Hz nstrument : GC8A : 13.088 min Run Time : Middle = FID hannel * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Zero Offset = 5% Attenuation = 401.53 cm/min hart Speed = Min / Tick = 1.00= 13.088 min End Time min 0.000 | tart Time = 80 90 70 50 0 30 40 60 20 0 10 mVolts 1. -11 1.586 Carbon Monox 2 2.373 Methane 3. 4 4.565 Carbon Dioxi 5 +11 6 +GR* 7 8 9. 9.724 NMOC_(ppmv) 10. 11 12 J082009 93 of 125

Status Codes 1 1 1 Þ Þ 1179 1120 352944 12003 338642 (counts) * * i:\gc8a\2018\jun\27jun031.run
\\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth Area 0 4 C Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 Unidentified Peak Factor: Identified Peaks: Calculation Date: 6/28/2018 09:17 3800 (10 Volts) 0.007 0.001 -0.170 -0.182 0.004 microVolts Offset (mim) Time 111 10.00 Hz 13.088 min N ч О 1.586 2.373 4.565 9.724 run 111 (nim) Ч 44 Time Ret. Ч this Page ification Failure; No Recovery Action Specified Verification Report .. Type: monitored before Sample Rate 88.5 89.5 16.6 1.2 Bus Address Rejected Peaks: 0 LSB: 0 counts Dev. Detector d₀ Run Time 0.000115 0.000108 0.001166 296.048020 Calculated 296.046631 Result (% v/v) from FID/NMOC Thu Jun 28 09:17:16 2018 External Standard Ч Out of verification tolerance Divisor: microVolts ction Date: 6/27/2018 17:34 300 PPMV NMOC ICV 0.001000 0.001000 0.001000 299.700012 1 Verification Expected se (used): 10 microVolts Result (% v/v) .. Peak Area Counts Middle = FID 25.0% Fixed Gas -19 al Unidentified Carbon Monox Carbon Dioxi S •• NMOC_ (ppmv) Measurement: ulation Type: eline Offset: GC8A ual injection scted Peaks: AS Peak Name ision Log: Methane Totals: :us Codes: Ч 1 1 1 .. •• •• •• •• station: tiplier: Date: rument rance Mode ator nel H 12 M 4 ١ ł × 2 . .

'\\airtech-server\insdata\gc8a\methods\nmoc fixed_161212bu_c.mth' eam: 5, Advance Time: 17:32:23 6/28/2018 09:17: Calculated results from channel Middle using method: 7/2018 17:47: Calculated results from channel Middle using method: '\\airtech-server\insdata\gc8a\methods\nmoc fixed_180627.mth'

ginal Notes 6

o Brended Notes: 22

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]								
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]		*****						
]	of 2	* * * * *						
]	Page 2							
		***						
]	8	* *						
	:16 2018	* * * * *						
	8 09:17:16	* * * * * *						
]	t Date: Thu Jun 28	****						
	te: Thu	* * * * * *						
	t Dat	* * #082009						

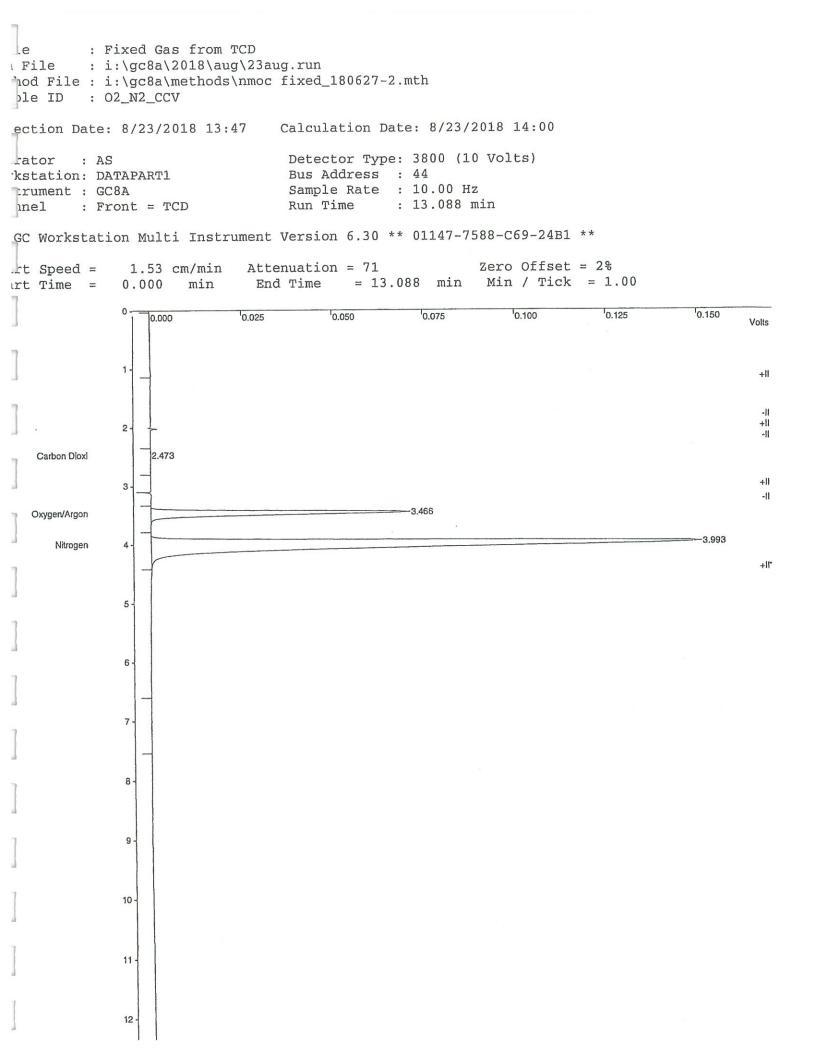
## 5. Continuing Calibration Verification

a. CCV Summary

b. Chromatograms/Results

**Continuing Calibration Criteria:** 

Form-15 Rev. 2 \VAIRTECH-SERVER\Shared Folders\Company\QA\Forms\GC Raw Data Pkg Dividers Rev2.doc QA Manager 10/2016



int Date: Thu Aug 23 14:01:00 2018 Page 1 of 1 Verification Report tle : Fixed Gas from TCD n File : i:\gc8a\2018\aug\23aug.run thod File : i:\gc8a\methods\nmoc fixed_180627-2.mth mple ID : 02_N2_CCV Calculation Date: 8/23/2018 14:00 jection Date: 8/23/2018 13:47 Detector Type: 3800 (10 Volts) erator : AS Bus Address : 44 Sample Rate : 10.00 Hz rkstation: DATAPART1 strument : GC8A : 13.088 min Run Time : Front = TCDannel GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification n Mode ak Measurement: Peak Area lculation Type: External Standard vel : 4 lerance : 25.0% ExpectedCalculatedRet.TimeResultResultDev.TimeOffset(% v/v)(% v/v)%(min)(min) Time Expected Calculated Status Area eak Peak No. Name (counts) Codes No. ------_____ ___ ____ _____ 911 
 1 Hydrogen
 10.000000
 1.930

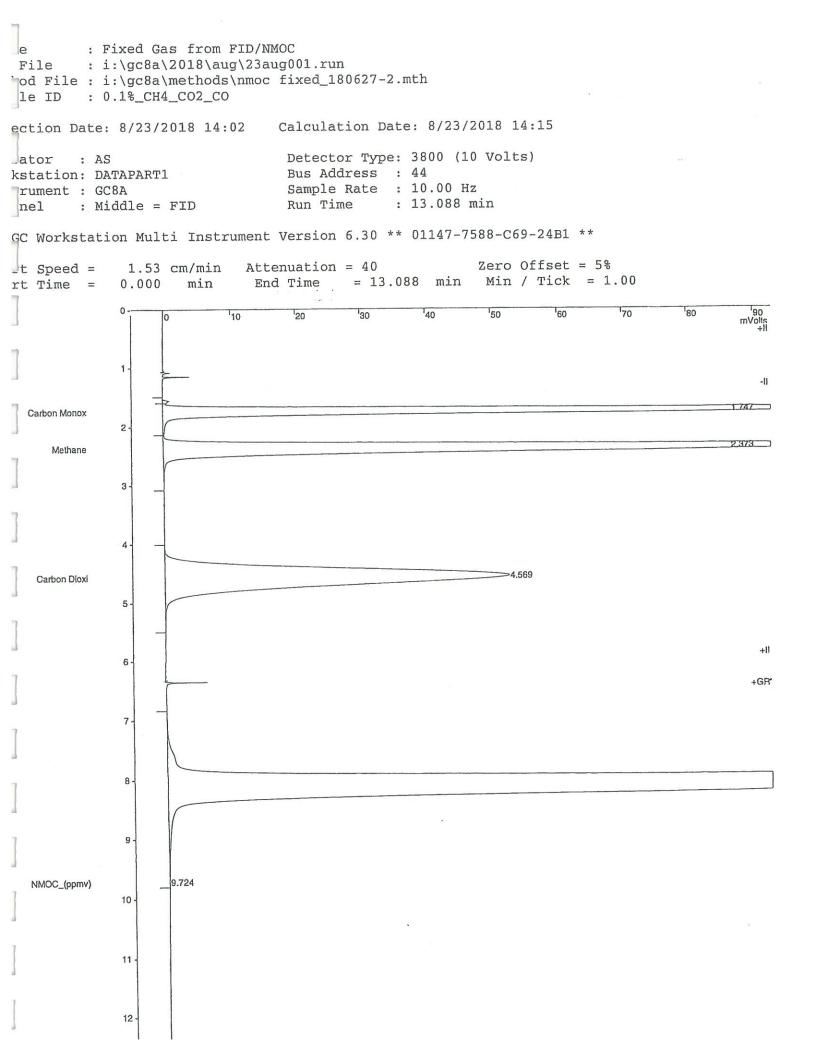
 2 Carbon Dioxi
 50.000000
 0.048908
 99.9
 2.473
 0.028
 911

 3 Oxygen/Argon
 21.900000
 23.180603
 5.8
 3.466
 0.010
 337524

 4 Nitrogen
 78.099998
 81.224274
 4.0
 3.993
 0.059
 1252035
 VM v C 78.099998 81.224274 4 Nitrogen 4.997 VM 50.000000 _____ preser serences ----1 104.453785 0.097 1590470 Totals: atus Codes: - Out of verification tolerance - Missing peak - Out of calibration range tal Unidentified Counts : 904 counts Rejected Peaks: 1 Identified Peaks: 5 tected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 ltiplier: 1 1 microVolts seline Offset: -8 microVolts LSB: ise (used): 5 microVolts - monitored before this run nual injection lib. out of range; No Recovery Action Specified rification Failure; No Recovery Action Specified vision Log: 23/2018 14:00: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' ream: 1, Advance Time: 13:47:23 iginal Notes: ***********

1000000

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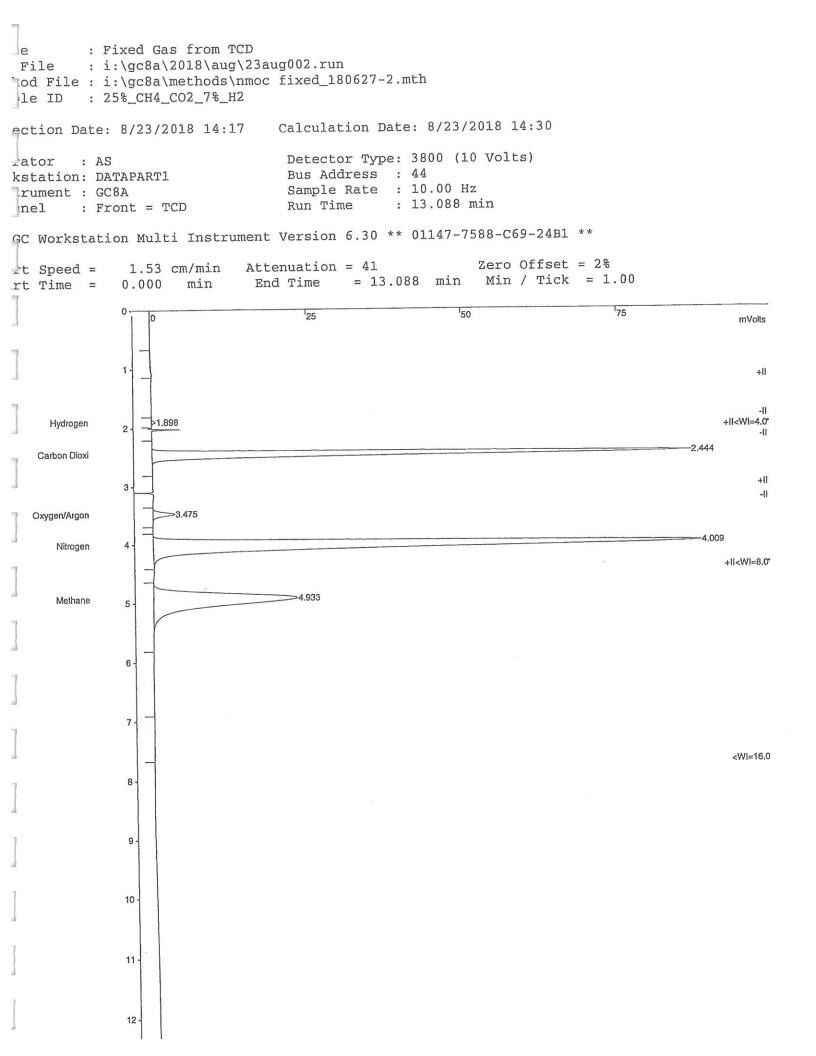


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iginal Notes: 'i:/9c8a/methods/somr/sbodrae/meth' ream: 2, Advarce Time: 14:00:44 23/2018 14:15: Calculated results from channel Middle using method: : BOT UOISIA rification Failure; No Recovery Action Specified nual injection nur zird stoled berolinom - zjlovorcim SI :(bezu) ezi seline Offset: -21 microVolts : SSI l microvolts Divisor: 1 1 : ISIIIEI I Unidentified Peak Factor: 0 Lected Peaks: 5 Rejected Peaks: 0 Ідептітіед Реакз: 4 : sanuob bailidabinu Lad Saunos #TSZ - Out of verification tolerance : Sabod Suff 714858.7202 :slsjoT 900.0-0562588 _____ ______ _____ _____ 7.64 80852.7202 00000.9999 (Vmgg)_DOMN 4 P27.2 τοο.ο A 6680972 4.569 2.373 251660°0 010.0 8.0 3 Carbon Dioxi 0.100000 1020617 0.100000 8.3 EEE801.0 2 месряле ₽00.0 TISIZST 706560.0 J Carbon Monox LTLT τ.9 0.100000 -0°057 ET6096 -----_____ _____ ----_____ .01 (시/지 문) ameN (uțu) (八/八 号) (sgunos) (utu) z Sabou Jusay 2 Tusea Feak Sak SMIT .V9d Jazilo Area snapas Expected Calculated .J9A Surr rerance \$0.25 : TƏA ₽: leulation Type: External Standard ik Measurement: Peak Area : Verification abom r ** IEA-2690-8827-7114 ** 05.3 noisiev Jammurisal iilum noitsistev GC Tanne : WIGGIG = FID uim 880.EI : Smit nuA vernment : GC8A ZH 00.01 : Sample Rate rkstation: DATAPAT1 : Bus Address 55 srator SY : Detector Type: 3800 (10 Volts) Calculation Date: 8/23/2018 14:15 jection Date: 8/23/2018 14:02 : 0.1%_CH4_CO2_CO ai sign 1 File : i:/gc8a/2018/aug/23aug001.run hdm.2-720081_bamoc fixed_180627-2.mth : Fixed Gas from FID/NMOC at: Verification Report

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......



```
Verification Report
tle : Fixed Gas from TCD
a File : i:\gc8a\2018\aug\23aug002.run
thod File : i:\gc8a\methods\nmoc fixed_180627-2.mth
mple ID : 25%_CH4_CO2_7%_H2
                                        Calculation Date: 8/23/2018 14:30
jection Date: 8/23/2018 14:17
                                          Detector Type: 3800 (10 Volts)
erator
         : AS
                                          Bus Address : 44
rkstation: DATAPART1
                                          Sample Rate : 10.00 Hz
strument : GC8A
                                                          : 13.088 min
annel : Front = TCD
                                          Run Time
 GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 **
n Mode
                : Verification
ak Measurement: Peak Area
lculation Type: External Standard
          : 3
: 25.0%
vel
lerance
                      Expected Calculated Ret. Time
Result Result Dev. Time Offset
(% v/v) (% v/v) % (min) (min)
                                                                                  Area
                                                                                            Status
eak Peak
No. Name
                                                                               (counts) Codes
No.
                                                         _____ ____
                                                                                -----
                                                                                             _____

      1 Hydrogen
      7.000000
      6.573445
      6.1
      1.898
      -0.032
      1577

      2 Carbon Dioxi
      25.000000
      22.225119
      11.1
      2.444
      -0.001
      413767

      3 Oxygen/Argon
      10.900000
      1.116918
      89.8
      3.475
      0.019
      16263

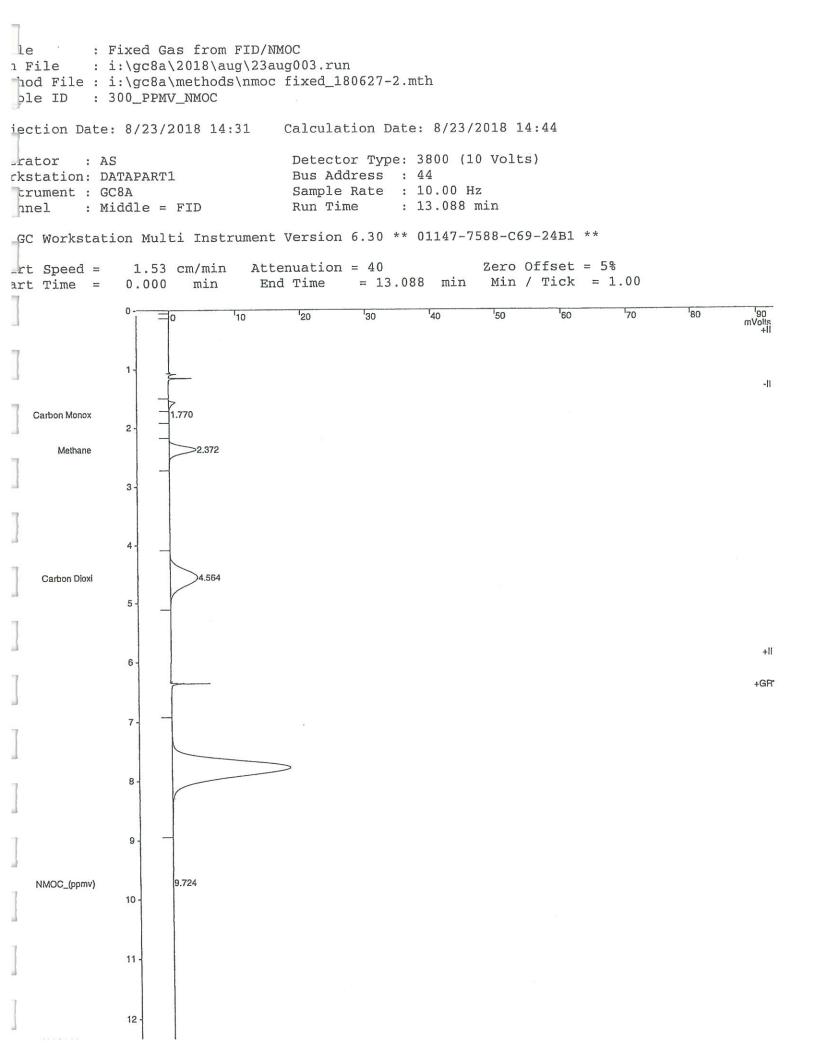
      4 Nitrogen
      39.099998
      46.031353
      17.7
      4.009
      0.076
      709552

      5 Methane
      25.000000
      24.533443
      1.9
      4.933
      -0.064
      317018

                                                                                             v
                                                                                            ------
                                                                     -0.002 1458177
                                   100.480278
     Totals:
atus Codes:
- Out of verification tolerance
                                        548 counts
tal Unidentified Counts :
                                                            Identified Peaks: 5
                               Rejected Peaks: 1
:tected Peaks: 7
                                                  Unidentified Peak Factor: 0
                         Divisor: 1
ltiplier: 1
                                                        1 microVolts
                                             LSB:
seline Offset: 1 microVolts
ise (used): 4 microVolts - monitored before this run
unual injection
rification Failure; No Recovery Action Specified
vision Log:
'23/2018 14:30: Calculated results from channel Front using method:
   'i:\gc8a\methods\nmoc fixed_180627-2.mth'
ream: 3, Advance Time: 14:15:18
iginal Notes:
```

int Date: Thu Aug 23 14:30:06 2018

Page 1 of 1



```
int Date: Thu Aug 23 14:44:41 2018
                                                    Page 1 of 1
                                  Verification Report
:le : Fixed Gas from FID/NMOC
1 File : i:\gc8a\2018\aug\23aug003.run
thod File : i:\gc8a\methods\nmoc fixed_180627-2.mth
nple ID : 300_PPMV_NMOC
                                    Calculation Date: 8/23/2018 14:44
jection Date: 8/23/2018 14:31
                                       Detector Type: 3800 (10 Volts)
erator
         : AS
rkstation: DATAPART1
                                      Bus Address : 44
                                       Sample Rate : 10.00 Hz
Run Time : 13.088 min
strument : GC8A
       : Middle = FID
                                       Run Time
annel
GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 **
               : Verification
n Mode
ak Measurement: Peak Area
lculation Type: External Standard
            : 2
vel
               : 25.0%
lerance
                    ExpectedCalculatedRet.TimeResultResultDev.TimeOffset(% v/v)(% v/v)%(min)(min)
                    Expected Calculated
                                                                                    Status
                                                                           Area
       Peak
Name
eak
                                                                         (counts) Codes
                    (% v/v)
No.
     _____
                                                                                     ____

        1 Carbon Monox
        0.001000
        0.000041
        95.9
        1.770
        0.002
        416

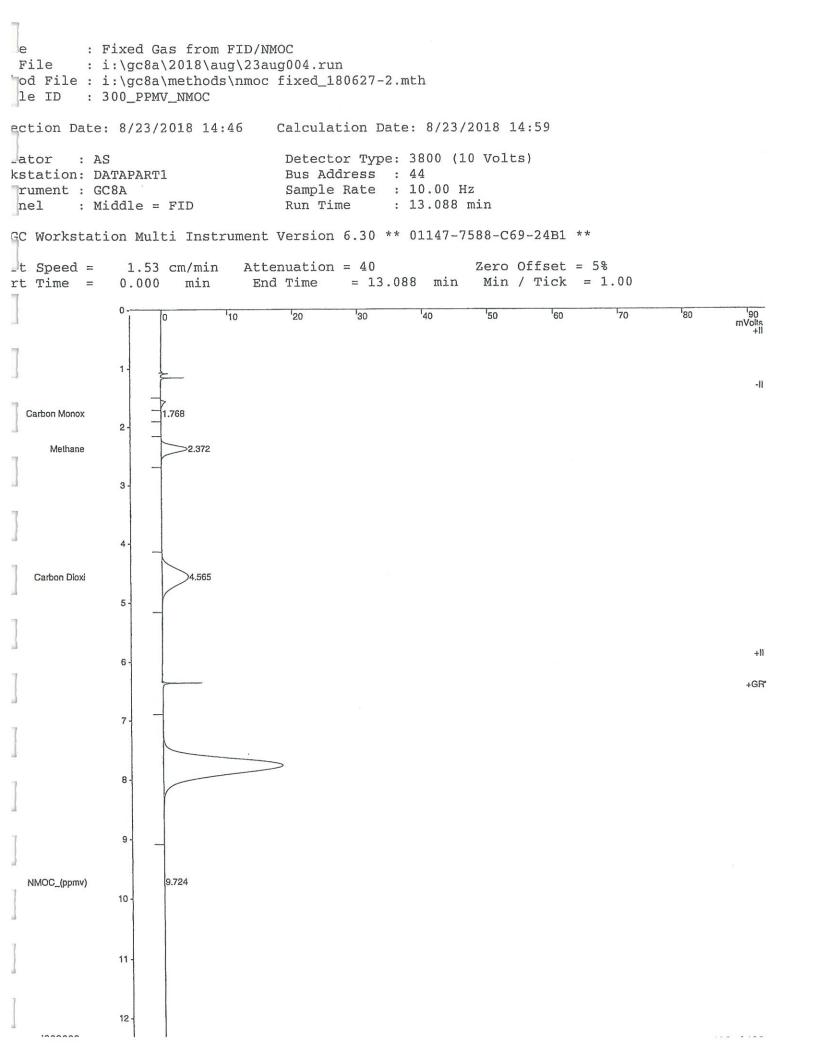
        2 Methane
        0.001000
        0.003182
        218.2
        2.372
        0.003
        32937

        3 Carbon Dioxi
        0.001000
        0.007749
        >500
        4.564
        0.006
        79760

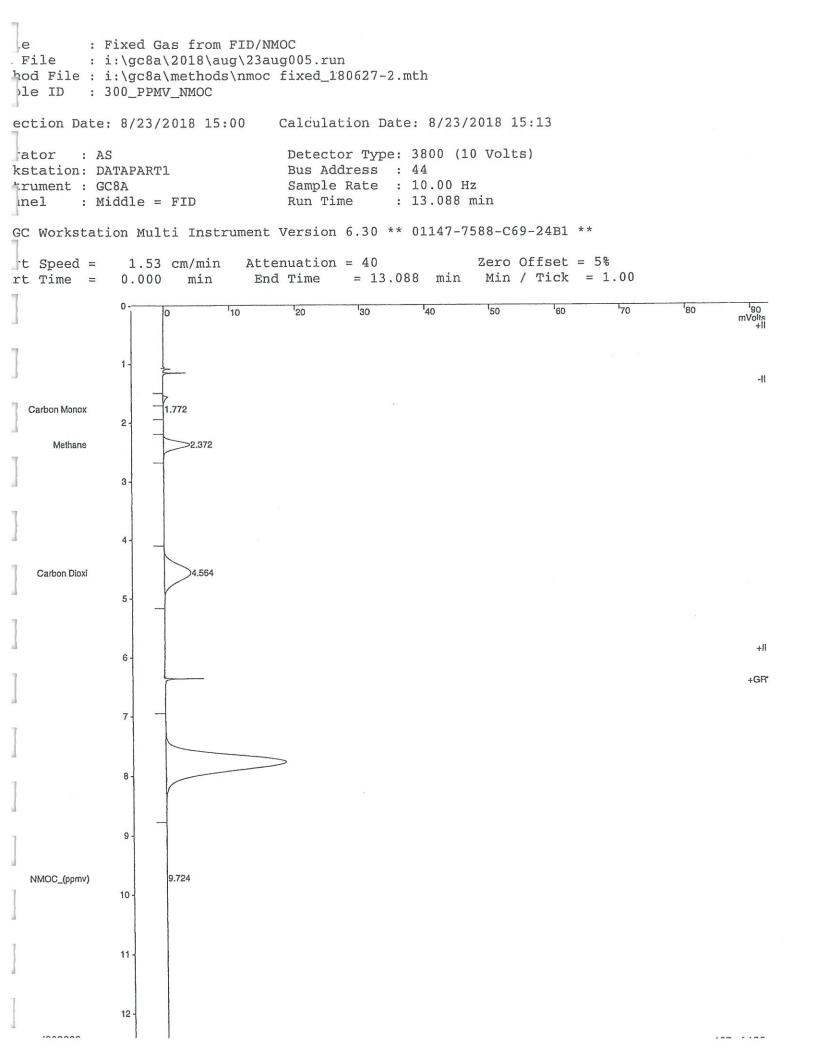
        4 NMOC_(ppmv)
        299.700012
        312.551270
        4.3
        9.724
        0.001
        357521

                                                                                    37
                                                                                    v
                                                                                    v
 4 NMOC_(ppmv) 299.700012 312.551270 4.3
          ------
___ ___
                                                               0.012
                                                                          470634
                               312.562242
    Totals:
atus Codes:
- Out of verification tolerance
                                   3894 counts
tal Unidentified Counts :
                            Rejected Peaks: 0 Identified Peaks: 4
tected Peaks: 6
                       Divisor: 1
                                              Unidentified Peak Factor: 0
ltiplier: 1
                                                      1 microVolts
                                            LSB:
seline Offset: -11 microVolts
vise (used): 8 microVolts - monitored before this run
unual injection
rification Failure; No Recovery Action Specified
vision Log:
'23/2018 14:44: Calculated results from channel Middle using method:
  'i:\gc8a\methods\nmoc fixed_180627-2.mth'
:ream: 4, Advance Time: 14:29:51
iginal Notes:
```

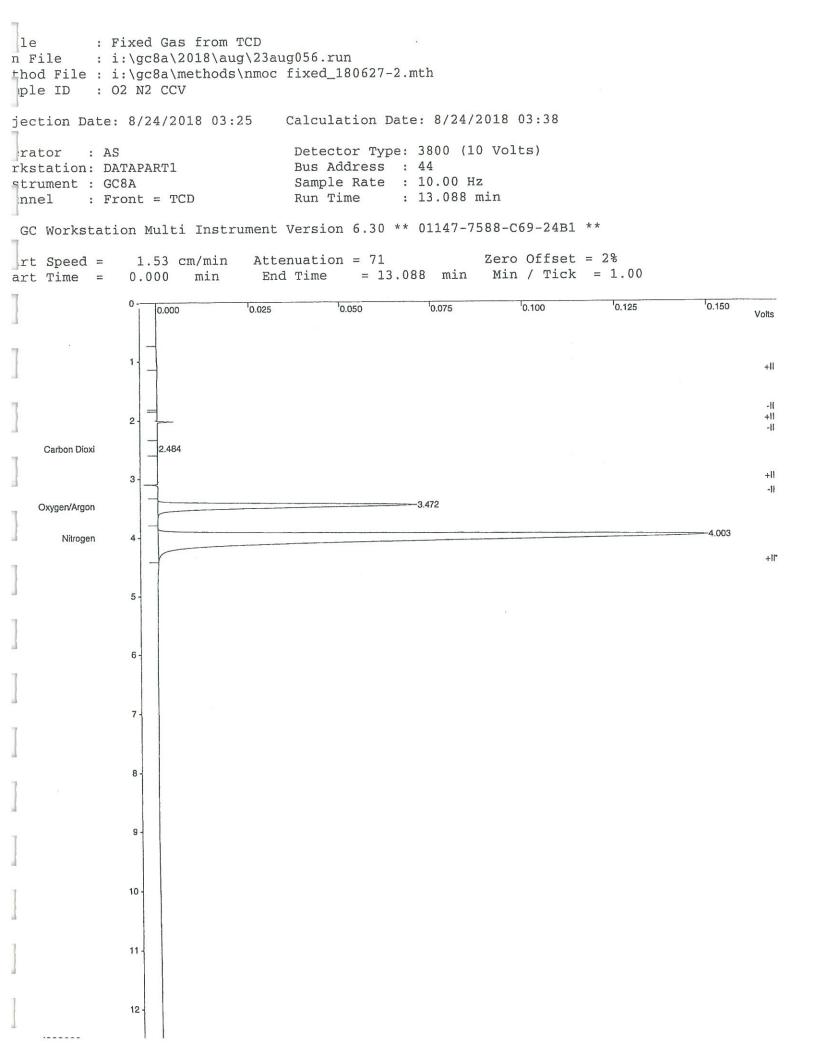
1000000



int Date: Thu Aug 23 14:59:14 2018 Page 1 of 1 Verification Report : Fixed Gas from FID/NMOC :le : i:\gc8a\2018\aug\23aug004.run ı File chod File : i:\gc8a\methods\nmoc fixed_180627-2.mth nple ID : 300_PPMV_NMOC Calculation Date: 8/23/2018 14:59 jection Date: 8/23/2018 14:46 Detector Type: 3800 (10 Volts) erator : AS Bus Address : 44 Sample Rate : 10.00 Hz rkstation: DATAPART1 strument : GC8A : 13.088 min Run Time : Middle = FID annel GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** n Mode : Verification ak Measurement: Peak Area lculation Type: External Standard : 2 vel : 25.0% lerance Ret. Time Expected Calculated Result Result Dev. (% v/v) (% v/v) % Offset Area Status Time Peak eak Name (min) (min) (counts) Codes 8 No. -----____ --- ------ ------ ------- ------_____ 1.768 0.000 2.372 0.003 4.565 0.007 419 v 1 Carbon Monox 0.001000 0.000041 95.9 0.003120 212.00.007454 > 50032299 V 0.001000 0.001000 2 Methane 76725 v 3 Carbon Dioxi 4 NMOC_(ppmv) 299.700012 311.282471 3.9 9.724 0.001 356070 _____ messes pessesses -----465513 311.293086 0.011 Totals: atus Codes: - Out of verification tolerance 3035 counts tal Unidentified Counts : Rejected Peaks: 0 Identified Peaks: 4 tected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 ltiplier: 1 LSB: 1 microVolts seline Offset: -19 microVolts ise (used): 9 microVolts - monitored before this run nual injection rification Failure; No Recovery Action Specified vision Log: 23/2018 14:59: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' ream: 4, Advance Time: 14:44:24 iginal Notes: 



int Date: Thu Aug 23 15:13:47 2018 Page 1 of 1 Verification Report tle : Fixed Gas from FID/NMOC : i:\gc8a\2018\aug\23aug005.run n File thod File : i:\gc8a\methods\nmoc fixed_180627-2.mth mple ID : 300_PPMV_NMOC jection Date: 8/23/2018 15:00 Calculation Date: 8/23/2018 15:13 Detector Type: 3800 (10 Volts) : AS erator Bus Address : 44 Sample Rate : 10.00 Hz rkstation: DATAPART1 strument : GC8A : Middle = FID Run Time : 13.088 min annel GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification n Mode ak Measurement: Peak Area lculation Type: External Standard vel : 2 lerance : 25.0% Ret. Time Expected Calculated Time Offset Result Result Dev. (% v/v) (% v/v) % Area Status Peak eak (counts) Codes B (min) (min) Name NO. _____ _____ ------------ ----- ----- ----- ---------1 Carbon Monox 0.001000 0.000048 95.2 1.772 0.004 490 V 0.001000 0.003098 209.8 2.372 0.007471 > 500 4.564 0.003 32073 V 2 Methane 0.006 76899 V 3 Carbon Dioxi 4 NMOC_(ppmv) 299.700012 309.801117 3.4 9.724 0.001 354375 354375 -----309.811734 0.014 463837 Totals: atus Codes: - Out of verification tolerance tal Unidentified Counts : 2915 counts Rejected Peaks: 0 Identified Peaks: 4 tected Peaks: 5 ltiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: 1 microVolts seline Offset: -12 microVolts ise (used): 9 microVolts - monitored before this run unual injection rification Failure; No Recovery Action Specified vision Log: '23/2018 15:13: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' :ream: 4, Advance Time: 14:58:57 iginal Notes: 



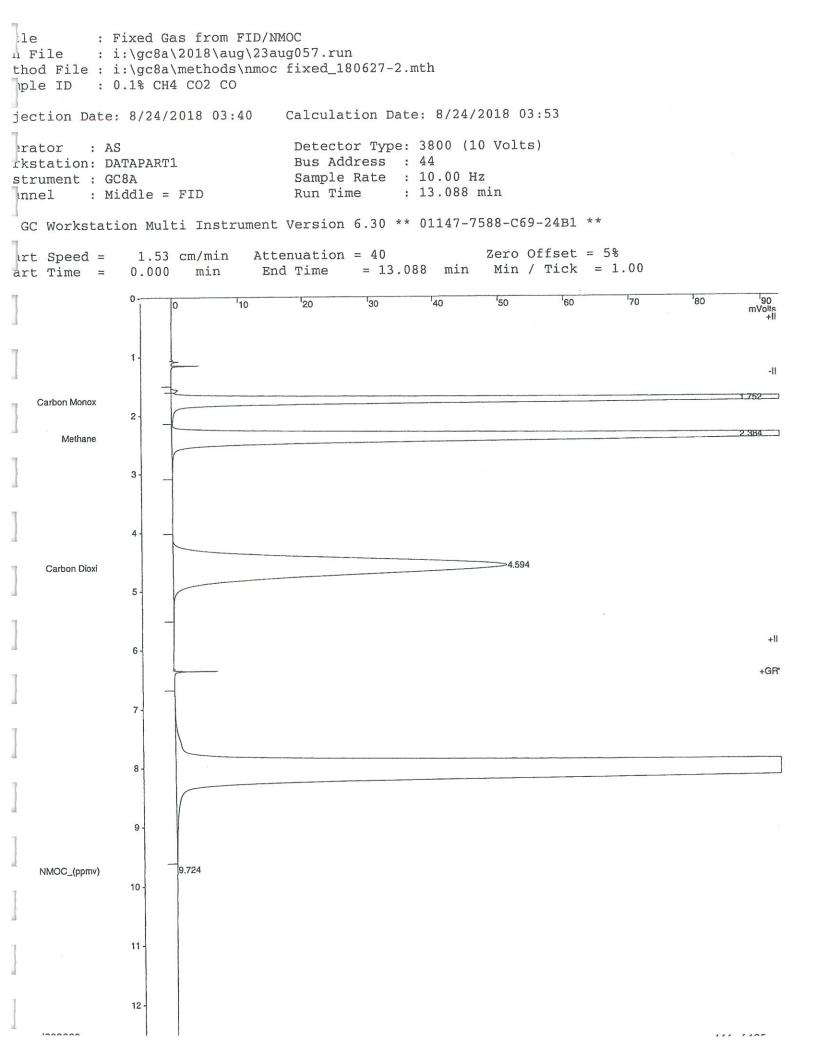
rint Date: Fri Aug 24 03:39:01 2018 Page 1 of 1 Verification Report : Fixed Gas from TCD itle un File : i:\gc8a\2018\aug\23aug056.run ethod File : i:\gc8a\methods\nmoc fixed_180627-2.mth ample ID : 02 N2 CCV njection Date: 8/24/2018 03:25 Calculation Date: 8/24/2018 03:38 Detector Type: 3800 (10 Volts) perator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min orkstation: DATAPART1 nstrument : GC8A : Front = TCD Run Time hannel * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification un Mode eak Measurement: Peak Area alculation Type: External Standard : 4 evel : 25.0% olerance Result Result Dev. Time Offset (% v/v) (% v/v) % (min) (min) Status Area Peak Peak (counts) Codes No. Name _____ ----____ ______ 1.930 VM 1 Hydrogen 10.000000 
 Inythogen
 10.000000
 0.045571
 99.9

 2 Carbon Dioxi
 50.00000
 23.171669
 5.8

 3 Oxygen/Argon
 21.900000
 23.171669
 5.8

 4 Nitrogen
 78.099998
 81.133293
 3.9

 5 Methane
 50.000000
 50.00000
 50.000000
 2.484 0.039 3.472 0.016 4.003 0.070 848 v 337394 C 1250633 4.997 VM 5 Methane _____ _____ ____ ---- ----- ------ ============ 104:350533 0.125 1588875 Totals: tatus Codes: - Out of verification tolerance - Missing peak - Out of calibration range otal Unidentified Counts : 0 counts Rejected Peaks: 2 Identified Peaks: 5 etected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 ultiplier: 1 LSB: 1 microVolts aseline Offset: -25 microVolts oise (used): 6 microVolts - monitored before this run anual injection alib. out of range; No Recovery Action Specified erification Failure; No Recovery Action Specified .evision Log: /24/2018 03:38: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' tream: 1, Advance Time: 03:23:51 riginal Notes: 



rint Date: Fri Aug 24 03:53:37 2018 Page 1 of 1 Verification Report itle : Fixed Gas from FID/NMOC
un File : i:\gc8a\2018\aug\23aug057.run ethod File : i:\gc8a\methods\nmoc fixed_180627-2.mth ample ID : 0.1% CH4 CO2 CO njection Date: 8/24/2018 03:40 Calculation Date: 8/24/2018 03:53 Detector Type: 3800 (10 Volts) perator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min orkstation: DATAPART1 nstrument : GC8A Run Time : Middle = FID hannel * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification un Mode eak Measurement: Peak Area alculation Type: External Standard evel : 4 olerance : 25.0% Ret. Time Time Offset (min) (min) Expected Calculated PeakPeakResultResultDev.No.Name(% v/v)(% v/v)% Area Status (counts) Codes 8 _____ ---- ----------- 

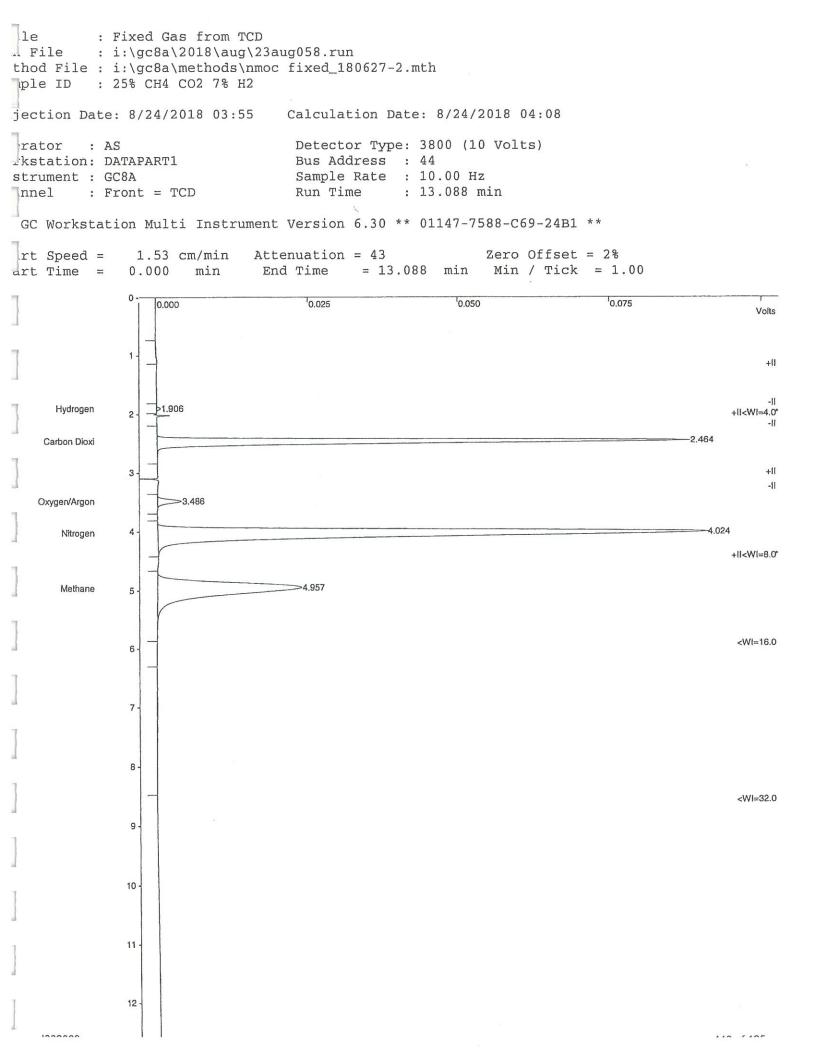
 1 Carbon Monox
 0.100000
 0.092291
 7.7
 1.752
 -0.016
 944380

 2 Methane
 0.100000
 0.106609
 6.6
 2.384
 0.015
 1103673

 3 Carbon Dioxi
 0.100000
 0.097117
 2.9
 4.594
 0.036
 999665

 4 NMOC_(ppmv)
 9999.00000
 4880.19726
 51.2
 9.724
 0.001
 5582359

 5582359 V _____ 0.036 8630077 Totals: 4880.49328 tatus Codes: - Out of verification tolerance otal Unidentified Counts : 2708 counts Rejected Peaks: 0 Identified Peaks: 4 etected Peaks: 5 Unidentified Peak Factor: 0 Divisor: 1 ultiplier: 1 aseline Offset: -18 microVolts LSB: 1 microVolts oise (used): 11 microVolts - monitored before this run anual injection erification Failure; No Recovery Action Specified evision Log: /24/2018 03:53: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' tream: 2, Advance Time: 03:38:45 riginal Notes: ****



rint Date: Fri Aug 24 04:08:11 2018 Page 1 of 1 Verification Report : Fixed Gas from TCD itle un File : i:\gc8a\2018\aug\23aug058.run :ethod File : i:\gc8a\methods\nmoc fixed_180627-2.mth ample ID : 25% CH4 CO2 7% H2 Calculation Date: 8/24/2018 04:08 njection Date: 8/24/2018 03:55 perator Detector Type: 3800 (10 Volts) : AS Bus Address : 44 Sample Rate : 10.00 Hz lorkstation: DATAPART1 nstrument : GC8A : 13.088 min : Front = TCD Run Time !hannel * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification un Mode 'eak Measurement: Peak Area alculation Type: External Standard : 3 evel : 25.0% 'olerance Expected Calculated Ret. Time Peak Result Result Dev. Time Offset Name (% v/v) (% v/v) % (min) (min) Area Status Peak (counts) Codes No. -----_____ ---------7.000000 6.690673 4.4 1.906 -0.024 25.000000 23.117918 7.5 2.464 0.019 1605 1 Hydrogen 

 1
 Hydrogen
 7.000000
 6.050001
 4.4

 2
 Carbon Dioxi
 25.000000
 23.117918
 7.5

 3
 Oxygen/Argon
 10.900000
 1.264839
 88.4

 4
 Nitrogen
 39.099998
 47.969131
 22.7

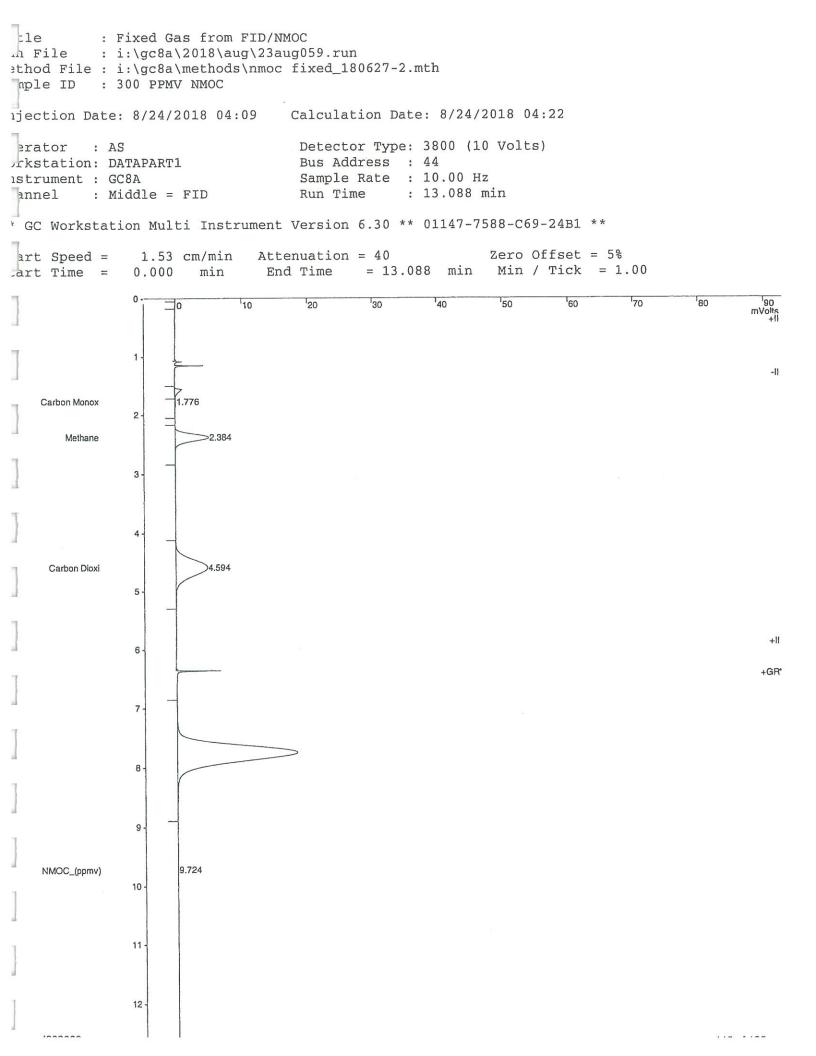
 5
 Methane
 25.000000
 25.515512
 2.1

 430389 2.464 0.019 3.486 0.030 18417 V 4.024 0.091 4.957 -0.040 739422 329708 ----104.558073 0.076 1519541 Totals: Status Codes: 7 - Out of verification tolerance 3998 counts otal Unidentified Counts : Identified Peaks: 5 Rejected Peaks: 1 )etected Peaks: 7 Unidentified Peak Factor: 0 fultiplier: 1 Divisor: 1 LSB: 1 microVolts Baseline Offset: -6 microVolts Joise (used): 4 microVolts - monitored before this run 1anual injection Verification Failure; No Recovery Action Specified levision Log: 3/24/2018 04:08: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' Stream: 3, Advance Time: 03:53:20 )riginal Notes: 

1

....

1000000



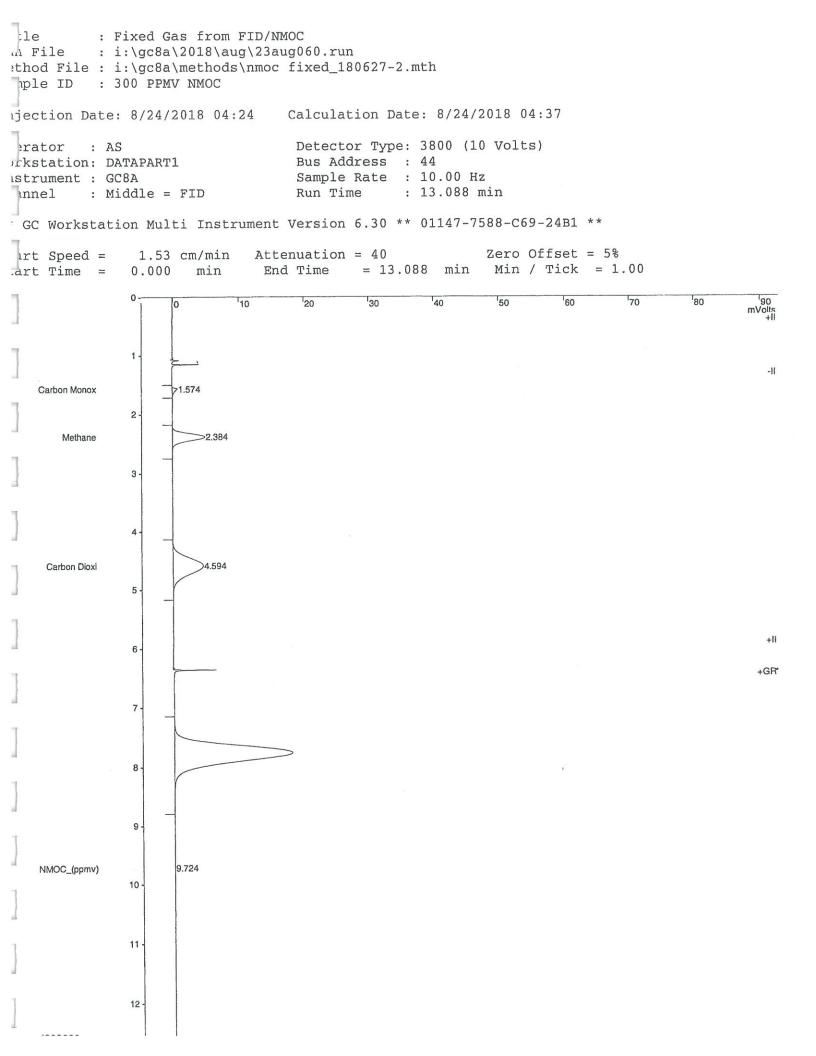
rint Date: Fri Aug 24 04:22:48 2018 Page 1 of 1 Verification Report : Fixed Gas from FID/NMOC itle : i:\gc8a\2018\aug\23aug059.run in File sthod File : i:\gc8a\methods\nmoc fixed_180627-2.mth ample ID : 300 PPMV NMOC Calculation Date: 8/24/2018 04:22 njection Date: 8/24/2018 04:09 Detector Type: 3800 (10 Volts) perator : AS Bus Address : 44 Sample Rate : 10.00 Hz Run Time : 13.088 min orkstation: DATAPART1 nstrument : GC8A : Middle = FID hannel * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification un Mode eak Measurement: Peak Area alculation Type: External Standard : 2 evel : 25.0% olerance Time Ret. Expected Calculated Time Offset Result Result Dev. (% v/v) (% v/v) % Status Area Peak Peak (counts) Codes (min) (min) No. Name ____ ____ ----------- 
 1 Carbon Monox
 0.001000
 0.000077
 92.3

 2 Methane
 0.001000
 0.004026
 302.6

 3 Carbon Dioxi
 0.001000
 0.009031
 >500
 1.776 0.008 784 V 0.015 
 2 Methane
 0.001000
 0.004026
 302.6
 2.384

 3 Carbon Dioxi
 0.001000
 0.009031 > 500
 4.594

 4 NMOC_(ppmv)
 299.700012
 301.884003
 0.7
 9.724
 41678 V 92961 v 0.036 345319 0.001 _____ - -- ------301.897137 0.060 480742 Totals: tatus Codes: - Out of verification tolerance 4561 counts otal Unidentified Counts : Identified Peaks: 4 Rejected Peaks: 0 etected Peaks: 6 Unidentified Peak Factor: 0 Divisor: 1 ultiplier: 1 1 microVolts aseline Offset: -43 microVolts LSB: 'oise (used): 7 microVolts - monitored before this run lanual injection 'erification Failure; No Recovery Action Specified evision Log: 1/24/2018 04:22: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' tream: 4, Advance Time: 04:07:56 riginal Notes: 



rint Date: Fri Aug 24 04:37:23 2018 Page 1 of 1 Verification Report itle : Fixed Gas from FID/NMOC un File : i:\gc8a\2018\aug\23aug060.run icthod File : i:\gc8a\methods\nmoc fixed_180627-2.mth
ample ID : 300 PPMV NMOC Calculation Date: 8/24/2018 04:37 njection Date: 8/24/2018 04:24 Detector Type: 3800 (10 Volts) : AS perator Bus Address : 44 orkstation: DATAPART1 Sample Rate : 10.00 Hz Run Time : 13.088 min nstrument : GC8A : Middle = FID hannel! * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Verification un Mode 'eak Measurement: Peak Area alculation Type: External Standard evel : 2 'olerance : 25.0% Expected Calculated Ret. Time Peak Peak Result Result Dev. Time Offset No. Name (% v/v) (% v/v) % (min) (min) Area Status (counts) Codes ----------- 

 1 Carbon Monox
 0.001000
 0.000305
 69.5
 1.574
 -0.194
 3118

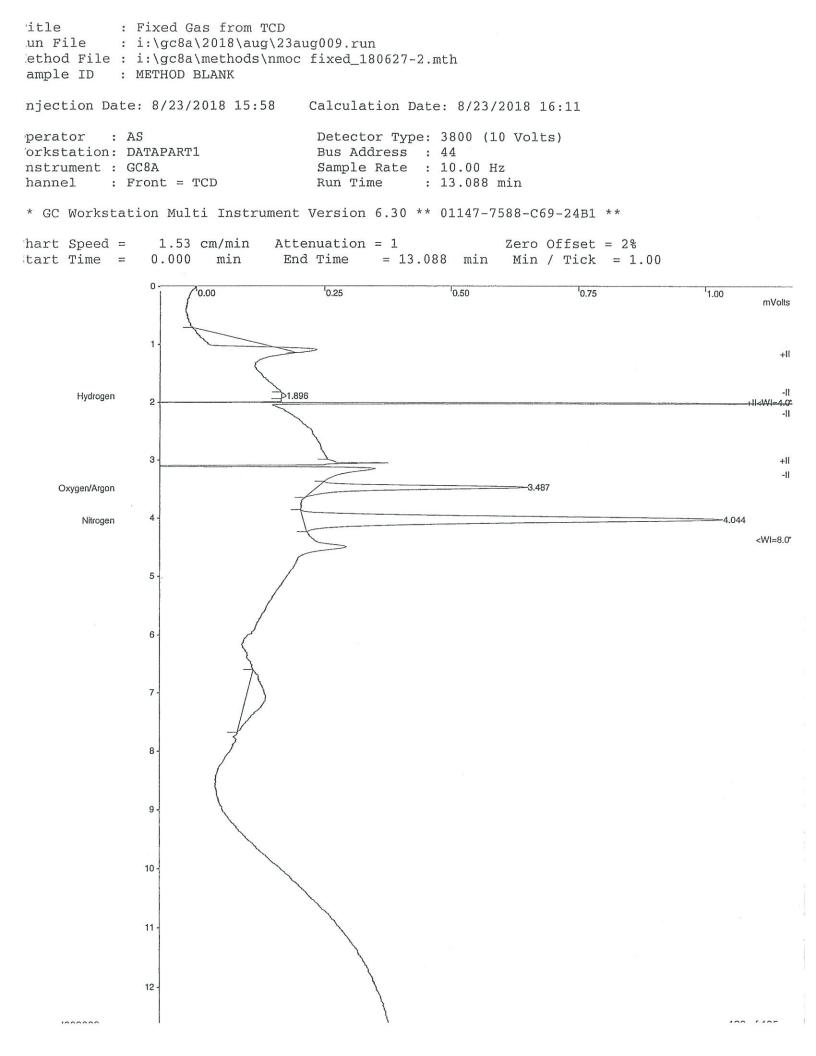
 2 Methane
 0.001000
 0.003939
 293.9
 2.384
 0.015
 40783

 3 Carbon Dioxi
 0.001000
 0.008726
 >500
 4.594
 0.036
 89817

 4 NMOC_(ppmv)
 299.700012
 299.374817
 0.1
 9.724
 0.001
 342449

 V 40783 V v _____ 299.387787 -0.142 476167 Totals: Status Codes: 7 - Out of verification tolerance 0 counts otal Unidentified Counts : Rejected Peaks: 0 Identified Peaks: 4 )etected Peaks: 4 Divisor: 1 Unidentified Peak Factor: 0 1ultiplier: 1 1 microVolts Baseline Offset: -43 microVolts LSB: Joise (used): 12 microVolts - monitored before this run fanual injection Verification Failure; No Recovery Action Specified levision Log: 3/24/2018 04:37: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' Stream: 4, Advance Time: 04:22:31 )riginal Notes: 

tle : Fixed Gas from FID/NMOC n File : i:\gc8a\2018\aug\23aug061.run ethod File : i:\gc8a\methods\nmoc fixed_180627-2.mth nmple ID : 300 PPMV NMOC njection Date: 8/24/2018 04:38 Calculation Date: 8/24/2018 04:51 Detector Type: 3800 (10 Volts) : AS erator Bus Address : 44 rkstation: DATAPART1 nstrument : GC8A Sample Rate : 10.00 Hz : 13.088 min Run Time annel : Middle = FID * GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** 1.53 cm/min Attenuation = 40 Zero Offset = 5% art Speed = End Time = 13.088 min Min / Tick = 1.00art Time = 0.000 min 0. 0 10 20 30 40 50 60 70 80 190 mVolts 1 -11 Carbon Monox 1.783 2 -Methane >2.384 3. 4 Carbon Dioxi 4 594 5 +11 6 +GR' 7. 8 9 NMOC_(ppmv) 9.724 10 11 12 ..... ....



int Date: Thu Aug 23 16:12:00 2018 Page 1 of 1 itle : Fixed Gas from TCD
n File : i:\gc8a\2018\aug\23aug009.run itle thod File : i:\gc8a\methods\nmoc fixed_180627-2.mth mple ID : METHOD BLANK ijection Date: 8/23/2018 15:58 Calculation Date: 8/23/2018 16:11 : AS erator Detector Type: 3800 (10 Volts) rkstation: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz istrument : GC8A pannel : Front = TCD Run Time : 13.088 min GC Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** : Analysis in Mode ak Measurement: Peak Area lculation Type: External Standard Time Ret. Width 
 Peak
 Peak
 Result
 Time
 Width

 No.
 Name
 (% v/v)
 (min)
 (min)
 Counts)
 Code
 Codes

 1 Hydrogen
 0.116291
 1.896
 -0.034
 28
 BB
 3.6

 2 Carbon Dioxi
 2.445

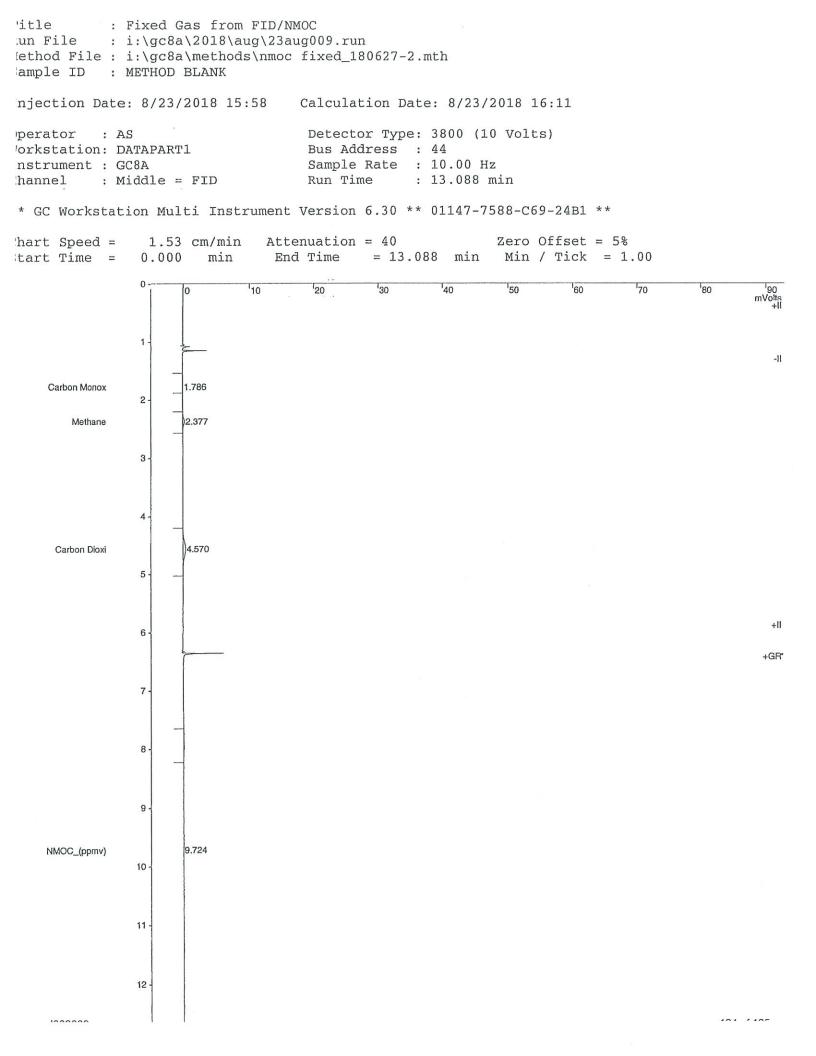
 3 Oxygen/Argon
 0.141045
 3.487
 0.031
 2054
 BB
 4.3

 4 Nitrogen
 0.425316
 4.044
 0.111
 6556
 BB
 7.3

 5 Methane
 4.997

 M 5 Methane 4.997 M ____ Totals: 0.682652 0.108 8638 atus Codes: - Missing peak tal Unidentified Counts : 1375 counts tected Peaks: 5 Rejected Peaks: 1 Identified Peaks: 5 iltiplier: 1 Divisor: 1 Unidentified Peak Factor: 0 LSB: 1 microVolts seline Offset: -1 microVolts pise (used): 5 microVolts - monitored before this run nual injection evision Log: 123/2018 16:11: Calculated results from channel Front using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' ream: 6, Advance Time: 15:57:12 iginal Notes: 

.....



it Date: Thu Aug 23 16:12:00 2018 Page 1 of 1 .e : Fixed Gas from FID/NMOC File : i:\gc8a\2018\aug\23aug009.run 10d File : i:\gc8a\methods\nmoc fixed_180627-2.mth )le ID : METHOD BLANK ection Date: 8/23/2018 15:58 Calculation Date: 8/23/2018 16:11 ator : AS Detector Type: 3800 (10 Volts) station: DATAPART1 Bus Address : 44 Sample Rate : 10.00 Hz :rument : GC8A nel : Middle = FID Run Time : 13.088 min 3C Workstation Multi Instrument Version 6.30 ** 01147-7588-C69-24B1 ** Mode : Analysis : Measurement: Peak Area ulation Type: External Standard Width Ret. Time ikPeakResultTimeOffsetAreaSep. 1/2Status>.Name(% v/v)(min)(min)(counts)Code (sec)Codes Status ...... _____ 

 1 Carbon Monox
 0.000031
 1.786
 0.018
 322
 BB
 0.0

 2 Methane
 0.000193
 2.377
 0.008
 2002
 BB
 7.6

 3 Carbon Dioxi
 0.000731
 4.570
 0.012
 7524
 BB
 18.3

 4 NMOC_(ppmv)
 1.013197
 9.724
 0.001
 1159
 GR
 0.0

 Totals:
 1.014152
 0.039
 11007

 ____ 1 Unidentified Counts : 0 counts Rejected Peaks: 0 Identified Peaks: 4 cted Peaks: 4 Unidentified Peak Factor: 0 iplier: 1 Divisor: 1 LSB: 1 microVolts line Offset: -11 microVolts se (used): 10 microVolts - monitored before this run al injection ision Log: 3/2018 16:11: Calculated results from channel Middle using method: 'i:\gc8a\methods\nmoc fixed_180627-2.mth' eam: 6, Advance Time: 15:57:12 jinal Notes: *******

**Appendix D** 

LandGEM Model Results for Puerto Rico Dump

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#### LandGEM Model Output PRD

			Biode	gradable wa	aste							Total dispo	sed waste		
Year		otal landfill ga (m3/year)		65% LFG (	(Maluaar)	Methane (m3/year)	(ou ftA2/mir		rear		otal landfill ga		(14-(	Methane	(au #40/
1975	(Mg/year)	(115/year) 0	(av 10-5/11/1) 0	05% LFG (	(Mg/year) 0	(moryear) 0	(av 10-3/11) 0	65% Methan 0	1975	(Mg/year) 0	(m3/year) 0	(av ft^3/mir 0	(Mg/year) 0	(m3/year) 0	(av ft^3/min 0
1976	84.97	69493.08	4.67	3.035	21.36		2.15		1976	110.87	90681.92	6.09	27.88		2.81
1977 1978	166.60 245.04	136261.29 200411.49	9.16 13.47	5.950997 8.752655	41.89 61.61	62789.20 92349.61	4.22 6.20	2.742219 4.033224	1977 1978	217.40 319.75	177808.15 261518.12	11.95 17.57	54.66 80.40	81934.00 120507.55	5,51 8,10
1979	320.40	262046.32	17.61	11.44446		120750.94	8.11	5.273607	1979	418.09	341945.76	22.98		157568.61	10,59
1980	392.80	321264.42	21.59	14.03072	98.76	148038.64	9.95	6.465354	1980	512.57	419219.80	28.17		193176.48	12.98
1981 1982	462.37 529.20	378160.54	25.41 29.08	16.51556		174256.37	11.71	7.610372	1981	603.34	493463.88	33.16		227388.15	15.28
1982	593.42	432825.73 485347.47	32.61	18.90298 21.19678		199446.10 223648.11	13.40 15.03	8.710493 9.767478	1982 1983	690.56 774.36	564796.80 633332.72	37.95 42.55		260258.37 291839.72	17.49 19.61
1984	655.12	535809.80	36.00	23.40065		246901.15	16,59	10.78302	1984	854.87	699181.31	46.98		322182.75	21.65
1985	714.40	584293.47	39.26	25.51809		269242.43	18.09	11.75874	1985	932.22	762447.94	51.23		351336.01	23.61
1986 1987	771.35 826.08	630876.08 675632.15	42.39 45.40	27.55252 29.50717		290707.70 311331.29	19.53 20.92	12.6962 13.5969	1986 1987	1006.54 1077.95	823233.85 881636.31	55.31		379346.16	25,49
1988	878.65	718633.31	48.28	31.38518		331146.23	22,25	14.46229	1988	1146.56	937748.78	59.24 63.01		406258.01 432114.64	27.30 29.03
1989	929.17	759948.37	51.06	33.18955	233.62	350184.21	23,53	15.29374	1989	1212.48	991661.04	66.63		456957.41	30.70
1990 1991	977.70 1024.33	799643.45	53.73	34.92316		368475.70	24.76	16.09259	1990		1043459.38	70.11		480826.08	32.31
1991	1024.33	837782.06 874425.23	56.29 58.75	36.58881 38.18914		386049.97 402935.15	25.94 27.07	16.86012 17.59756	1991 1992		1093226.67 1141042.56	73.45 76.67		503758.85 525792.41	33,85 35,33
1993	1112.18	909631.61	61.12	39.72672		419158.25	28.16	18.30607	1993		1186983.56	79.75		546962.03	36,75
1994	1153.54	943457.52	63.39	41.20402		434745.23	29.21	18.98681	1994	1505.26	1231123.19	82.72	378.47	567301.57	38.12
1995 1996	1193.27	975957.10 1007182.35	65.57 67.67	42.62339		449721.03	30.22	19.64086	1995		1273532.08	85.57		586843.58	39.43
1990		1007182.35	69.69	43.9871 45.29734		464109.63 477934.04	31,18 32,11	20.26926 20.87301	1996 1997		1314278.10 1353426.44	88.31 90.94		605619.35 623658.90	40.69 41.90
1998		1066007.79	71.62	46.55621		491216.39	33.00	21.4531	1998		1391039.75	93.46		640991.12	43.07
1999		1093702.10	73.49	47.76571		503977.93	33,86	22.01044	1999		1427178.22	95.89		657643.72	44.19
2000 2001		1120310.51 1145875.58	75.27 76.99	48.92779 50.04431		516239.08 528019.47	34.69 35.48	22.54593 23.06042	2000		1461899.68	98.22		673643.37	45.26
2002		1170438.24	78.64	51,11704		539337.94	36.24	23.55473	2001 2002		1495259.70 1527311.64	100.47 102.62		689015.67 703785.21	46.29 47.29
2003	1459.92	1194037,77	80.23	52.14771		550212.61	36,97	24,02967	2003		1558106.82	104.69		717975.62	48.24
2004		1216711.96	81.75	53.13797		560660,87		24.48598	2004		1587694.50	106.68	488.09	731609.62	49.16
2005 2006		1169004.00	78,55	51.0544		538677.04	36,19	23,52587	2005		1525440.11	102.49		702922.80	47.23
2008		1123166,70 1079126,70	75.47 72.51	49.05253 47.12915		517555.22 497261.59	34.77	22.60341 21.71711	2006 2007		1465626,74 1408158,70	98.48 94.61		675360.80 648879.53	45.38 43.60
2008		1036813.54	69,66	45,28119		477763.68	32,10	20,86557	2008		1352944.00	90.90		623436.60	41,89
2009	1217.98	996159,50	66,93	43,50569		459030,30	30,84	20.04742	2009		1299894,31	87.34	399.62	598991.30	40.25
2010 2011	1170.22 1124.33	957099.53 919571.12	64.31 61.79	41.79981 40,16082		441031.46 423738.37	29.63 28.47	19.26135 18.5061	2010 2011		1248924.73 1199953.69	83.92		575504.51	38.67
2012	1080.25	883514.22	59.36	38,58609		407123.35	27.35	17.78047	2011		1152902.83	80.62 77.46		552938,66 531257,62	37,15 35,70
2013	1037.89	848871,13	57.04	37.07311		391159.82	26,28	17.08329	2013		1107696,86	74.43		510426,71	34,30
2014 2015	997.19	815586,42	54.80	35.61945		375822.22	25.25	16,41344	2014		1064263,45	71.51		490412.60	32,95
2015	958.09 920.53	783606.82 752881.15	52.65 50,59	34.22279 32.8809		361086.02 346927.64	24.26 23.31	15.76986 15.15152	2015 2016	1250.22 1201.20	1022533.08 982438.99	68,70 66,01		471183.24 452707.88	31.66 30.42
2017	884.43	723360.26	48.60	31.59162		333324.41	22.40	14.55742	2010	1154.10	943917.00	63.42		434956.95	29.22
2018	849.75	694996.90	46.70	30.35289	213.66	320254.57	21.52	13,98661	2018	1108.85		60.93		417902.05	28.08
2019	816.43	667745.68	44.87	29.16274		307697.21	20.67	13.43819	2019	1065.37	871345.21	58.55		401515.87	26,98
2020 2021	784.42 753.66	641563.00 616406.95	43.11 41.42	28.01925 26.9206		295632.23 284040.32	19.86 19.08	12.91127 12.40501	2020 2021	1023.60	837179.28	56.25		385772.21	25.92
2022	724.11	592237.29	39.79	25.86503		272902.94	18.34	11.91861	2021	983.46 944.90	804353.01 772813.88	54.04 51.93		370645.87 356112.64	24.90 23.93
2023	695.72	569015.34	38.23	24.85085	· 174.93	262202.27	17.62	11.45127	2023	907.85	742511.41	49.89		342149.26	22.99
2024 2025	668.44	546703.93	36.73	23.87643		251921.17	16.93	11.00226	2024	872.25	713397.12	47.93		328733.39	22.09
2025	642.23 617.05	525267,36 504671,33	35.29 33.91	22.94022 22.04072		242043.20 232552.55	16.26 15.63	10.57085 10.15637	2025 2026	838.05 805.19	685424.42 658548.55	46.05 44.25		315843.57 303459.17	21.22 20.39
2027	592.85	484882.88	32.58	21.17649		223434.03	15.01	9.758129	2027	773.62	632726.49	42.51		291560.37	19,59
2028	569.61	465870.35	31.30	20.34615	143.22	214673.06	14.42	9.375507	2028	743.28	607916.93	40.85		280128,12	18.82
2029 2030	547.27 525.81	447603.32 430052.54	30.07 28.90	19.54837		206255.61	13.86	9.007888	2029	714.14	584080.16	39.24		269144.14	18,08
2030	505.20	413189.94	27.76	18.78187 18.04542		198168.21 190397.92	13.31 12.79	8.654684 8.315329	2030 2031	686.14 659.23	561178.05 539173.95	37.71 36.23		258590.85 248451.35	17.37 16.69
2032	485.39	396988,53	26,67	17.33785		182932.31	12.29	7.98928	2032	633,38	518032,63	34.81		238709.44	16,04
2033	466.35	381422,39	25.63	16,65802		175759.44	11.81	7.676016	2033	608.55	497720.28	33.44		229349.51	15,41
2034 2035	448.07	366466,60	24.62	16.00485		168867.81	11.35	7.375035	2034	584.69	478204.39	32.13		220356.58	14.81
2035	430.50 413.62	352097.24 338291.31	23.66 22.73	15.37729 14.77434		162246.41 155884.64	10,90 10,47	7.085856 6.808015	2035 2036	561.76 539.73	459453.73 441438.29	30.87 29.66		211716.28 203414.76	14.23 13.67
2037	397.40	325026,72	21.84	14,19503		149772.31	10.06	6.541069	2030	518.57	424129.25	28.50		195438.76	13,13
2038	381.82	312282,24	20,98	13,63843		143899.65	9.67	6,28459	2038	498.24	407498.90	27.38	125.27	187775.49	12.62
2039 2040	366.85 352.46	300037.48 288272.84	20,16 19,37	13,10366 12,58986	92.24 88.62	138257.27 132836.12	9.29 8.93	6.038168 5.801408	2039 2040	478.70 459.93	391520,64 376168,90	26.31		180412.71	12.12
2040	338.64	276969.50	19.37	12.09621		127627.54	8,93	5.573931	2040	459.93	361419.11	25.27 24.28		173338.63 166541.92	11.65 11.19
2042	325.36	266109.37	17.88	11.62191		122623.20	8.24	5.355374	2041	424.57	347247.66	23.33		160011.72	10.75
2043	312.61	255675.07	17.18	11.1662	78.60	117815.07	7.92	5.145387	2043	407.92	333631.88	22.42	102.57	153737.57	10.33
2044	300.35	245649.91	16.51	10.72837	75.52	113195.48	7.61	4.943634	2044	391.93	320549,99	21,54	98.54	147709.44	9.92

#### LandGEM Model Output PRD

			Biode	gradable wa	aste							Total dispos	sed waste		
Year	Т	otal landfill ga		gradable m	aste	Methane			Year		otal landfill ga	is		Methane	
			(av ft^3/mir 6			(m3/year)			ne Capture			(av ft^3/mir			(av ft^3/min 9.54
2045 2046	288.57 277.26	236017.84 226763.45	15.86 15.24	10.30771 9.903535	72.56 69.71	108757.02 104492.60	7.31 7.02	4.749791 4.563549	2045 2046	376,56 361,79	307981.05 295904.94	20.69 19.88		141917.67 136352.99	9.54
2040	266.39	217871.92	14.64	9.515212	66.98	100395.38	6.75	4.38461	2047	347.61	284302.34	19.10		131006.52	8.80
2048	255.94	209329.04	14.06	9.142115	64.35	96458.82	6.48	4.212687	2048	333.98	273154.68	18.35	83.97	125869.68	8.46
2049	245.91	201121.13	13.51	8.783648	61.83	92676.62	6.23	4.047505	2049	320.88	262444.14	17.63		120934.26	8.13
2050	236.26	193235.06	12.98	8.439236	59.40	89042.72	5.98	3.8888	2050	308.30	252153.55	16.94		116192.36 111636.39	7.81 7.50
2051 2052	227.00 218.10	185658.21 178378.44	12.47 11.99	8.108329 7.790397	57.08 54.84	85551.30 82196.79	5.75 5.52	3.736318 3.589815	2051 2052	296.21 284.60	242266.47 232767.07	16.28 15.64		107259.06	7.50
2052	209.55	171384.13	11.59	7.484931	52.69	78973.81	5.31	3.449056	2052	273.44	223640.14	15.03		103053.38	6.92
2054	201.33	164664.06	11.06	7.191443	50.62	75877.20	5.10	3.313817	2054	262.72	214871.08	14.44	66.06	99012.60	6.65
2055	193.44	158207.49	10.63	6.909462	48.64	72902.01	4.90	3.18388	2055	252.42	206445.87	13.87	63.47	95130.26	6.39
2056	185.85	152004.08	10.21	6.638538	46.73	70043.48	4.71	3.059038	2056	242.52	198351.01	13.33	60.98	91400.15	6.14
2057	178.56	146043.92	9.81 9.43	6.378238	44.90 43.14	67297.04 64658.28	4.52 4.34	2.939092 2.823848	2057 2058	233.01 223.87	190573.56 183101.06	12.80 12.30	58.59 56.29	87816.29 84372.97	5.90 5.67
2058 2059	171.56 164.84	140317.45 134815.53	9.43	6.128143 5.887855	43.14		4.34	2.713124	2059	215.09	175921.56	11.82	54.08	81064.66	5.45
2059	158.37	129529.34	8.70	5.656989	39.82	59687.12	4.01	2.606741	2060	206.66	169023.58	11.36	51.96	77886.07	5.23
2061	152.16	124450.42	8.36	5.435175	38.26		3.85	2.504529	2061	198.56	162396.07	10.91	49.92	74832.11	5.03
2062	146.20	119570.65	8.03	5.222059	36.76		3.70	2.406325	2062	190.77	156028.43	10.48	47.97	71897.90	4.83
2063	140.46	114882.21	7.72	5.017299	35.32		3.56	2.311972	2063	183.29	149910.47	10.07 9.68	46.09 44.28	69078.74 66370.13	4.64 4.46
2064	134.96 129.66	110377.62 106049.65	7.42 7.13	4.820568 4.631551	33.93 32.60		3.42 3.28	2.221318 2.134219	2064 2065	176.10 169.20	144032.40 138384.80	9.68	44.20	63767.72	4.40
2065 2066	129.66	101891.38	6.85	4.449945	31.32		3.15	2.050535	2005	162.56	132958.66	8.93	40.87	61267.35	4.12
2007	119.69	97896.17	6.58	4.27546	30.10		3.03	1.970132	2067	156.19	127745.27	8.58	39.27	58865.02	3.96
2068	115.00	94057.60	6.32	4.107817	28.92		2.91	1.892882	2068	150.07	122736.31	8.25	37.73	56556.89	3.80
2069	110.49	90369.55	6.07	3.946747	27.78		2.80	1.818661	2069	144.18	117923.75	7.92	36.25	54339.26	3.65
2070	106.16	86826.11	5.83	3.791993	26.69 25.65		2.69 2.58	1.74735 1.678836	2070 2071	138.53 133.10	113299.90 108857.34	7.61 7.31	34.83 33.47	52208.59 50161.46	3.51 3.37
2071 2072	102.00 98.00	83421.61 80150.60	5.61 5.39	3.643307 3.500451	25.65		2.58	1.613008	2071	127.88	104588.99	7.03	32.15	48194.60	3.24
2072	94.16	77007.85	5.17	3.363196	23.67	35485.22	2.38	1.549761	2073	122.86	100487.99	6.75	30.89	46304.87	3.11
2074	90.46	73988.33	4.97	3.231323	22.75	34093.82	2.29	1.488994	2074	118.05	96547.80	6.49	29.68	44489.23	2.99
2075	86.92	71087.21	4.78	3.104621	21.85		2.20	1.43061	2075	113.42	92762.11	6.23	28.52	42744.78	2.87
2076	83.51	68299.84	4.59	2.982888	21.00		2.11	1.374515	2076	108.97	89124.85	5.99	27.40 26.32	41068.73 39458.40	2.76 2.65
2077 2078	80.23 77.09	65621.76 63048.70	4.41 4.24	2.865927 2.753552	20.17 19.38		2.03 1.95	1.320619 1.268837	2077 2078	104.70 100.59	85630.22 82272.61	5.75 5.53	25.29	37911.22	2.55
2078	74.07	60576.52	4.07	2.645584	18.62		1.88	1.219085	2079	96.65	79046.65	5.31	24.30	36424.70	2.45
2080	71.16	58201.28	3.91	2.541849	17.89		1.80	1.171284	2080	92.86	75947.19	5.10	23.35	34996.47	2.35
2081	68.37	55919.18	3.76	2.442182	17.19		1.73	1.125357	2081	89.22	72969.26	4.90	22.43	33624.23	2.26
2082	65.69	53726.56	3.61	2.346422	16.52		1.66	1.081231	2082	85.72	70108.09	4.71	21.55	32305.81 31039.08	2.17 2.09
2083	63.11 60.64	51619.91 49595.86	3.47 3.33	2.254418 2.166021	15.87 15.25		1.60 1.54	1.038836	2083 2084	82.36 79.13	67359.12 64717.93	4.53 4.35	20.71 19.90	29822.02	2.09
2084 2085	58.26	49595.88	3.33	2.08109	14.65		1.48	0.958966	2085	76.03	62180.30	4.18	19.12	28652.68	1.93
2086	55.98	45782.75	3.08	1.999489	14.07		1.42	0.921365	2086	73.05	59742.18	4.01	18.37	27529.19	1.85
2087	53.78	43987.58	2.96	1.921088	13.52		1.36	0.885237	2087	70.18	57399.65	3.86	17.65		1.78
2088	51.67	42262.81	2.84	1.845761	12.99			0.850527	2088	67.43	55148.98	3.71	16.95		1.71
2089	49.65	40605.66	2.73 2.62	1.773388	12.48 11.99		1.26 1.21	0.817177	2089 2090	64.79 62.24	52986.56 50908.92	3.56 3.42	16.29 15.65	24416.21 23458.83	1.64 1.58
2090 2091	47.70 45.83	39013.49 37483.75	2.62	1.703852 1.637043	11.52		1.16	0.75435	2090	59.80	48912.76	3.29	15.04	22539.00	1.50
2092	44.03	36013.99	2.42	1.572854	11.07			0.724771	2092	57.46	46994.86	3.16	14.45		1.46
2093	42.31	34601.86	2.32	1.511182	10.64		1.07	0.696352	2093	55.21	45152.17	3.03	13.88	20806.12	1.40
2094	40.65	33245.10		1.451927	10.22		1.03	0.669048	2094	53.04	43381.72	2.91	13.34	19990.30	1.34
2095	39.05	31941.54	2.15	1.394996	9.82 9.43		0.99	0.642814 0.617609	2095 2096	50.96 48.96	41680.70 40046.38	2.80 2.69	12.81 12.31	19206.47 18453.37	1.29 1.24
2096 2097	37.52 36.05	30689.10 29485.76		1.340298 1.287744	9.43		0.95	0.593392	2090	48.90	38476.14	2.09	11.83	17729.80	1.19
2097		28329.61	1.90	1.237251	8.71			0.570125	2098	45.20	36967.47	2.48	11.36	17034.61	1.14
2099				1.188737	8.37			0.54777	2099	43.43	35517.95	2.39	10.92		1.10
2100		26151.52		1.142126	8.04			0.526292	2100	41.72	34125.27	2.29	10.49		1.06
2101	30.72		1.69	1.097343	7.72			0.505656	2101	40.09	32787.20	2.20	10.08 9.68		1.02 0.98
2102				1.054316	7.42			0.485829	2102 2103	38.52 37.01	31501.60 30266.40	2.12 2.03	9.00		0.98
2103 2104				0.973256	6.85			0.448476	2103	35.55	29079.64	1.95	8.94	13399.90	0.90
2104				0.935094	6.58		0.66	0.430891	2105	34.16	27939.41	1.88	8.59	12874.48	0.87
2106	25.15	20571.52	1.38	0.898428	6.32			0.413996	2106	32.82	26843.89	1.80	8.25		0.83
2107					6.08			0.397763	2107	31.53	25791.33	1.73	7.93		0.80
2108				0.829354	5.84			0.382166	2108 2109	30.30 29.11	24780.03 23808.39	1.66 1.60	7.62		0.77 0.74
2109 2110				0.796835	5.61			0.367181	2109	29.11 27.97	23808.39	1.60	7.03		
2110					5.18			0.338951	2110	26.87	21977.92	1.48	6.76		
2112					4.97			0.325661	2112	25.82	21116.15	1.42	6.49	9730.32	0.65
2113	19.01	15547.62	1.04		4.78			0.312891	2113	24.81	20288.18	1.36	6.24	9348.79	
2114					4.59			0.300623		23.83	19492.67	1.31	5.99		
2115	17.55	14352.26	0.96	0.626812	4.41	6613.52	0.44	0.288835	2115	22.90	18728.35	1.26	5.76	8630.02	0.58

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**Appendix E** 

LandGEM Model Results for Marpi Solid Waste Facility This page intentionally left blank

				egradable wa	iste									Total dispos	ed waste		
Year		Total landfill gas				Methane				Year			Total landfill gas			Methane	
200	(Mg/year)	(m3/year) 0	(av ft^3/min 0	75% LFG C ( 0	Mg/year) 0		(av ft^3/min 0	75% Metha 0	Btu		2003	(Mg/year)	(m3/year)	(av ft^3/mir (l	Mg/year) 0	(m3/year)	(av ft^3/min
200				7,640558	60.69		6,11		3557,444		2003	263.86	200575,52	13,48	80.29	120345.31	
200		294076.69	19.76	14.81923	117.72	176446.01	11.86	8.89154	6899,835		2005	511.84	389072.49	26.14	155.74	233443.50	
200		418013.00	28.09	21.06468	167.33	250807.80	16.85	12.63881	9807,716		2006	733.54	557598.52	37.46	223,20	334559,11	
200		524135.80	35.22	26.41247	209.81	314481.48	21.13	15.84748	12297.64		2007	938.82	713638.85	47.95	285.66	428183.31	
200 200		624818.85 704104.02	41.98 47.31	31.48613 35.4815	250.11	374891,31	25.19	18.89168	14659.94		2008	1130.85	859612.03	57.76	344.09	515767.22	
200		766311.15	51.49	35.4615	281.85 306.75		28.39 30.89	21.2889 23.16976	16520.19 17979.73		2009 2010	1261.80 1359.81	959151.88 1033652.23	64.45 69.45	383.94 413,76	575491.13 620191.34	
201		828523.54	55.67	41.7513	331.65		33.40	25.05078	19439.4		2010	1467.70	1115661.43	74.96	446.59	669396.86	
201	2 1170.18	889507.42	59.77	44.82442	356.06		35.86	26.89465	20870.25		2012	1574.29	1196685,79	80,41	479.02	718011.47	
201		920019.03	61.82	46.36197	368.27	552011.42	37.09	27.81718	21586.14		2013	1632.37	1240836.36	83.37	496.69	744501.82	
201		978849.97	65.77	49.32661	391.82		39.46	29.59596	22966.47		2014	1718.47	1306283.60	87.77	522.89	783770,16	
201 201		1037597.34 1096032.37	69.72 73,64	52.28703	415.34	622558.40	41.83	31.37222	24344.84		2015	1796.54	1365632.00	91.76	546.65	819379.20	
201		1183902.62	79.55	55.23171 59.6597	438.73 473.90	657619.42 710341.57	44.19 47.73	33.13903 35.79582	25715.88 27777.56		2016 2017	1893.85 2052.74	1439600.10 1560383.80	96.73 104.84	576.26 624.60	863760.06 936230.28	
201		1271680.27	85.44	64.08303	509.04	763008.16	51.27	38,44982	29837.06		2018	2183.73	1659950.64	111,53	664.46	936230.28	
201	9 1756.68	1335333.62	89.72	67.29068	534.52	801200.17	53.83	40.37441	31330.54		2019	2292.97	1742991.57	117,11	697.70	1045794.94	
202		1397285,70	93.88	70.41259	559.32		56.33	42.24756	32784.1		2020	2399.30	1823813,32	122.54	730.05	1094287.99	
202		1457608.78	97.94	73.45242	583.46		58.76	44.07145			2021	2502.83	1902510.16	127.83	761.55	1141506.10	
202 202			101.88	76.41365	606.99 629.91	909823.40 944185.90	61.13	45.84819	35578.2		2022	2603.68	1979172.73	132.98	792.24	1187503.64	
202			109.48	82.1137	652.27	977691.29	63.44 65.69	47.5798 49.26822	36921.93 38232.14		2023 2024	2701.97 2797.81	2053888.13 2126740.14	138.00 142.90	822.15 851.31	1232332.88 1276044.09	
202			113.15		674.07		67.89	50.91531	39510.28		2025	2891.30	2197809.29	147.67	879.76	1318685.57	
202			116.72		695.35	1042277.45	70.03	52.52287			2026	2982.55	2267173.00	152.33	907.52	1360303.80	
202			120.21	90.15438	716.14		72.12	54.09263			2027	3071.66	2334905.70	156.88	934.64	1400943.42	
202		1839769.01	123.61	92.71039	736.44		74.17	55.62624	43165.96		2028	3158.71	2401078.97	161.33	961.13	1440647.38	
202		1889348.48 1937835.93	126.95 130.20	95.20882 97.65222	756.29 775.69		76.17 78.12	57.12529 58.59133	44329.23 45466.87		2029 2030	3243.80 3327.02	2465761.64 2529019.87	165,67 169,92	987.02 1012.34	1479456.98 1517411.92	
203		1985280,16	133,39	100.043	794,69		80.03	60.02583	46580.04		2030	3408.45	2529019.87	174.08	1012.34	1554550,39	
203			136.51	102.3837	813.28		81.91	61.4302	47669.84		2031	3408.45	2651515.15	178.15	1061.37	1590909.09	
203		2077224.76	139.57	104.6764	831.49		83.74	62.80582	48737.31		2033	3566.26	2710872.23	182.14	1085,13	1626523.34	
203			142.56	106.9233	849.34		85.54	64.15398	49783.49		2034	3642.79	2769045.17	186.05	1108.42	1661427.10	111.63
203			145.50	109,1266	866.84	1299321.86	87.30	65,47596	50809.34		2035	3717.83	2826088,38	189.88	1131.25	1695653.03	
203 203			148.38 151.21	111.2883 113.4103	884.01 900.87	1325059.96 1350325.65	89.03	66.77296 68.04616	51815.82 52803.82		2036	3791.45	2882054.23	193.64	1153.65	1729232.54	
203			153.99	115,4945	917.42		90.73 92.40	69.29668	53774.22		2037 2038	3863.73 3934.71	2936993.08 2990953.36	197.34 200.96	1175.65 1197.25	1762195.85	
203			156.72	117.5427	933.69		94.03	70.52559	54727.86		2039	4004.47	3043981,69	204.52	1218,47	1826389.01	122.71
204			159.41	119.5566	949.69		95.65	71.73394	55665.54		2040	4073.07	3096122.87	208.03	1239.34	1857673.72	
204			162.05	121.5379	965.43		97.23	72.92273	56588.04		2041	4140.55	3147420.06	211.47	1259.88	1888452.04	
204 204		2450531.44 2488649,15	164.65	123.4882	980.92		98.79	74.09291	57496.1		2042	4206.98	3197914.74	214.87	1280.09	1918748.84	
204		2526211.68	167.21 169.74	125,409 127,3019	996.18 1011.21	1493189.49 1515727.01	100.33	75.24542 76.38113	58390.44 59271.76		2043 2044	4272.40 4336.88	3247646.84 3296654.79	218.21	1300.00	1948588,10	
204			172.22	129.1682	1026.04		103.33	77.50093	60140.72		2044	4400.44	3344975.56	221.50 224.75	1319.61 1338.96	1977992.87 2006985.33	132.90 134.85
204			174.68	131.0094	1040.66		104.81	78.60561	60997.95		2046	4463.15	3392644.73	227.95	1358.04	2035586.84	
204		2635846,31	177.10	132,8266	1055.10		106,26	79.69599	61844.09		2047	4525.05	3439696,56	231.11	1376.87	2063817.94	
204		2671461.10	179.50	134.6214	1069.36		107.70	80.77282	62679.7		2048	4586.18	3486164.02	234.23	1395.47	2091698.41	140.54
204 205		2706652.19	181.86	136.3947	1083.44		109.12	81.83683	63505.38		2049	4646.59	3532078.85	237.32	1413.85	2119247,31	142.39
205		2600522.84 2498554.88	174.73 167.88	131.0466 125.9082	1040.96 1000.14		104.84	78.62797 75.54492	61015.3 58622.86		2050 2051	4706.30 4765.37	3577471.59 3622371.67	240.37	1432.02	2146482.95	
205		2490585.14	161.30	120.9713	960.93		96,78	72.58276	56324.22		2051	4/65.37 4823.83	3622371.67 3666807.41	243.39 246.37	1450.00 1467.78	2173423.00 2200084.45	
205	3 3034.23	2306456.85	154.97	116.2279	923.25		92,98	69,73675	54115.72		2053	4881.71	3710806,11	249.33	1485.39	2226483.66	
205			148.89	111.6706	887.05	1329611.63	89.34	67.00233	51993.81		2054	4939.05	3754394.02	252.26	1502.84	2252636.41	151.35
205			143.06	107.2919	852.27	1277476.81	85.83	64.37513	49955.1		2055	4995.88	3797596,46	255,16	1520.14	2278557.88	
205 205		2045643.72 1965432.88	137.45 132.06	103.0849 99.0429	818.85 786.74		82.47 79.23	61.85095	47996.34		2056	5052.24	3840437.81	258.04	1537.29	2304262.69	
205		1888367.15	126.88	99.0429	755.89		79.23	59.42574 57.09562	46114.37 44306.2		2057 2058	5108.16 5163.66	3882941,56 3925130,33	260,89 263,73	1554.30 1571.19	2329764.93 2355078.20	
205		1814323.22	121.90	91,42812	726.25		73.14	54.85687	42568.93		2059	5218.78	3967025,95	266,54	1587.96	2380215.57	159.93
206		1743182.59	117.12	87.84317	697.78		70.27	52.7059	40899.78		2060	5273.53	4008649.44	269.34	1604.62	2405189.66	161.60
206		1674831.42	112.53		670.42	1004898.85	67.52	50.63927	39296.08		2061	5327.96	4050021.05	272.12	1621.18	2430012.63	
206		1609160.34	108.12	81.08947	644.13	965496.21	64.87	48.65368	37755.26		2062	5382.08	4091160.33	274.88	1637.65	2454696.20	164.93
206 206		1546064.26 1485442.22	103,88	77.9099	618.87	927638.56	62.33	46.74594	36274.85		2063	5435.92	4132086.12	277.63	1654.03	2479251.67	166.58
206		1485442.22 1427197.19	99.81 95.89	74.85501 71.9199	594.61 571.29	891265.33 856318.32	59.88 57.54	44.91301 43.15194	34852.49 33485.91		2064 2065	5489.50 5542.85	4172816.58 4213369,24	280.37	1670.33	2503689.95	
200		1371235.99	92.13	69.09988	548.89		55.28	43.15194 41.45993	33485.91 32172.91		2065	5542.85	4213369.24 4253761.00	283.10 285.81	1686.57 1702.73	2528021.54 2552256.60	169.86 171.49
206	7 1733.18	1317469.06	88,52	66.39044	527.37	790481.44	53.11	39.83426	30911.39		2067	5648.93	4294008.18	288,51	1718.84	2576404.91	173.11
206			85.05	63.78723	506.69		51.03	38.27234	29699.34		2068	5701.71	4334126.53	291.21	1734.90	2600475.92	174.73
206		1216177.22	81.71	61.2861	486.82		49.03	36.77166			2069	5478.14	4164183.00	279.79	1666,88	2498509,80	167.87
207	1537.19	1168490.23	78.51	58.88304	467.73	701094.14	47.11	35.32982	27415.94		2070	5263.34	4000903.05	268.82	1601.52	2400541.83	161.29

			Biode	gradable wa	aste								Total dispo	sed waste			
Year		Total landfill gas		-		Methane				Year		Total landfill gas			Methane		
			(av ft^3/min				(av ft^3/min		Btu 26340.95	2071	(Mg/year) 5056.96	(m3/year) 3844025.39	(av ft^3/min) 258.28	(Mg/year) 1538.72	(m3/year) 2306415.24	(av ft^3/min 154.97	
2071 2072	1476.92 1419.01	1122673.08 1078652.43	75.43 72.47	56.5742 54.35589	449.39 431.77	673603.85 647191.46	43.48	32.61354	25308.1	2071	4858.68	3693299.00	248.15	1478.39	2215979.40	148.89	
2072	1363.37	1036357.87	69.63	52.22457	414.84	621814.72	41.78	31.33474		2073	4668.17	3548482.68	238.42	1420.42	2129089.61	143.05	
2074		995721.69	66.90	50.17681	398.58	597433.02	40.14	30.10609	23362.32	2074	4485.12	3409344.68	229.07	1364.72	2045606.81	137.44	
2075		956678.89	64.28	48.20935	382.95	574007.33	38.57	28.92561	22446.27	2075		3275662.36	220.09	1311.21	1965397.42	132.05	
2076		919166.97	61.76	46.31904 44.50284	367.93 353.51	551500.18 529875.55	37.06 35.60	27.79142 26.70171		2076 2077	4140.29 3977.95	3147221.81 3023817.47	211.46 203.17	1259.80 1210.40	1888333.08 1814290.48	126.88 121.90	
2077 2078		883125.92 848498.06	59.34 57.01	44.50284	339.64	509098.83	34.21	25.65472		2078		2905251.89	195.20	1162.94	1743151.14	117.12	
2079		815227.97	54.78	41.0813	326.33	489136.78	32.87	24.64878		2079		2791335.34	187.55	1117.34	1674801.20	112.53	
2080	1030.41	783262.43	52.63	39.47048	313.53	469957.46	31.58	23.68229	18377.46	2080	3528.12	2681885.51	180.20	1073.53	1609131.31	108.12	
2081	990.01	752550.27	50.56	37.92282	301.24	451530.16	30.34	22.75369 21.86151	17656.87 16964.53	2081 2082	3389.78 3256.87	2576727.28 2475692.36	173.13 166.34	1031.44 990.99	1546036.37 1485415.41	103.88 99.80	
2082 2083		723042.35 694691.45	48.58 46.68	36.43585 35.00718	289.43 278.08	433825.41 416814.87	29.15 28.01	21.00431	16299.34	2082		2378619.07	159.82	952.14	1427171.44	95.89	
2084		667452.21	44.85	33.63452	267.17	400471.33	26.91	20.18071	15660.23	2084	3006.47	2285352.08	153.55	914.80	1371211.25	92.13	
2085	843.63	641281.04	43.09	32.3157	256.70	384768.62	25.85	19.38942	15046.19	2085		2195742.15	147.53	878.93	1317445.29	88.52	
2086		616136.05	41.40	31.04858	246.63	369681.63	24.84	18.62915	14456.22	2086		2109645.87	141.75	844.47	1265787.52	85.05 81.71	
2087	778.77	591977.01	39.77 38.22	29.83115 28.66145	236.96 227.67	355186.20 341259.15	23.86 22.93	17.89869 17.19687	13889.38 13344.77	2087 2088	2666.50 2561.94	2026925.47 1947448.58	136.19 130.85	811.36 779.54	1216155.28 1168469.15	78.51	
2088 2089		568765.26 546463.65	36.72	27.53762	218.74	327878.19	22.03	16.52257	12821.52	2089		1871088.03	125.72	748.98	1122652.82	75.43	
2000		525036.51	35.28	26.45785	210.17	315021.90	21.17	15.87471	12318.78	2090	2364.97	1797721.62	120,79	719.61	1078632.97	72.47	
2091	663.62	504449.53	33.89	25.42043	201.93	302669.72	20.34	15.25226	11835.75	2091	2272.24	1727231.95	116.05	691.39	1036339.17	69.63	
2092		484669.78	32.56	24.42368	194.01	290801.87	19.54	14.65421 14.07961	11371.66 10925.77	2092 2093		1659506.21 1594436.05	111.50 107.13	664.28 638.24	995703.73 956661.63	66.90 64.28	
2093 2094		465665.61 447406.60	31.29 30.06	23.46601 22.5459	186.40 179.09	279399.36 268443.96	18.77 18.04	13,52754	10925.77	2093		1531917.31	107.13	613.21	919150.39	61.76	
2094		429863.53	28.88	21.66186	172.07	257918.12	17.33	12.99712	10085.76	2095		1471849.98	98.89	589.17	883109.99	59.34	
2096		413008.34	27.75	20.81249	165.32	247805.01	16.65	12.48749		2096		1414137.91	95.02	566.06	848482.75	57.01	
2097		396814.05	26.66	19.99642	158.84	238088.43	16.00	11.99785		2097		1358688.77	91.29	543.87 522.54	815213.26 783248.29	54.77	
2098		381254.75	25.62	19.21235	152.61	228752.85 219783.32	15.37 14.77	11.52741 11.07541	8945.268 8594.519	2098 2099		1305413.82 1254227.82	87.71 84.27	522.54	752536.69	52.63 50.56	
2099 2100		366305.54 351942.49	24.61 23.65	18.45902 17.73523	146.63 140.88	211165.50	14.19	10.64114		2100		1205048.84	80.97	482.37	723029.30	48.58	
2101		338142.63	22.72	17.03982	135.35		13.63	10.22389	7933.741	2101	1523.13	1157798.20	77.79	463.45	694678.92	46.68	
2102	427.40	324883.87	21.83	16.37168	130.05		13.10	9.823008		2102		1112400.28	74.74	445.28	667440.17	44.85	
2103		312144.99	20.97	15.72974	124.95		12.58	9.437843		2103 2104			71.81 69.00	427.82 411.05	641269.47 616124.93	43.09 41.40	
2104 2105		299905.61 288146.14	20.15 19.36	15.11297 14.52038	120.05 115.34		12.09 11.62	9.06778 8.712227		2104			66.29	394.93	591966.33	39.77	
2106		276847.77	18.60	13.95103	110.82		11.16	8.370616		2106		947924.99	63,69	379.44	568754.99		
2107		265992.42	17.87	13.404	106.47	159595.45	10.72	8.042399		2107		910756.32	61.19	364.57	546453.79		
2108			17.17	12.87842	102.30		10.30	7.727052		2108		875045.05	58.79	350.27	525027.03	35.28	
2109			16.50 15.85	12.37345 11.88828	98.29 94.43		9.90 9.51	7.42407 7.132968	5761.078 5535.183	2109 2110			56.49 54.27	336.54 323.34	504440.43 484661.04	33.89 32.56	
2110			15.23	11.42213	90.73		9.14	6.85328		2111		776095.34	52.15	310.66	465657.21	31.29	
2112			14.63	10.97427	87.17		8.78	6.584559	5109.618	2112	980.95	745664.21	50.10	298.48	447398.53	30.06	
2113			14.06	10.54396	83.76		8.44	6.326375		2113			48.14	286.78	429855.78		
2114		201032.74	13.51	10.13052	80.47		8.10	6.078314		2114		688334.82 661344.83	46.25 44.44	275.53 264.73	413000.89 396806.90	27.75 26.66	
2115			12.98 12.47	9.733301 9.351652	77.32 74.28		7.79 7.48	5.83998 5.610991	4531.825 4354.129	2115 2116		635413.12	42.69	254.35	381247.87	25.62	
2117			11.98	8.984969	71.37		7.19	5.390981	4183.402	2117			41.02	244.38	366298.93		
2118			11.51	8.632663	68.57	102785.28	6.91	5.179598	4019.368	2118			39.41	234.79	351936.14		
2119		164591.69	11.06	8.294172	65.88		6.64	4.976503					37.87	225.59	338136.53		
2120		158137.96	10.63	7.968953 7.656485	63.30 60.82		6.38 6.13	4.781372 4.593891	3710.344 3564.86	2120			36.38 34.95	216.74 208.24	324878.01 312139.36	21.83 20.97	
212			10.21 9.81	7.35627	58.43		5.89	4.413762					33.58	200.08	299900.20		
2123		140255.79	9.42	7.067827	56.14		5.65	4.240696	3290.78	2123	631.77	480234.91	32.27	192.23	288140.94		
2124			9.05	6.790693	53.94		5.43	4.074416	3161.747	2124			31.00	184.70	276842.78		
212			8.70	6.524427	51.83		5.22 5.01	3.914656		2125			29.79 28.62	177.45 170.50	265987.62 255558.09		
212			8.36 8.03	6.2686 6.022805	49.79 47.84		4.82	3.76116 3.613683					27.50	163.81	245537.52		
212			7.72	5.786647	45.97		4.63	3.471988		2128				157.39	235909.85	15.85	
2129			7.41	5.55975	44.16		4.45	3.33585						151.22			
213			7.12	5.341749	42.43		4.27	3.205049					24.39	145.29			
213			6.84	5.132296	40.77			3.079377 2.958633		2131 2132			23.43 22.51	139.59 134.12			
213			6.57 6.32	4.931055 4.737706	39.17 37.63			2.930633						128.86			
213			6.07	4.551938	36.16			2.731163			406.88	309288.77	20.78	123.80	185573.26	12.47	
213	5 114.17	86787.95	5.83	4.373454	34.74		3.50	2.624072						118.95			
213			5.60	4.201968	33.38		3.36	2.521181					19.18 18.43	114.29 109.81	171305.71 164588.72		
213 213			5.38 5.17	4.037207 3.878906	32.07 30.81			2.422324 2.327343					17.71	105.50			
213			4.97	3.726812	29.60			2.236087					17.01	101.36			
214			4.77	3.580681	28.44	42633.58	2.86	2.148409						97.39			
214	1 89.81	68269.82	4.59	3.440281	27.33			2.064168						93.57			
214			4.41	3.305385 3.175779	26.26			1.983231		2142				89.90 86.38			
214	3 82.91	63020.99	4.23	3.1/3//9	23.23	57012.59	2.04	1.505400	1470.040	2140	200.07	210/00.40	14.00	00.00	120110.01	00	

Year	Tot	Inven al landfill ga	tory conver as	itional until	2019 Methane	Year			Reachate re tal landfill ga		from 2020	Methane	Yea		Total	tal landfill g	95		Methane	
				(Mg/year)		(av ft^3/min)					(Mg/year)		(av ft^3/min)		(Mg/year)	(m3/year)	as (av ft^3/mir	(Mg/year)		(av ft^3
2003	0	0	0	0	0	0					, ,			2003	0	0	0	0	(m3/year) 0	)
2004 2005	199.4635 386.8692					6.112446 11.85539													90972.72	
	549.9122		28.08624	167.326		16.85175								2005			19.75898 28.08624		176446 250807.8	
		524135.8																	314481.5	
	821.9732	624818.9												2008	821.9732	624818.9	41.9815	250.1081	374891.3	3 25.1
	020.2100				422462.4	20,0002								2009					422462.4	
		766311.1 828523.5	51,48835		459786.7									2010					459786.7	
	1170,181	889507.4			533704 5									2011	1089.955				497114.1 533704.5	
2013					552011.4									2012	1210.32		61.81597		552011.4	
	1287.715	978850	65,76881	391.8229	587310	39,46129								2014	1287,715	978850	65.76881	391.8229	587310	39.46
2010	1364.999				622558.4									2015	1364,999	1037597	69,71604			
	1441.873				657619.4 710341.6									2016	1441.873				657619.4	
		1271680	85.44404	509 0397	763008.2	51,26643								2017	1557.469 1672.944				710341.6	
	1756.683	1335334			801200.2									2019	1756.683	1335334	89.7209		801200.2	
2020					838371.4		2020	0	0	0	0	0	0	2020	1838,183	1397286			838371.4	
	1766.107		90.20223		805498.4		2021	1928,677						2021	3694,784		188,7076	1124.24		
2022	1696.857	1289857	86.66535 83.26716			51,99921	2022	2899.93		148.1112		1322620			4596.787		234.7765	1398,7		
	1566.396	1190688	80,0022			49,96029 48,00132	2023	3395.835 3655.785		173.4391 186.7158		1548796	104.0634	2023	5026.157 5222.181	3820609 3969615	256,7062	1529.348 1588.993		
	1504,977		76,86527		686400.5		2025	3798,658			1155.847		116.4077	2024	5303.635		270.8781			
2026	1445.966	1099144	73,85134			44.31081	2026	3883,49			1181,659		119.0073	2026			272,1969			
	1389.269				633627.5		2027	3939,596		201.2111	1198.731	1796799	120.7267	2027	5328.865	4050710	272.1667	1621.455	2430426	
	1334.795		68.17338 65.50026		608782.6		2028	3981,535		203.3531		1815927	122.0119	2028	5316.33		271,5265		2424709	
2029			62.93196		561977.2	39.30016 37.75918	2029	4016.538 4048.195	3053151	205.1409	1222.143	1831891	123.0845	2029	5298.995 5280.366		270.6411 269.6897			
	1183.857				539941.7		2031	4078.292		208.2949	1240.933	1860056	124.9769	2030	5262.148	3999996	269.6897			
2032	1137.437				518770.3		2032	4107.713	3122458		1249.886		125.8785	2032	5245.15		267.8911			
	1092.838		55.81564			33.48939	2033	4136.901		211.2883	1258.767	1886787	126.773	2033		3975359	267.1039	1591.293	2385216	
2034	1049,987		53.62708		478885.4		2034	4166,074		212,7783	1267.644	1900092		2034			266,4054			
2035	969.26		51,52433			30.9146 29.70242	2035	4195,344 4224,764	3189070	214.2732	1276.55	1913442	128.5639	2035 2036	5204.16 5194.024		265.7975 265.2799			
	931,2548				424733.2		2037	4254.364		217.2876	1294.508		130.3726	2030			264,8506			
		680132	45,69798	272.2494	408079.2	27.41879	2038	4284,158	3256581	218,8093	1303,574		131,2856		5178.897		264,5073			
	859,6565		43,90614			26,34368	2039	4314.153		220.3413	1312.701	1967629		2039	5173.81					
2040	825,9489 793 563				376704.6 361933.8	25.31073	2040	4344,356 4374,768	3302340		1321.891		133,1303		5170.304		264.0684			
						23.36475	2041	4405.392	3325458	223,4371	1331,144		134.0623		5168.331 5167.839		263,9676 263,9425			
2043	732,5509		37,41434				2043	4436.23		226.5762	1349,846		135,9457		5168,781		263,9425			
	703,8272					21,56838	2044	4467.284	3395784	228,1623	1359,295	2037470	136,8974	2044	5171.111	3930794	264,1096			158.
	676,2297				308419.6		2045	4498,555		229.7594	1368.81		137.8557		5174.785		264,2972			
	649.7144 624.2387	493877.2	33,18355 31,8824				2046	4530.045 4561.755		231.3677 232.9873	1378.392		138.8206		5179,759			1576.085		
2048					273543.7		2047	4593.687			1388.04		139,7924		5185.994 5193.449		264.8697 265.2505	1577.982	2365264	
2049					262817.9		2049		3516312			2109787				3954341		1582.88		
	553,6501		28,27715			16,96629	2050	2297,126		117.3235	698,9642	1047689	70.39411		2850,776		145,6007			87.
	531,9412 511,0834		27,16839			16,30103	2051		867111.8					2051	1672.66				762878.5	
	491,0436	388497.5				15,66186 15,04775	2052	566,4642	430595 213827.1		172,3624		17.35897	2052	1077.548				491455.5	
	471,7895	358628.4	24.0962		215177.1		2055	139 6884	106183.4	7.134451	42 50406	63710.05		2053	772,3414 611,4778				352254.9 278887.1	
2055	453,2904	344566.4	23,15138	137,9262	206739.8	13,89083	2055		52729,12			31637.47				397295.5			238377.3	
	435,5166	331055.8	22.2436	132,518		13,34616	2056		26184.51		10.48137	15710.7		2056	469,9633	357240.3	24.00293	142.9994	214344.2	14.4
	418,4397		21.37141			12.82285	2057		13002.84				0.524196						198646.6	
2058		293620.1	20,53343	122.3295		12,32006	2058	8.494458	6457.02 3206,461			3874.212		2058 2059	410,5269		20,96727		187236 178096	
		282107.1					2060	2.094708	1592,282	0.106985	0.637373	955.3689		2059		296826.6 283699.4				
	356,5708	271045.5	18,21152	108,4966	162627.3	10,92691	2061		790,7036			474.4222		2061					163101.7	
	342,5895		17,49743				2062		392.6518					2062		260810.3	17.52382	104.3995	156486,2	10.5
	329,1564	250206.6	16.81135				2063	0.25651	194.9851			116,9911			329,4129		16.82445		150240,9	
	303.8496		16,15217 15,51883			9.6913 9.311299	2064	0.127379	96.82674 48.08274		0.038759		0.003903 0.001938		316.3773 303.9129				144295.6 138610.7	
	291,9355		14,91033			8,946197	2066		23.87718			14.32631							133162.3	
2067			14.32569			8,595412	2067		11.85706										127934.3	
	269,4904		13,76397			8.258381	2068	0.007746		0,000396	0.002357	3,532824	0.000237	2068					122914.6	
2069			13,22428			7.934565	2069		2.923914			1.754349							118093.4	
2070	248,771 239,0166	189102.1 181687.3	12,70574 12,20754			7.623446	2070	0.00191			0.000581	0.871184			248,7729 239,0175	189103.5			113462.1	
	229,6446		11.72888				2071	0.000949		4.84E-05 2.41E-05		0.432617	2,91E-05	2071	239,0175	181688		72.72771 69.87588	109012.8	
2073	220,6401		11,26898				2073			1,19E-05		0,106682			229,6451	167718.7			100631.2	
	211,9887	161142.1	10,82712	64,50343	96685.29	6.496273	2074	0.000116	0.088295	5.93E-06	3.53E-05	0.052977	3.56E-06	2074					96685.34	
2075			10,40258				2075		0.043846			0.026307							92894.23	
2076	195,6902		9.994692		89251.77 85752.16		2076	2.86E-05	0.021773	1.46E-06	8.72E-06	0.013064		2076	195.6902				89251.78	
	100,01/1					5,761677 5,535758	2077	1.42E-05 7.06E-06	0.010812	7.26E-07 3.61E-07	4.33E-06 2.15E-06	0.006487		2077	188,0171	142920.3			85752.16	
2077 2078	180,6448	137316 3																		
2077	180.6448 173.5617	137316.3 131932	8.864497			5.318698	2079	3.51E-06							173 5617		elenene.			5 31
2077 2078 2079 2080	173.5617	131932 126758.9	8.864497 8.516915	52.81094 50.7402	79159.22 76055.34	5.318698 5.110149				1.79E-07 8.9E-08	1.07E-06		1.07E-07	2079	173,5617 166,7562		8.864497	52.81094	79159.22	

2082	153.9354	117013.2	7.862103	46.83911	70207.93	4.717262	2082					0.000196							70207.93	
2083	147.8995	112425.1	7.553826	45.00252	67455.03	4.532296	2083	2.13E-07	0.000162	1.09E-08	6.49E-08	9.73E-05	6.54E-09	2083	147.8995	112425.1	7.553826	45,00252	67455.03	4.532296
2084	142,1003	108016.8	7 257636	43 23794	64810.08	4 354582	2084	1.06E-07	8.05E-05	5.41E-09	3.22E-08	4.83E-05	3.25E-09	2084	142.1003	108016.8	7.257636	43.23794	64810.08	4.354582
2085		103781.4			62268.85			5.26E-08		2.69E-09	1.6E-08	2.4E-05	1.61E-09	2085	136.5284	103781.4			62268.85	
	130.5204	103701.4	0.97300	41.34230	02200.00	4.103030								2086					59827.25	
2086					59827.25		2086	2.61E-08		1.33E-09	7.95E-09	1.19E-05	8E-10		131.1751					
2087	126.0316	95802.31	6.436946	38.34862	57481.39		2087	1.3E-08		6.62E-10	3.95E-09	5.92E-06			126.0316	95802.31	6.436946	38.34862		3.862168
2088	121.0899	92045.85	6.18455	36.84495	55227.51	3.71073	2088	6.44E-09	4.9E-06	3.29E-10	1.96E-09	2.94E-06	1.97E-10	2088	121.0899	92045.85	6.18455	36.84495	55227.51	3.71073
2089		88436.68		35.40023		3.56523	2089	3.2E-09	2.43E-06	1.63E-10	9.73E-10	1.46E-06	9.8E-11	2089	116.3419	88436.68	5.94205	35.40023	53062.01	3.56523
2000	111.78	84969.03	5 700050		50981.42		2090	1.59E-09	1.21E-06	8.11E-11	4.83E-10	7.24E-07	4.87E-11	2090	111.78	84969.03				3.425435
																			48982.41	
					48982.41		2091	7.89E-10		4.03E-11	2.4E-10	3.6E-07		2091	107.3971					
2092	103.186	78436.3	5.270126	31.39719	47061.78	3.162075		3.92E-10		2E-11	1.19E-10	1.79E-07	1.2E-11	2092	103.186				47061.78	
2093	99,13999	75360.77	5.063481	30,16609	45216.46	3.038089	2093	1.95E-10	1.48E-07	9.93E-12	5.92E-11	8.87E-08	5.96E-12	2093	99.13999	75360.77	5.063481	30,16609	45216.46	3.038089
2094	95.25265	72405.83	4.864939	28,98326	43443.5	2.918963	2094	9.66E-11	7.34E-08	4.93E-12	2.94E-11	4.41E-08	2.96E-12	2094	95,25265	72405.83	4.864939	28.98326	43443.5	2.918963
	91.51774						2095			2.45E-12					91.51774				41740.06	2.804509
												1.09E-08			87.92928		4,490905		40103,4	
	87.92928				40103.4															
	84.48153						2097	1.18E-11		6.04E-13	3.6E-12	5.39E-09		2097	84.48153				38530.93	
2098	81.16896	61700.18	4.145628	24.69791	37020.11	2.487377	2098	5.87E-12	4.46E-09	3E-13	1.79E-12	2.68E-09	1.8E-13		81.16896				37020.11	
2099	77.98628	59280.88	3.983075	23.72949	35568.53	2.389845	2099	2.92E-12	2.22E-09	1.49E-13	8.87E-13	1.33E-09	8.94E-14	2099	77.98628	59280.88	3.983075	23.72949	35568.53	2.389845
2100					34173.87			1.45E-12	1.1E-09			6.61E-10	4.44E-14	2100	74.92839	56956.44	3.826897	22,79904	34173.87	2.296138
					32833.89					3.67E-14		3.28E-10		2101	71.99041				32833.89	
					31546.46			3.57E-13		1.82E-14	1.09E-13	1.63E-10			69.16762				31546.46	
	66.45552	50515.83	3.394153	20.22093		2.036492			1.35E-10		5.4E-14				66.45552	50515.83				2.036492
2104	63.84976	48535.08	3.261066	19,42806	29121.05	1.95664	2104	8.81E-14	6.69E-11	4.5E-15	2.68E-14	4.02E-11	2.7E-15	2104	63.84976	48535.08	3.261066	19.42806	29121.05	1.95664
	61,34618			18.66628	27979.2	1 879919	2105	4.37E-14	3.32E-11	2.23E-15	1.33E-14	1.99E-11	1.34E-15	2105	61.34618	46631.99	3.133198	18.66628	27979.2	1.879919
	58,94076					1.806206	2106			1.11E-15		9.91E-12			58,94076				26882.12	
															56,62966				25828.05	
	56.62966					1.735384	2107	1.08E-14				4.92E-12								
2108	54,40918	41358.87	2.778897	16.5555	24815.32	1.667338	2108					2.44E-12			54.40918	41358.87			24815.32	
2109	52.27576	39737.16	2.669935	15.90635	23842.3	1.601961	2109	2.66E-15				1.21E-12		2109	52.27576	39737.16		15,90635	23842,3	
2110				15.28265	22907.43	1.539147	2110	1.32E-15	1E-12	6.75E-17	4.02E-16	6.02E-13	4.05E-17	2110	50.226	38179.05	2,565245	15,28265	22907.43	1.539147
					22009.21				4.99E-13		2E-16	2.99E-13	2 01E-17	2111	48.25661	36682.02	2 464661	14.68341	22009.21	1.478796
		35243.7	2.404001	14.00341	21146.22	1.420812	2112					1.49E-13			46.36444	35243.7	2.36802			1.420812
	46.36444																			
		33861.78			20317.07		2113			8.26E-18		7.38E-14			44.54647	33861.78				1.365101
2114	42.79978	32534.04	2.185958	13.02302	19520.42	1.311575	2114		6.11E-14		2.44E-17	3.66E-14			42.79978	32534.04				
2115	41.12157	31258.36	2.100245	12.51238	18755.02	1.260147	2115	3.99E-17	3.03E-14	2.04E-18	1.21E-17	1.82E-14	1.22E-18	2115	41.12157	31258.36	2.100245	12.51238	18755.02	1.260147
2116				12.02176			2116			1.01E-18	6.03E-18	9.03E-15	6.07E-19	2116	39.50917	30032.7	2.017894	12.02176	18019.62	1.210736
2117	37.96			11.55038					7.48E-15		2.99E-18			2117	37.96		1.938771			1.163262
									3.71E-15		1.49E-18	2.23E-15			36,47156	27723.68	1.862751	11.09748		1.11765
		27723.68		11.09748		1.11765														
2119	35.04149	26636.62	1.789711	10.66235		1.073827	2119	2.43E-18			7.38E-19	1.11E-15		2119	35.04149	26636.62				1.073827
2120	33,6675	25592.18	1.719535	10.24427	15355.31	1.031721	2120	1.2E-18	9.15E-16	6.15E-20	3.66E-19	5.49E-16	3.69E-20	2120	33.6675	25592.18				1.031721
2121	32.34738	24588.7	1.652112	9.842586	14753.22	0.991267	2121	5.98E-19	4.55E-16	3.05E-20	1.82E-19	2.73E-16	1.83E-20	2121	32.34738	24588.7	1.652112	9.842586	14753.22	0.991267
					14174.74				2.26E-16		9.04E-20	1.35E-16		2122	31.07902	23624.56	1.587331	9,456652	14174.74	0.952399
	29.86039								1.12E-16		4.49E-20		4.52E-21		29,86039				13618.94	
															28.68955	21808.22			13084.93	
	28.68955			8,72959					5.57E-17		2.23E-20		2.24E-21							
2125	27.56461	20953.1	1.407837	8.387298	12571.86	0.844702			2.76E-17		1.11E-20		1.11E-21		27,56461		1.407837	8.387298		
2126	26.48379	20131.52	1.352635	8,058427	12078.91	0.811581	2126	1.81E-20	1.37E-17	9.22E-22	5.5E-21	8.24E-18	5.53E-22	2126	26.48379	20131.52	1.352635	8.058427	12078.91	0.811581
				7.742452			2127	8.97E-21	6.82E-18	4.58E-22	2.73E-21	4.09E-18	2.75E-22	2127	25.44535	19342.15	1.299597	7,742452	11605.29	0.779758
		18583.74	1.248639	7,438866				4.45E-21	3.39E-18		1.36E-21	2.03E-18		2128	24.44762		1.248639		11150.24	
									1.68E-18		6.73E-22	1.01E-18		2129	23,48902	17855.06	1.199679		10713.03	
		17855.06										5.01E-19		2120	22.568					
2130		17154.95		6.866939			2130	1.1E-21	8.35E-19		3.34E-22									
2131	21.68309	16482.3	1.107443	6.597682				5.45E-22	4.15E-19		1.66E-22				21,68309					
2132	20.83289	15836.02	1.06402	6.338984	9501.61	0.638412		2.71E-22	2.06E-19		8.24E-23	1.24E-19			20.83289	15836.02		6.338984		0.638412
2133	20.01602	15215.08	1.022299	6.090428	9129.046	0.61338	2133	1.34E-22	1.02E-19	6.87E-24	4.09E-23	6.13E-20	4.12E-24	2133	20.01602	15215.08	1.022299	6.090428	9129.046	0.61338
					8771.091		2134	6.68E-23	5.08E-20		2.03E-23	3.05E-20	2.05E-24	2134	19.23118	14618.49	0.982214	5.851619	8771.091	0.589329
	18.47711	14045.29					2135	3.32E-23	2.52E-20		1.01E-23	1.51E-20		2135	18.47711				8427.172	
														2136	17.75262				8096.738	
2136		13494.56	0.906698		8096.738		2136	1.65E-23	1.25E-20		5.01E-24	7.51E-21								
2137				5.189921		0.522688			6.22E-21		2.49E-24		2.51E-25		17.05653		0.871146			
2138	16.38773				7474.231		2138		3.09E-21		1.24E-24	1.85E-21			16.38773				7474.231	
2139	15,74516	11968.6	0.804169	4,790901	7181.162	0.482501	2139	2.02E-24	1.53E-21	1.03E-25	6.14E-25	9.2E-22	6.18E-26	2139	15.74516				7181.162	
2140					6899.585		2140		7.61E-22		3.05E-25		3.07E-26	2140	15.12778	11499,31	0.772637	4.603047	6899,585	0.463582
	14.53461							4.97E-25	3.78E-22		1.51E-25	2.27E-22		2141	14.53461					
									1.88E-22		7.51E-26	1.13E-22		2142	13.9647				6369.119	
2142					6369.119		2142	2.47E-25												
2143	13.41714	10198.97	0.685268	4.082536	6119.383	0.411161	2143	1.23E-25	9.32E-23		3.73E-26	5.59E-23			13.41714					
							2144	6.09E-26	4.63E-23		1.85E-26	2.78E-23			6.09E-26		3.11E-27		2.78E-23	1.87E-27
							2145	3.02E-26	2.3E-23	1.54E-27	9.2E-27	1.38E-23	9.27E-28	2145	3.02E-26	2.3E-23	1.54E-27	9.2E-27	1.38E-23	9.27E-28
							2146	1.5E-26	1.14E-23	7.67E-28	4.57E-27	6.85E-24	4.6E-28	2146	1.5E-26	1.14E-23	7.67E-28	4.57E-27	6.85E-24	4.6E-28
							2147	7.46E-27		3.81E-28	2.27E-27	3.4E-24		2147	7.46E-27	5.67E-24	3.81E-28	2.27E-27	3.4E-24	2.29E-28
							2148	3.7E-27	2.82E-24		1.13E-27	1.69E-24		2148	3.7E-27	2.82E-24	1.89E-28	1.13E-27	1.69E-24	1.13E-28
									2.022-24	1.092-20				2140					1.002-24	
									4 45 64	0 305 55							0 205 30	E 6E 30	9 205 35	5 645 20
							2149	1.84E-27	1.4E-24		5.6E-28	8.39E-25			1.84E-27	1.4E-24	9.39E-29	5.6E-28		
							2149 2150	1.84E-27 9.13E-28	6.94E-25	4.66E-29	2.78E-28	4.17E-25	2.8E-29	2150	9.13E-28	6.94E-25	4.66E-29	2.78E-28	4.17E-25	2.8E-29
							2149	1.84E-27 9.13E-28 4.53E-28	6.94E-25 3.45E-25	4.66E-29 2.32E-29	2.78E-28 1.38E-28	4.17E-25 2.07E-25	2.8E-29 1.39E-29	2150 2151	9.13E-28 4.53E-28	6.94E-25 3.45E-25	4.66E-29 2.32E-29	2.78E-28 1.38E-28	4.17E-25 2.07E-25	2.8E-29 1.39E-29
							2149 2150	1.84E-27 9.13E-28 4.53E-28	6.94E-25	4.66E-29 2.32E-29	2.78E-28	4.17E-25	2.8E-29 1.39E-29	2150	9.13E-28	6.94E-25	4.66E-29	2.78E-28	4.17E-25 2.07E-25	2.8E-29 1.39E-29 6.9E-30
							2149 2150 2151	1.84E-27 9.13E-28 4.53E-28 2.25E-28	6.94E-25 3.45E-25 1.71E-25	4.66E-29 2.32E-29 1.15E-29	2.78E-28 1.38E-28 6.85E-29	4.17E-25 2.07E-25 1.03E-25	2.8E-29 1.39E-29 6.9E-30	2150 2151 2152	9.13E-28 4.53E-28 2.25E-28	6.94E-25 3.45E-25 1.71E-25	4.66E-29 2.32E-29 1.15E-29	2.78E-28 1.38E-28 6.85E-29	4.17E-25 2.07E-25	2.8E-29 1.39E-29 6.9E-30
							2149 2150 2151 2152 2153	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28	6.94E-25 3.45E-25 1.71E-25 8.5E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29	4.17E-25 2.07E-25 1.03E-25 5.1E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30	2150 2151 2152 2153	9.13E-28 4.53E-28 2.25E-28 1.12E-28	6.94E-25 3.45E-25 1.71E-25 8.5E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29	4.17E-25 2.07E-25 1.03E-25 5.1E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30
							2149 2150 2151 2152 2153 2153	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30	2150 2151 2152 2153 2153	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30
							2149 2150 2151 2152 2153 2154 2155	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31	2150 2151 2152 2153 2154 2155	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31
							2149 2150 2151 2152 2153 2154 2155 2156	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31	2150 2151 2152 2153 2154 2155 2156	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31
							2149 2150 2151 2152 2153 2154 2155	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31	2150 2151 2152 2153 2154 2155 2156 2157	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31
							2149 2150 2151 2152 2153 2154 2155 2156	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31	2150 2151 2152 2153 2154 2155 2156	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27 2.57E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31 1.72E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30 1.03E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27 1.54E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31 1.03E-31
							2149 2150 2151 2152 2153 2154 2155 2156 2157	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30 3.38E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31 1.72E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27 1.54E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31 1.03E-31	2150 2151 2152 2153 2154 2155 2156 2157	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31 1.72E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27 1.54E-27	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31 1.03E-31
							2149 2150 2151 2152 2153 2154 2155 2156 2157 2158	1.84E-27 9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30 3.38E-30 1.68E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27 2.57E-27 1.27E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31 1.72E-31	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30 1.03E-30 5.1E-31	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27 1.54E-27 7.65E-28	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31 1.03E-31	2150 2151 2152 2153 2154 2155 2156 2157 2158	9.13E-28 4.53E-28 2.25E-28 1.12E-28 5.55E-29 2.76E-29 1.37E-29 6.8E-30 3.38E-30 1.68E-30	6.94E-25 3.45E-25 1.71E-25 8.5E-26 4.22E-26 2.1E-26 1.04E-26 5.17E-27 2.57E-27	4.66E-29 2.32E-29 1.15E-29 5.71E-30 2.84E-30 1.41E-30 6.99E-31 3.47E-31 1.72E-31 8.56E-32	2.78E-28 1.38E-28 6.85E-29 3.4E-29 1.69E-29 8.39E-30 4.17E-30 2.07E-30 1.03E-30 5.1E-31	4.17E-25 2.07E-25 1.03E-25 5.1E-26 2.53E-26 1.26E-26 6.25E-27 3.1E-27 1.54E-27 7.65E-28	2.8E-29 1.39E-29 6.9E-30 3.43E-30 1.7E-30 8.45E-31 4.2E-31 2.08E-31 1.03E-31

# Appendix F

# Puerto Rico Dump Conceptual Design

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Project	CNM	Landfill Gas Ext	raction Feasibility S	Study	Project No.	63	33060	1
Subject	Marp	Solid Waste Lar		Sheet No.	1	of	2	
	LFG	Extraction Well S	spacing		Drawing No.			
Compute	ed by _	SS	11/12/18	Checked by		Date		

Reference:

NSPS Background Information Document (BID). Appendix E. 1991

LandGEM – Landfill Gas Emissions Model, Version 3.02 U.S. Environmental Protection Agency (EPA). Model Output- October 2018.

Draft Closure Plan. Marpi Solid Waste Facility. Saipan, CNMI. Prepared by Harding ESE. October 25, 2002.

## **OBJECTIVE**:

Determine the radius of influence for landfill gas (LFG) collection to establish the spacing between the LFG extraction wells. This will be calculated using the EPA method.

## **PROCEDURE**:

Well spacing is determined by finding the radius of influence using the EPA method and using this radius to determine the spacing.

**A. EPA Method** – This analysis will be used to calculate the radius of influence of the landfill gas extraction wells.

$$R = 131.1 \left(\frac{Q_w DC}{L\rho Q_{gen} \eta}\right)^{1/2}$$

Where:

R = Radius of influence (feet [ft])

 $Q_w$  = Well flow (cubic feet per minute [ft³/min])

DC = Design capacity (tons)

L = Length of perforations (ft)

 $\rho$  = Waste density (pounds per cubic yard [lb/yd³])

 $Q_{gen} = LFG$  generation rate (ft³/min)

 $\eta$  = Extraction efficiency.

**B.** Spacing – Well spacing is found from the radius of influence:

spacing = 
$$R\sqrt{3}$$

Where:

R = Radius of Influence (ft) Spacing = spacing of wells (ft)

## Solution:

LandGEM model output was used to project LFG generation from Marpi Landfill and the peak LFG generation rate in 2049 was projected to be 182 cubic feet per minute (cfm). Due to heterogeneity of landfills not every well is going to be the same depth. To create an extraction well coverage of approximately 1 per acre, 25 extraction wells were assumed for the calculation. On average the landfill is 70 ft deep, therefore an average well would consist of 20 ft of solid pipe, 10 ft separation from the liner and 40 ft of perforated pipe. Minimally, it is assumed that 182 cfm



Project	CNMI	_andfill Gas Ext	raction Feasibility S	Study	Project No.	6	33060	)1
Subject	Marpi S	Solid Waste Lar	ndfill Facility		Sheet No.	2	of	2
	LFG E	xtraction Well S	pacing		Drawing No.			
Compute	ed by	SS	11/12/18	_Checked by		Date		

total for  $Q_w$  is divided among the 25 extraction wells, therefore the  $Q_w$  is 7.3 cfm per well. DC is 1.25E06 tons (Harding, October 2002),  $\rho$  is 1000 lb/yd³, Q_{gen} is 182 cfm and  $\eta$  is 75%. Completing this calculation yields:

$$R = 131.1 \left(\frac{7.3 * 1.25E06}{40 * 1000 * 182 * 0.75}\right)^{1/2}$$
$$R = 153 ft$$
$$spacing = 153 * \sqrt{3}$$
$$spacing = 265 ft$$

Using the standard that 1 cfm of gas captured per foot of perforated pipe, the maximal spacing was determined. As before, DC is 1.25E06 tons,  $\rho$  is 1000 lb/yd³, Q_{gen} is 182 cfm and  $\eta$  is 75%. Solving this calculation shows that the maximal spacing necessary is:

$$R = 131.1 \left(\frac{40 * 1.25E06}{40 * 1000 * 182 * 0.75}\right)^{1/2}$$
$$R = 397 ft$$
$$spacing = 397 * \sqrt{3}$$
$$spacing = 687 ft$$

### **CONCLUSION**:

Based on EA's recent project experience and professional judgment, the maximal calculation overestimates the LFG extraction well spacing. Therefore, being conservative, the wells are spaced at 260 ft with a radius of influence of 150 ft to balance the landfill gas extraction capacity with the cost of the system. Additionally, the spacing of 260 ft meets the design standard of 1 LFG extraction well per acre of landfill area. A total of 24 wells will be needed as per the estimated spacing of 260 ft requirement. The radius of influence for the future wells are presented on Figure 1.

Attachment 1: LandGEM Model Output Figure 1: Active LFG Collection System at MSWF

#### Attachment 1

				Biodegrad	lable waste		
Year		(14-1	Total landfill gas		/h.a. /	Methane	( (100/ ))
	2003	(Mg/year) 0	(m3/year) (a	av ft^3/min) 0	(Mg/year) 0	(m3/year)	(av ft^3/min)
	2003	199.46	151621.21	10.19	60.69	0 90972.72	0 6.11
	2004	386.87	294076.69	10.19	117.72	176446.01	11.86
	2006	549.91	418013.00	28.09	167.33	250807.80	16.85
	2007	689.52	524135.80	35.22	209.81	314481.48	
	2008	821.97	624818.85	41.98	250.11	374891.31	25.19
	2009	926.28	704104.02	47.31	281.85	422462.41	28.39
	2010	1008.11	766311.15	51.49	306.75	459786.69	
	2011	1089.95	828523.54	55.67	331.65	497114.12	33.40
	2012	1170.18	889507.42	59.77	356.06	533704.45	35.86
	2013	1210.32	920019.03	61.82	368.27	552011.42	37.09
	2014	1287.71	978849.97	65.77	391.82	587309.98	39.46
	2015	1365.00	1037597.34	69.72	415.34	622558.40	41.83
	2016	1441.87	1096032.37	73.64	438.73	657619.42	44.19
	2017	1557.47	1183902.62	79.55	473.90	710341.57	47.73
	2018	1672.94	1271680.27	85.44	509.04	763008.16	51.27
	2019	1756.68	1335333.62	89.72	534.52	801200.17	53.83
	2020	1838.18	1397285.70	93.88	559.32	838371.42	56.33
	2021	1917.54	1457608.78	97.94	583.46	874565.27	58.76
	2022	1994.85	1516372.34	101.88	606.99	909823.40	61.13
	2023	2070.19	1573643.17	105.73	629.91	944185.90	63.44
	2024	2143.65	1629485.48	109.48	652.27	977691.29	65.69
	2025	2215.32	1683961.00	113.15	674.07	1010376.60	67.89
	2026	2285.26	1737129.08	116.72	695.35	1042277.45	70.03
	2027	2353.56	1789046.80	120.21	716.14	1073428.08	72.12
	2028	2420.29	1839769.01	123.61	736.44	1103861.41	74.17
	2029	2485.51	1889348.48	126.95	756.29	1133609.09	76.17
	2030	2549.30	1937835.93	130.20	775.69	1162701.56	78.12
	2031	2611.71	1985280.16	133.39	794.69	1191168.09	80.03
	2032	2672.82	2031728.06	136.51	813.28	1219036.84	81.91
	2033	2732.67	2077224.76	139.57	831.49	1246334.85	83.74
	2034	2791.33	2121813.64	142.56	849.34	1273088.18	85.54
	2035	2848.85	2165536.43	145.50	866.84	1299321.86	87.30
	2036	2905.28	2208433.27	148.38	884.01	1325059.96	89.03
	2037	2960.68	2250542.76	151.21	900.87	1350325.65	90.73
	2038	3015.09	2291902.03	153.99	917.42	1375141.22	92.40
	2039	3068.55	2332546.82	156.72	933.69	1399528.09	94.03
	2040	3121.13	2372511.49	159.41	949.69	1423506.89	95.65
	2041	3172.85	2411829.09	162.05	965.43	1447097.45	97.23
	2042	3223.77	2450531.44	164.65	980.92	1470318.86	98.79
	2043	3273.91	2488649.15	167.21	996.18	1493189.49	100.33
	2044	3323.33	2526211.68	169.74	1011.21	1515727.01	101.84
	2045	3372.05	2563247.36	172.22	1026.04	1537948.42	103.33
	2046	3420.12	2599783.49	174.68	1040.66	1559870.09	104.81
	2047		2635846.31	177.10	1055.10	1581507.79	106.26
ACTERIOUS	2048	3514.41	2671461.10	179.50	1069.36	1602876.66	107.70
和關係	2049	3560.70	2706652.19	181.86	1083.44	1623991.31	109.12
	2050 2051	3421.09	2600522.84 2498554.88	174.73	1040.96	1560313.70	104.84
	2031	3286.94	2490004.00	167.88	1000.14	1499132.93	100.73

### Attachment 1

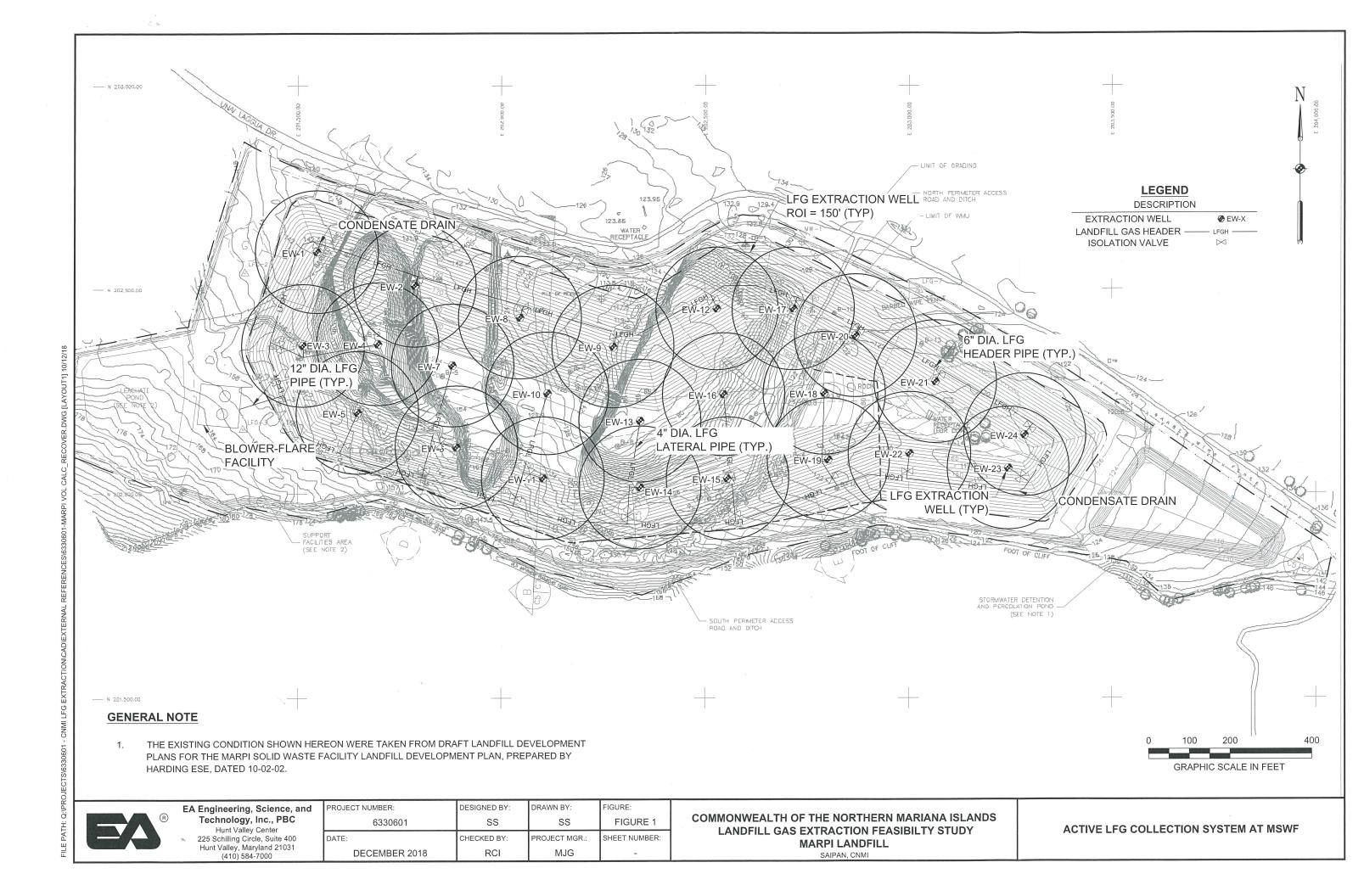
			-	able waste		
Year		Total landfill gas			Methane	
	(Mg/year)	(m3/year)	(av ft^3/min)	(Mg/year)	(m3/year)	(av ft^3/min)
20	52 3158.06	2400585.14	161.30	960.93	1440351.08	96.78
20	53 3034.23	2306456.85	154.97	923.25	1383874.11	92.98
20	54 2915.26	2216019.38	148.89	887.05	1329611.63	89.34
20	55 2800.95	2129128.02	143.06	852.27	1277476.81	85.83
20	56 2691.12	2045643.72	137.45	818.85	1227386.23	82.47
20	57 2585.60	1965432.88	132.06	786.74	1179259.73	79.23
20	58 2484.22	1888367.15	126.88	755.89	1133020.29	76.13
20	59 2386.81	1814323.22	121.90	726.25	1088593.93	73.14
20	60 2293.22	1743182.59	117.12	697.78	1045909.55	70.27
20	61 2203.31	1674831.42	112.53	670.42	1004898.85	67.52
20	62 2116.91	1609160.34	108.12	644.13	965496.21	64.87
20	63 2033.91	1546064.26	103.88	618.87	927638.56	62.33
	64 1954.16	1485442.22	99.81	594.61	891265.33	59.88
	65 1877.53		95.89	571.29	856318.32	57.54
	66 1803.91	1371235.99	92.13	548.89	822741.59	55.28
	67 1733.18	1317469.06	88.52	527.37	790481.44	53.11
	68 1665.22		85.05	506.69	759486.21	51.03
	69 1599.93		81.71	486.82	729706.33	49.03
	1537.19		78.51	467.73	701094.14	47.11
	1476.92		75.43	449.39	673603.85	45.26
	1419.01		72.47	431.77	647191.46	43.48
	1363.37		69.63	414.84	621814.72	41.78
	1309.91		66.90	398.58	597433.02	40.14
	1258.55		64.28	382.95	574007.33	38.57
	1209.20		61.76	367.93		
	1161.79			353.51	529875.55	35.60
	1116.23			339.64	509098.83	34.21
	1072.46			326.33		
	1030.41			313.53		
	990.01			301.24		
	951.19			289.43		29.15
	913.89			278.08		
	878.06		44.85	267.17		
	843.63		43.09	256.70		25.85
	86 810.55			246.63	369681.63	24.84
	087 778.77		39.77			
	088 748.23					
	718.89					22.03
	690.71					
	091 663.62					20.34
	637.60				290801.87	19.54
	093 612.60		31.29			
	)94 588.58					
	)95 565.50					
	)96 543.33					
	097 522.02					
	098 501.56					
	099 481.89					
	100 462.99					
2	402.93	, 001042.40	20.00	140.00	2.11.00.00	

### Biodegradable waste

#### Attachment 1

Ň					lable waste		
Year		(Makinga)	Total landfill gas		/	Methane	
a half of the second seco	2101	(Mg/year)	(m3/year)	(av ft^3/min)		(m3/year)	(av ft^3/min)
	2101	444.84	338142.63	22.72	135.35	202885.58	13.63
	2102		324883.87	21.83		194930.32	13.10
	2103		312144.99	20.97		187286.99	12.58
	2104		299905.61	20.15		179943.37	12.09
	2105		288146.14	19.36		172887.69	11.62
	2106		276847.77	18.60		166108.66	11.16
	2107		265992.42	17.87		159595.45	10.72
	2108		255562.70	17.17	102.30	153337.62	10.30
	2109		245541.95	16.50	98.29	147325.17	9.90
	2110		235914.11	15.85		141548.47	9.51
	2111	298.18	226663.78	15.23		135998.27	9.14
	2112		217776.17	14.63		130665.70	8.78
	2113		209237.04	14.06	83.76	125542.23	8.44
	2114		201032.74	13.51	80.47	120619.65	8.10
	2115		193150.14	12.98	77.32	115890.08	7.79
	2116		185576.61	12.47	74.28	111345.97	7.48
	2117		178300.05	11.98	71.37	106980.03	7.19
	2118		171308.80	11.51	68.57	102785.28	6.91
	2119		164591.69	11.06	65.88	98755.01	6.64
	2120	208.04	158137.96	10.63	63.30	94882.77	6.38
	2121	199.88	151937.28	10.21	60.82	91162.37	6.13
	2122	192.04	145979.73	9.81	58.43	87587.84	5.89
	2123	184.51	140255.79	9.42	56.14	84153.47	5.65
	2124	177.28	134756.28	9.05	53.94	80853.77	5.43
	2125	170.33	129472.41	8.70	51.83	77683.44	5.22
	2126	163.65	124395.72	8.36	49.79	74637.43	5.01
	2127	157.23	119518.10	8.03	47.84	71710.86	4.82
	2128	151.07	114831.72	7.72	45.97	68899.03	4.63
	2129	145.14	110329.11	7.41	44.16	66197.47	4.45
	2130	139.45	106003.04	7.12	42.43	63601.83	4.27
	2131	133.98	101846.60	6.84	40.77	61107.96	4.11
	2132	128.73	97853.14	6.57	39.17	58711.88	3.94
	2133	123.68	94016.26	6.32	37.63	56409.76	3.79
	2134	118.83	90329.83	6.07	36.16	54197.90	3.64
	2135	114.17	86787.95	5.83	34.74	52072.77	3.50
	2136	109.70	83384.95	5.60	33.38	50030.97	3.36
	2137	105.39	80115.38	5.38	32.07	48069.23	3.23
	2138	101.26	76974.01	5.17	30.81	46184.40	3.10
	2139		73955.81	4.97	29.60	44373.49	2.98
	2140	93.48	71055.96	4.77	28.44	42633.58	2.86
	2141	89.81	68269.82	4.59	27.33	40961.89	2.75
	2142		65592.92	4.41	26.26	39355.75	2.64
	2143	82.91	63020.99	4.23	25.23	37812.59	2.54
						1990 A. (1990) A	an manage an

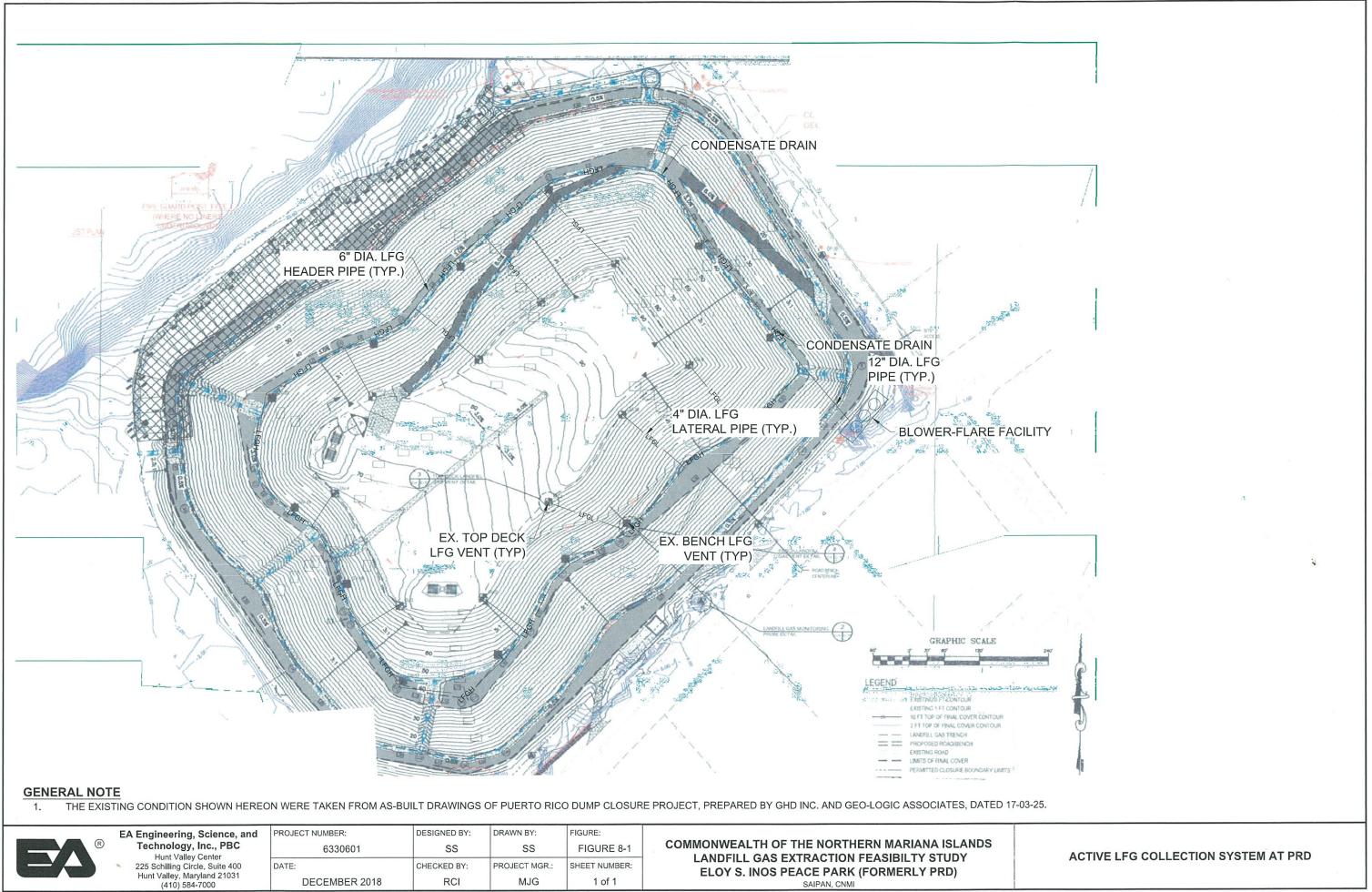




Appendix G

Marpi Solid Waste Facility Conceptual Design

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, and	PROJECT NUMBER:	DESIGNED BY:	DRAWN BY:	FIGURE:	
С	6330601	SS	SS	FIGURE 8-1	COMMON
00	DATE:	CHECKED BY:	PROJECT MGR.:	SHEET NUMBER:	LANE
31	DECEMBER 2018	RCI	MJG	1 of 1	

SAIPAN, CNMI

**Appendix H** 

# **EPA LFG Energy Cost Model**

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C&F: Collection a	nd Flaring System
Typical components include	• Engineering, permitting, and administration;
	<ul> <li>Wells and wellheads;</li> </ul>
	<ul> <li>Pipe gathering system (includes additional fittings/installations);</li> </ul>
	<ul> <li>Condensate knockout system;</li> </ul>
	<ul> <li>Blowers;</li> </ul>
	<ul> <li>Instrument controls;</li> </ul>
	▶ Flare; and
	<ul> <li>Site survey, preparation, and utilities.</li> </ul>
Drilling and pipe crew mobilization	\$20,000
Installed capital cost of vertical gas extraction	$\left(\begin{array}{c} \text{average waste} \\ \text{depth (ft)} \end{array}\right) * \$85/\text{ft} = \$X/\text{well},$
wells	(\$4,675 * number of wells) for default average waste depth of 65 feet
Installed capital cost of wellheads and pipe gathering system	\$17,000 * number of wells
Installed capital cost of knockout, blower, and flare system	(ft ³ /min) ^{0.61} * \$4,600
Engineering, permitting, and surveying	\$700 * number of wells
Annual O&M cost (excluding energy costs)*	(\$2,600 * number of wells) + \$5,100 for flare
Electricity usage by blowers	0.002 kWh / ft ³

Note: Raw cost data are in 2013\$'s.

* Annual O&M for wells include the cost for monthly wellhead monitoring for gas quality and wellhead adjustment purposes as well as the cost to maintain each well.

SENG: Small Reciprocat	ing Engine-Generator Set
Typical components include	<ul> <li>Gas compression and treatment (includes dehydration equipment and filtration);</li> </ul>
	<ul> <li>Reciprocating engine and generator (includes motor controls, switch-gear, radiators, exhaust silencers, and all wiring and plumbing;</li> </ul>
	<ul> <li>Electrical interconnect equipment; and</li> </ul>
	<ul> <li>Site work, housings, utilities, and total facility engineering, design, and permitting.</li> </ul>
	(Includes all equipment downstream of collection and flaring system.)
Installed capital cost	\$2,300 * kW capacity
	\$0.024 * kWh generated/yr
Annual O&M cost (excluding energy)	(before parasitic uses)
Parasitic loss efficiency	92% of capacity due to parasitic electrical needs of compression and treatment
Fuel use rate	36 ft ³ /kWh generated (before parasitic uses)
Gross capacity factor [*]	Assume 93%

Note: Raw cost data are in 2008\$'s.

*

Gross capacity factor accounts for loss of energy production due to problems in the gas collection system, problems with project equipment, weather related interruptions of the local utilities, and shut-downs at the energy consumer end of the system.

MTUR: Mici	roturbine-Generator Set
Typical components include	<ul> <li>Gas compression and treatment (includes dehydration equipment, siloxane adsorbers, and filtration);</li> </ul>
	<ul> <li>Microturbine and generator (includes exhaust silencers and all wiring and plumbing);</li> </ul>
	<ul> <li>Electrical interconnect equipment; and</li> </ul>
	<ul> <li>Site work, housings, utilities, and total facility engineering, design, and permitting.</li> </ul>
	(Includes all equipment downstream of collection and flaring system.)
Installed capital cost	\$19,278 * (kW capacity) ^{0.6207}
Annual O&M cost (excluding energy)	(\$0.0736 - (0.0094 * ln(kW capacity))) * kWh generated/yr
Annual O&W cost (excluding energy)	(before parasitic uses), includes gas cleanup system O&M and microturbine overhauls
Parasitic loss efficiency	83% of rated capacity due to parasitic electrical needs of boost compressor and cooling water pumps, fans, and dryer system
Fuel use rate	14,000 Btu/kWh generated (HHV)
Fuel use rate	(before parasitic uses)
Gross capacity factor*	Assume 93%

Note: Raw cost data are in 2006\$'s.

Gross capacity factor accounts for loss of energy production due to problems in the gas collection system, problems with project equipment, weather related interruptions of the local utilities, and shut-downs at the energy consumer end of the system.

LCH: Leach	nate Evaporator
Typical components include	<ul> <li>Leachate evaporation unit;</li> </ul>
	<ul> <li>Leachate surge tank;</li> </ul>
	<ul> <li>Process control instruments; and</li> </ul>
	<ul> <li>Site work, housings, utilities, and total facility engineering, design, and permitting.</li> </ul>
Annualized capital and O&M costs [*]	$320,000 * \left(\frac{\text{gallons evaporated/yr}}{3,467,500}\right)^{0.19}$
Fuel use rate	80 Btu/gallon evaporated
Electricity usage	0.055 kWh/gallon evaporated
Leachate evaporation limit	No more than 95% of the available leachate can be evaporated

Note: Raw cost data are in 2008\$'s.

* Competitive rental costs were found for leachate evaporation, and were used to develop a combined capital and operating cost.

## **Appendix I**

## **Cost-Benefit Analysis for Landfill Gas Beneficial Reuse Alternatives**

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MSWF - Uption 2 (Electricity Generation using Microturbine)

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Year Year of operation	2055 31	2056 32	2057 33	2058 34	2059 35	2060 36	2061 37	2062 38	2063 39	2064 40	2065 41	2066 42	2067 43	2068 44	2
Annual Return ^(a) \$ 153,100 \$ 153,100 \$ 153,100 \$ 153,100	\$ 153,100 \$	153,100 S	153,100 \$	153,100 S	153,100 \$	153,100 S	153,100 S	153,100 S	153,100 S	153,100 S	153,100 S	153,100 \$	153,100 \$	153,100 S	
Installed Capital Cost LFG Collection System (s) $^{\rm (b)}$ Installed Capital Cost Microturbine Energy System (s) $^{\rm (b)}$															
Annual O&M Cost LFG collection System (\$) \$ Annual O&M Cost Energy System(\$) \$	\$ 62,400 \$ \$ 45,300 \$	62,400 \$ 45,300 \$	62,400 \$ 45,300 \$	62,400 S 45,300 S	62,400 \$ 45,300 \$	62,400 S 45,300 S	62,400 \$ 45,300 \$	62,400 S 45,300 S	62,400 S 45,300 S	62,400 S 45,300 S	62,400 S 45,300 S	62,400 \$ 45,300 \$	62,400 \$ 45,300 \$	62,400 \$ 45,300 \$	
Annual Debt Service ^(c) \$ 215,400 \$	\$ 215,400 \$	215,400 \$	215,400 \$ 215,400 \$	215,400 \$	215,400 S	215,400 \$	215,400 \$	215,400 S	215,400 \$	215,400 \$	215,400 \$	215,400 \$	215,400 \$	215,400 \$	
Net income         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (170,000)         \$ (160,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)         \$ (162,100)	Net income \$ (170,000) \$ (170,000) \$ (170,000) \$ (170,000) Cash flow \$ (170,000) \$ (170,000) \$ (170,000) \$ (170,000) e cash flow \$ (3,453,700) \$ (3,623,700) \$ (3,93,700) \$ (3,963,700) (NPV, i=3%) \$ (68,000) \$ (66,100) \$ (64,100) \$ (62,300) esent value \$ (2,128,200) \$ (2,194,300) \$ (2,258,400) \$ (2,320,700) esent value \$ (2,128,200) \$ (2,194,300) \$ (2,258,400) \$ (2,320,700)	(170,000) S (170,000) S (3,623,700) S (66,100) S (2,194,300) S	(170,000) \$ (170,000) \$ (3,793,700) \$ ( (64,100) \$ (2,258,400) \$ (	(170,000) \$ (170,000) \$ (3,963,700) \$ (62,300) \$ (2,320,700) \$	(170,000) \$ (170,000) \$ (4,133,700) \$ (60,500) \$ (2,381,200) \$	(170,000) \$ (170,000) \$ (4,303,700) \$ (58,700) \$ (2,439,900) \$	(170,000) S (170,000) S (4,473,700) S (57,000) S (2,496,900) S	(170,000) \$ (170,000) \$ 4,643,700) \$ (55,300) \$ 2,552,200) \$	(170,000) S (170,000) S (4,813,700) S ( (53,700) S ( (2,605,900) S (	(170,000) \$ (170,000) \$ (4,983,700) \$ ( (52,200) \$ ( (2,658,100) \$ (	(170,000) \$ (170,000) \$ (5,153,700) \$ ( (50,600) \$ (2,708,700) \$ (	(170,000) \$ (170,000) \$ (5,323,700) \$ ( (49,200) \$ (2,757,900) \$ (	(170,000) S (170,000) S (5,493,700) S (47,700) S (2,805,600) S	(170,000) \$ (170,000) \$ (5,663,700) \$ (46,400) \$ (2,852,000) \$	(5 (2

generation (SKMh) I Return was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF energy production system. Future demand may vary. I costs for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. I Debt Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)

MSWF - Uption 2 (Electricity Generation using Microturbine)

ic Analysis

Year Year of operation	2040 16	2041	2042 18	2043 19	2044 20	2045 21	2046 22	2047 23	2048 24	2049 25	2050 26	2051 27	2052 28	2053 29	
Annual Return ^(a) S		153,100 \$ 153,100 \$ 153,100	153,100 \$	153,100 \$	153,100 S	153,100 S	153,100 \$	153,100 S	153,100 \$	153,100	\$ 153,100	153,100	\$ 153,100	\$ 153,100 \$	
Installed Capital Cost LFG Collection System $(\$)^{\rm (b)}$ Installed Capital Cost Microturbine Energy System $(\$)^{\rm (b)}$														S S	
Annual O&M Cost LFG Collection System (\$) 8 Annual O&M Cost Energy System(\$) 5	62,400 \$ 57,000 \$	62,400 \$ 57,000 \$	62,400 \$ 57,000 \$	62,400 \$ 57,000 \$	62,400 S 57,000 S	62,400 S 57,000 S	62,400 \$ 57,000 \$	62,400 \$ 57,000 \$	62,400 \$ 57,000 \$	62,400 57,000	s 62,400 s 57,000	62,400 57,000	5 62,400 57,000	5 62,400 \$	
Annual Debt Service ^(c) S		164,300 \$ 164,300 \$	164,300 \$	164.300 \$	164,300 S	164,300 \$	164,300 \$	164.300 \$	164,300 \$	164,300	\$ 164,300	\$ 164,300	5 164,300 \$	164,300 \$	
Net income 5 Cash flow 5 Cumulative cash flow 5 Present value of cash flow (NPV, i=3%) 5 Cumulative present value 5		(130,600)         \$ (130,600)         \$ (130,600)           (130,600)         \$ (130,600)         \$ (130,600)           (1467,000)         \$ (1597,600)         \$ (176,800)           (81,400)         \$ (1,291,000)         \$ (176,800)           (145,100)         \$ (1,224,200)         \$ (1,301,000)	(130,600)         \$         (130,600)         \$         (130,600)         \$           (130,600)         \$         (130,600)         \$         (130,600)         \$           (1467,000)         \$         (1324,600)         \$         (1,724,200)         \$         (1,6800)         \$           (81,400)         \$         (72,4200)         \$         (1,301,000)         \$         (1,301,000)         \$	(130,600) \$ (130,600) \$ (1,858,800) \$ (74,500) \$ (1,375,500) \$	(130,600) S (130,600) S (1,989,400) S (72,400) S (1,447,900) S (1,447,900) S	s (130,600) \$ 5 (130,600) \$ 5 (2,120,000) \$ 5 (70,200) \$ 5 (1,518,100) \$	(130,600) \$ (130,600) \$ (2,250,600) \$ (2,250,600) \$ (1,586,300) \$ (1,586,300) \$	(130,600) \$ (130,600) \$ (2,381,200) \$ (66,200) \$ (1,652,500) \$	(130,600) \$ (130,600) \$ (2,511,800) \$ (64,300) \$ (1,716,800) \$ (1,716,800) \$	(130,600) (130,600) (2,642,400) (62,400) (1,779,200)	\$ (130,600) \$ (130,600) \$ (2,773,000) \$ (60,600) \$ (1,839,800)	(130,600) (130,600) (2,903,600) (58,800) (1,898,600)	<pre>(130,600) (130,600) (3,034,200) (5,7100) (1,955,700) </pre>	(130,600) \$ (130,600) \$ (3,164,800) \$ (55,500) \$ (2,011,200) \$	<i>1</i> 3

r generation (\$KWh) al Return was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF energy production system. Future demand may vary, al costs for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. I Debt Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)

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ysis Expected LFG energy project lifetime (yrs) Year Year of operation	Ann	$\label{eq:constraint} \begin{array}{llllllllllllllllllllllllllllllllllll$	Annual O&M Cost LFG Collection System (\$) Annual O&M Cost Energy System(\$)	Annual De		Cumulative	Present Value of Cash Flow (NPV, i=3%)	Cumulative Present value Net Present Value (NPV, j=3%)
oject lifetime (yrs) Year Year of operation	Annual Return ^(a)	system (\$) ^(b) \$ system (\$) ^(b) \$	l System (\$) y System(\$)	Annual Debt Service ^(c)	Net Income Cash Flow	Cumulative Cash Flow	(NPV, i=3%)	esent value (NPV, i=3%)
45 2024 0		1,079,000 903,000						
2025 1	\$		69 KN	\$ 1.	s s	s	s S	S (2,85
25	53,100 S		62,400 S 51,100 S	28,300 S	(88,700) \$ (88,700) \$	(88,700) S	(86,200) S	\$ (86,200) \$ \$ (2,897,000)
2026 2	153,100 \$ 153,100 \$ 153,		62,400 \$ 51,100 \$	128,300 \$ 128,300 \$	(88,700) \$ (88,700) \$	(177,400) \$	(83,700) S	(169,900) \$
2027 3	153,100 \$		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88,700) \$			
2028 4	153,100 \$		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88,700) \$	(354,800) \$	(78,900) \$	(330,000) \$
2029 5	153,100 S		62,400 S 51,100 S	128,300 \$	(88,700) \$ (88,700) \$	(443,500) \$	(76,600) \$	(406,600) S
2030 6	153,100 S		62,400 S 51,100 S	128,300 \$	(88,700) \$ (88.700) \$	(532,200) \$	(74,300) \$	(480,900) \$
2031 7	153,100 S		62,400 S 51,100 S	128,300 \$	(88,700) \$ (88.700) \$	(620,900) \$	(72,200) \$	(553,100) S
2032 8	153,100 S		62,400 S 51,100 S	128,300 \$	(88,700) \$ (88,700) \$	\$ (009,602)	(70,100) \$	(623,200) \$
2033 9	153,100 S		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88.700) \$	(798,300) \$	(68,000) S	(691,200) S
2034 10	153,100 S		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88,700) \$	(887,000) \$	(66,100) \$	(757,300) \$
2035 11	153,100 \$		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88,700) \$	(975,700) \$ ('		(821,400) \$
2036 12	153,100 S		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$ (88,700) \$	-		(883,700) \$
2037 13	153,100 \$		62,400 \$ 51,100 \$	128,300 \$	(88,700) \$	(1.153.100) \$ (1.		(944,200) \$
2038 14	153,100		62,400 51,100	128,300	(88,700) (88,700)		(58,700)	(1,002,900)

ation (\$KVM) \$0.145 n was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF energy production system. Future demand may vary, for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)

ysis

MSWF - Uption 1 (Electricity Generation using Small Reciprocating Engine)

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Year Year of operation	2055 31	2056 32	2057 33	2058 34	2059 35		2060 36	2061 37	2062 38	2063 39	2064 40	2065 41	2066 42	2067 43	2068 44	
Annual Return ^(a) \$ 153,100 \$ 153,100 \$ 153,100 \$	\$ 153,100	\$ 153,100	\$ 153,100 \$	\$ 153,100	S 153.	153,100 S	153,100 S	153,100 \$	153,100 \$	\$ 153,100 \$	153,100 \$	153,100 \$	153,100 \$	153,100	153,100 \$	10
Installed Capital Cost LFG Collection System (\$)^{(b)} Installed Capital Cost Small Engine Energy System (\$)^{(b)}																
Annual O&M Cost LFG Collection System (\$) S Annual O&M Cost Energy System(\$) S	s 62,400 \$ 62,400	\$ 62,400 \$ \$ 62,400 \$	\$ 62,400 \$	5 62,400 5 62,400	s 62. S 62.	62,400 S 62,400 S	62,400 \$ 62,400 \$	62,400 \$ 62,400 \$	62,400 \$ 62,400 \$	62,400 \$ 62,400 \$	62,400 \$ 62,400 \$	62,400 \$ 62,400 \$	62,400 S 62,400 S	62,400 62,400	62,400 \$ 62,400 \$	10 10
Annual Debt Service ^(c) \$ 217,400 \$ 217,400 \$ 217,400 \$ 217,400	\$ 217,400	\$ 217,400	\$ 217,400	217,400	\$ 217.	217,400 \$	217,400 \$	217,400 \$	217,400 \$	217,400 \$	217,400 \$	217,400 \$	217,400 S	217,400	217,400 S	10
Net Income         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (189,100)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)         \$ (19,12,00)	\$ (189,100) \$ (189,100) \$ (4,483,400) \$ (75,700) \$ (2,774,000)	Net Income         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (189,100)         5         (199,100)         5         (199,100)         5         (199,100)         5         (199,100)         5         (199,100)         5         (199,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5         (191,100)         5 <t< th=""><th>\$ (189,100) \$ (189,100) \$ (4,861,600) \$ (71,300) \$ (2,918,800)</th><th>\$ (189,100) \$ (189,100) \$ (5,050,700) \$ (69,300) \$ (2,988,100)</th><th>s (5.2) () () () () () () () () () () () () ()</th><th>~~~</th><th>(189,100) \$ (189,100) \$ (5,428,900) \$ (65,300) \$ (3,120,700) \$</th><th>\$ (189,100) \$ \$ (189,100) \$ \$ (5,618,000) \$ \$ (5,400) \$ \$ (63,400) \$ \$ (3,184,100) \$</th><th>\$ (189,100) \$ \$ (189,100) \$ \$ (5,807,100) \$ \$ (61,500) \$ \$ (3,245,600) \$</th><th><pre>(189,100) \$ (189,100) \$ (189,100) \$ (5,996,200) \$ (59,800) \$ (3,305,400) \$ </pre></th><th>(189,100) \$ (189,100) \$ (6,185,300) \$ (58,000) \$ (3,363,400) \$</th><th>(189,100) \$ (189,100) \$ (6,374,400) \$ (56,300) \$ (3,419,700) \$</th><th>(189,100) \$ (189,100) \$ (6,563,500) \$ (54,700) \$ (3,474,400) \$</th><th>(189,100) 3 (189,100) 5 (6,752,600) 5 (53,100) 3 (3,527,500) 5</th><th>(189,100) \$ (189,100) \$ (189,100) \$ (6,941,700) \$ (51,600) \$ (3,579,100) \$</th><th>10 10 10 10 10</th></t<>	\$ (189,100) \$ (189,100) \$ (4,861,600) \$ (71,300) \$ (2,918,800)	\$ (189,100) \$ (189,100) \$ (5,050,700) \$ (69,300) \$ (2,988,100)	s (5.2) () () () () () () () () () () () () ()	~~~	(189,100) \$ (189,100) \$ (5,428,900) \$ (65,300) \$ (3,120,700) \$	\$ (189,100) \$ \$ (189,100) \$ \$ (5,618,000) \$ \$ (5,400) \$ \$ (63,400) \$ \$ (3,184,100) \$	\$ (189,100) \$ \$ (189,100) \$ \$ (5,807,100) \$ \$ (61,500) \$ \$ (3,245,600) \$	<pre>(189,100) \$ (189,100) \$ (189,100) \$ (5,996,200) \$ (59,800) \$ (3,305,400) \$ </pre>	(189,100) \$ (189,100) \$ (6,185,300) \$ (58,000) \$ (3,363,400) \$	(189,100) \$ (189,100) \$ (6,374,400) \$ (56,300) \$ (3,419,700) \$	(189,100) \$ (189,100) \$ (6,563,500) \$ (54,700) \$ (3,474,400) \$	(189,100) 3 (189,100) 5 (6,752,600) 5 (53,100) 3 (3,527,500) 5	(189,100) \$ (189,100) \$ (189,100) \$ (6,941,700) \$ (51,600) \$ (3,579,100) \$	10 10 10 10 10

teration (\$/kWh) start was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF energy production system. Future demand may vary. stor was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF is to both LFC collection systems and energy production systems include additional 40% cost factor for on-siland construction in Salpan. It Service was calculated based on a projected prime interest rate of 6% (http://mortgage.x.com/general/indexes/prime_rate_forecast.asp)

MSWP - Uption 1 (Electricity Generation using Small Reciprocating Engine)

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2053 29	153,100		62,400 95,900	165,800	(171,000) (171,000) (4,156,800) (72,600) (2,641,600)
	o s		s s o s	0	\$ \$ \$ \$ \$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2052 28	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,985,800) (74,800) (2,569,000)
	s O		s s O O	\$	****
2051 27	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,814,800) (77,000) (2,494,200)
	s		s s	\$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2050 26	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,643,800) (79,300) (2,417,200)
	0 2		s s o o	\$	\$ \$ \$ \$ () () () () () () () () () () () () () () () () () (
2049 25	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,472,800) (81,700) (2,337,900)
	S		s s	\$	\$ \$ \$ \$ \$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2048 24	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,301,800) (3,256,200) (2,256,200)
	s (		s s	S	\$ \$ \$ \$ \$ 0 0 0 0 0
2047 23	153,100		62,400 95,900	165,800	(171,000) (171,000) (3,130,800) (86,700) (2,172,000)
	0 \$		0 0	0 \$	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2046 22	153,100		62,400 95,900	165,800	(171,000) (171,000) (2,959,800) (89,300) (2,085,300)
	s 0		s s o o	\$	0000
2045 21	153,100		62,400 95,900	165,800	(171,000) (171,000) (2,788,800) (92,000) (1,996,000)
	s o		s s o s	\$ 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2044 20	153,100		62,400 95,900	165,800	\$ (171,000) \$ (171,000) \$ (2,617,800) \$ (94,700) \$ (1,904,000)
	s 0		8 S 0 O	0 \$	
2043 19	153,100		62,400 95,900	165,800	(171,00 (171,00 (2,446,80 (97,60 (1,809,30
	0 \$		s s o o	s 0	00000
2042 18	153,100 \$		62,400 95,900	165,800 \$	(171,00) (171,00) (2,275,80) (100,50) (1,711,70)
	ŝ		8 8 0 0	ŝ	\$ \$ \$ \$ \$ () () () () ()
2041 17	153,100 S 153,100 S		62,400 95,900	165,800 \$	(171,000 (171,000 (2,104,800 (103,500 (1,611,200
	S		s s	ŝ	S S S S S S S S S S S S S S S S S S S
2040 16			62,400 \$ 95,900 \$	165,800 \$	Net Income         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5         (171,000)         5 <t< td=""></t<>
L L	Annual Return ^(a) \$	(q	\$ (s	Annual Debt Service ^(c) \$	933(99) 9999999
Year Year of operation	turn	u (\$) ⁽	em (\$	vice	icom i Flov i=3% i=3% i=3% i=3%
obe	al Re	/sten /sten	Syste	t Ser	let In Cash VPV, VPV, VPV,
ar of	nnu	n S) Jy S)	tion :	Deb	Pre-
Ye	4	ectio	t En	nual	mula h Flo ative t Val
		Installed Capital Cost LFG Collection System ( $\mathbf{S}^{(b)}$ led Capital Cost Small Engine Energy System ( $\mathbf{S}^{(b)}$	Annual O&M Cost LFG Collection System (\$) \$ Annual O&M Cost Energy System(\$) \$	An.	Net Income Cash Flow Cumulative Cash Flow Cumulative Present Value Cumulative Present Value Net Present Value (NPV, i=3%)
		LFG Eng	st LF J&M		ue of CL CL
		Cost mall	A Co: ual C		t Val
		oital ( ost S	0&N Ann		sent
		I Cap	nual		Pre
		Capit	An		
		Inst Iled (			
		Installed Capital Cost LFG Collection System ( $\$)^{(b)}$ Installed Capital Cost Small Engine Energy System ( $\$)^{(b)}$			
		0.000			

y generation (S/k/M) ial Return was calculated assuming consumption of 10 hours of continuous electricity per day from 290 kW capacity MSWF energy production system. Future demand may vary, tal costs for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. al Debt Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)

MSWF - Uption 1 (Electricity Generation using Small Reciprocating Engine)

ysis Expected LFG Energy Project Lifetime (yrs) Year Year of operation	45 2024 0	2025 1	2026 2		2027 3	2028 4	2029 5	2030 6	2031 7	2032 8	2033 9	2034 10	2035 11	2036 12	2037 13	2038 14
Annuai Return ^(a)		\$ 153,100	0 S 15	153,100 \$ 153,100 \$	153,100 S	153,100 \$	153,100 S	153,100 S	153,100 \$	153,100 S	153,100 \$	153,100 \$	153,100 S	153,100 \$	153,100 \$	153,100
Installed Capital Cost LFG Collection System (\$) ^(b) \$ 1,079,000 Installed Capital Cost Small Engine Energy System (\$) ^(b) \$ 921,000	1,079,000 921,000															
Annual O&M Cost LFG Collection System (\$) Annual O&M Cost Energy System(\$)		62,400 77,600	ŝ	62,400 S 77,600 S	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,400 \$ 77,600 \$	62,40C 77,60C
Annual Debt Service ^(c)	07	129,400 \$		129,400 S	129,400 \$	129,400 \$	129,400 \$	129,400 S	129,400 \$	129,400 \$	129,400 \$	129,400 \$	129,400 \$	129,400 \$	129,400 \$	129,400
Net Income Cash Flow Cumulative Cash Flow Present Value of Cash Flow (NPV, i=3%) Cumulative Present Value Net Present Value (NPV, i=3%)		(116,300) S (116,300) S (116,300) S (116,300) S (113,000) S (113,000) S (113,000) S (113,000) S (3,629,100) S	~~~~	(116,300) \$ (116,300) \$ (232,600) \$ (109,700) \$ (222,700) \$	(116.300) \$ (116.300) \$ (348.900) \$ (106.500) \$ (329.200) \$	(116,300) \$ (116,300) \$ (465,200) \$ (103,400) \$ (432,600) \$	(116.300) \$ (116.300) \$ (581,500) \$ (100.400) \$ (533,000) \$	(116,300) \$ (116,300) \$ (97,500) \$ (630,500) \$	(116,300) S (116,300) S (814,100) S (94,600) S (725,100) S	(116,300) \$ (116,300) \$ (930,400) \$ (91,900) \$ (817,000) \$	(116,300) \$ (116,300) \$ (1,046,700) \$ ( (89,200) \$ (906,200) \$	(116.300) \$ (116.300) \$ (1,163,000) \$ ( (86.600) \$ (992,800) \$ (	(116,300) \$ (116,300) \$ (1,279,300) \$ ( (84,100) \$ ( (1,076,900) \$ (	(116,300) \$ (116,300) \$ 1,395,600) \$ (81,600) \$ 1,158,500) \$ 1,158,500) \$	(116,300) \$ (116,300) \$ (1,511,900) \$ ( (79,300) \$ (1,237,800) \$ (	(116,300 (116,300 1,628,200 (76,900 1,314,700

ation (\$KWh) n was calculated assuming consumption of 10 hours of continuous electricity per day from 290 KW capacity MSWF energy production system. Future demand may vary. for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. Service was calculated based on a projected prime interest rate of 6% (http://mortgage.x.com/general/indexes/prime_rate_forecast asp)

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Expected LFG energy project lifetime (yrs) Project Year Year of operation	15 2024 0	2025 1		2026 2	2027 3	2028 4	2029 5	2030 6	2031 7	2032 8	2033 9	2034 · 10	2035 11	2036 12	2037 13	2038 14
Annual Return ^(a)		5	21,700 \$	21,700 \$	21,700 \$	21,700 S	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700
Installed Capital Cost LFG Collection System ( $\$^{(b)}$ $\$$ Installed Capital Cost Small Engine Energy System ( $\$^{(b)}$ $\$$	617,000 271,000															
Annual O&M Cost LFG Collection System (\$) Annual O&M Cost Energy System(\$)		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 S 14,000 S	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 \$ 14,000 \$	59,800 14,000
Annual Debt Service ^(c)		6	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500 S	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500 \$	91,500
Net Income Cash Flow Cumulative Cash Flow Present Value of Cash Flow (NPV, i=3%) Cumulative Present Value Net Present Value (NPV, i=3%)		\$ (143,600) \$ (143,600) \$ (143,600) \$ (143,600) \$ (139,500) \$ (139,500) \$ (1,715,000)	ຑຑຑຑຑ	(143,600) \$ (143,600) \$ (287,200) \$ (135,400) \$ (274,900) \$	(143,600) S (143,600) S (430,800) S (131,500) S (406,400) S (406,400) S	(143,600) S (143,600) S (574,400) S (127,600) S (127,600) S (534,000) S	(143,600) \$ (143,600) \$ (718,000) \$ (718,000) \$ (123,900) \$ (657,900) \$	(143,600) \$ (143,600) \$ (861,600) \$ (120,300) \$ (778,200) \$	(143,600) S (143,600) S (1,005,200) S ( (116,800) S (895,000) S (	<pre>\$ (143,600) \$ \$ (143,600) \$ \$ (143,600) \$ \$ (1,148,800) \$ \$ (1,148,800) \$ \$ \$ (113,400) \$ \$ \$ (1,008,400) \$ \$ \$ \$ (1,008,400) \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</pre>	(143,600) S (143,600) S (1,292,400) S ( (110,100) S (1,118,500) S (	(143,600) \$ (143,600) \$ (1,43,600) \$ (1,436,000) \$ (1,225,400) \$ (1,225,400) \$	(143,600) \$ (143,600) \$ (1,579,600) \$ (103,800) \$ (1,329,200) \$	(143,600) \$ (143,600) \$ (1,723,200) \$ (100,800) \$ (1,430,000) \$	(143,600) \$ (143,600) \$ (1,866,800) \$ ( (97,800) \$ ( 1,527,800) \$ (	\$ (143,600) \$ (143,600) \$ (2,010,400) \$ (95,000) \$ (1,622,800)

ation (SKWh) New scaludlated assuming consumption of 10 hours of continuous electricity per day from 41 kW capacity PRD energy production system. Future demand may vary. To both LFG collection systems and energy production systems included an additional 40% cost factor for on-Island construction in Saipan. Service was calculated based on a projected prime interest rate of 6% (http://mortgage.x.com/general/indexes/prime_rate_forecast.asp)

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					noilqu - UHH	1 (Electricity G	ארט - Uption 1 (בופכתיכוץ Generation using Small Keciprocating בחפוחe)	small Keciprocati	ng Engine)							
ysis Expected LFG Energy Project Lifetime (yrs) Project Year Year of operation	15 2024 0	2025 1		2026 2	2027 3	2028 4	2029 5	2030 6	2031 7	2032 8	2033 9	2034 10	2035 11	2036 12	2037 13	2038 14
Annual Return ^(a)		S 21.	21,700 \$	21,700 \$	21,700 \$	21,700 \$	\$ 21.700 \$	21,700 S	21,700 S	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700 \$	21,700
Installed Capital Cost LFG Collection System (\$) ^(b) $$ Installed Capital Cost Small Engine Energy System (\$) ^(b) $$	617,000 133,000															
Annual O&M Cost LFG Collection System (\$) Annual O&M Cost Energy System(\$)		5 59,	59,800 \$ 11,200 \$	59,800 S 11,200 S	59,800 \$ 11,200 \$	59,800 5 11,200 5	\$ 59,800 \$ \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 \$ 11,200 \$	59,800 11,200
Annual Debt Service ^(c)		\$ 77,	77,300 \$	77,300 \$	77,300 \$	77,300 \$	\$ 77,300 \$	77,300 S	77,300 \$	77,300 \$	77,300 \$	77,300 \$	77,300 \$	77,300 \$	77,300 \$	77,300
Net Income Cash Flow Cumulative Cash Flow Present Value of Cash Flow (NPV, I=3%) Cumulative Present Value Net Present Value (NPV, I=3%)		<pre>\$ (126.600) \$ (126.600) \$ (126.600) \$ (126.600) \$ (123.000) \$ (123.000) \$ (1.513.000) \$ (1.513.000)</pre>	~~~	(126,600) S (126,600) S (253,200) S (119,400) S (242,400) S (242,400) S	(126,600) \$ (126,600) \$ (379,800) \$ (115,900) \$ (358,300) \$ (358,300) \$	(126,600) (126,600) (506,400) (112,500) (470,800)	\$ (126.600) \$ \$ (126,600) \$ \$ (633.000) \$ \$ (109.300) \$ \$ (580.100) \$ \$ (580.100) \$	(126,600) \$ (126,600) \$ (759,600) \$ (106,100) \$ (686,200) \$	(126,600) \$ (126,600) \$ (886,200) \$ (103,000) \$ (789,200) \$	\$ (126,600) \$ \$ (126,600) \$ \$ (1.012.800) \$ \$ (1.012.800) \$ \$ (100,000) \$ \$ (889,200) \$	(126,600) S (126,600) S (1,139,400) S (97,100) S (986,300) S (	(126,600) (126,600) 1,266,000) (94,300) 1,080,600)	(126,600) \$ (126,600) \$ (1,392,600) \$ (91,500) \$ (1,172,100) \$ (1,172,100) \$	(126,600) \$ (126,600) \$ (1,519,200) \$ (88,800) \$ (1,260,900) \$	(126,600) \$ (126,600) \$ (1645,800) \$ ( (86,300) \$ (1,347,200) \$ ( (1,347,200) \$ (	\$ (126,600 \$ (126,600 \$ (1,772,400 \$ (83,700 \$ (1,430,900

ation (\$KWh) T was calculated assuming consumption of 10 hours of continuous electricity per day from 41 kW capacity PRD energy production system. Future demand may vary. To thoth LFG collection systems and energy production systems included an additional 40% cost factor for on-Island construction in Saipan. Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)

MSWH - Uption 3 (Leachate Evaporator)

2038 14	,		\$ 62,40 \$ 146,20	\$ 79,30	\$ (287,90) \$ (287,90) \$ (3,980,60) \$ (190,40) \$ (3,204,20)
2037 13			62,400 146,200	79,300	\$ (287,900) \$ (287,900) \$ (3,692,700) \$ (196,100) \$ (3,013,800) \$ (3,013,800)
2036 12			62,400 S 146,200 S	79,300 \$	\$ (287,900) 5 \$ (287,900) 5 \$ (3,404,800) 5 \$ (202,000) 5 \$ (2,817,700) 5
2035 11	نې ۱		62,400 \$ 146,200 \$	79,300 \$	(287,900) \$ (287,900) \$ (3,116,900) \$ (208,000) \$ (2,615,700) \$
2034 10	69 1		62,400 \$ 146,200 \$	79,300 \$	(287,900) \$ (287,900) \$ (2.829,000) \$ (2.829,000) \$ (214,300) \$ (2.407,700) \$
2033 9	\$ <del>9</del>		62,400 \$ 146,200 \$	79,300 \$	(287,900) \$ (287,900) \$ (2.541,100) \$ ( (2.541,100) \$ ( (220,700) \$ (2,193,400) \$ ()
2032 8	\$		62,400 \$ 146,200 \$	79,300 \$	(287,900) \$ (287,900) \$ (2.253.200) \$ (2 (2.253.200) \$ (2 (1,972,700) \$ (2
2031 2 7	\$		62,400 S 146,200 S	79,300 \$	\$ (287,900) \$ ( \$ (287,900) \$ ( \$ (1,965,300) \$ (2 \$ (234,100) \$ (2 \$ (1,745,400) \$ (1
2030 2 6	5		62,400 \$ 146,200 \$	79,300 S	\$ (287,900) \$ ( \$ (287,900) \$ ( \$ (1.677,400) \$ (1 \$ (241,200) \$ (1 \$ (1,511,300) \$ (1
2029 2 5	<b>\$</b>		62,400 S 146,200 S	79,300 \$	\$ (287,900) \$ ( \$ (287,900) \$ ( \$ (1,389,500) \$ ( \$ (1,389,500) \$ (1 \$ (270,100) \$ (1 \$ (1,270,100) \$ (1
2028 4	\$		62,400 S 146,200 S	79,300 \$	(287,900) \$ (287,900) \$ (1,101,600) \$ (255,800) \$ (1,021,700) \$ (1,021,700) \$
2027 3	, S		62,400 S 146,200 S	79,300 \$	(287,900) \$ (287,900) \$ (813,700) \$ (1 (263,500) \$ (765,900) \$ (1
2026 2	\$		62,400 S 146,200 S	79,300 \$	(287,900) \$ (287,900) \$ (525,800) \$ (271,400) \$ (502,400) \$ (502,400) \$
2025	50,000 \$		62,400 S 146,200 S	79,300 \$	(237,900) \$ (237,900) \$ (237,900) \$ (231,000) \$ (231,000) \$ (7,397,400) \$
45 2024 0	\$	1,079,000 146,200	<i>м</i> м	s	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Expected LFG Energy Project Lifetime (yrs) Year Year of operation	Annual Return ^(a)	Installed Capital Cost LFG Collection System (\$) ^(b) \$ 1,079,000 apital and O&M Costs Leachate Evaporator System (\$) ^(b) \$ 146,200	Annual O&M Cost LFG Collection System (\$) Annual O&M Cost Leachate Evaporator System (\$)	Annual Debt Service ^(c)	Net Income Cash Flow Cumulative Cash Flow Present Value of Cash Flow (NPV, i=3%) Cumulative Present Value Net Present Value (NPV, i=3%)
Expected		Installed Capital apital and O&M Costs L	Annual O&N Annual O&M Cost		Presen

In was calculated from the capital cost of additional leachate pond construction that would be replaced by the leachate evaporator system. for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. Service was calculated based on a projected prime interest rate of 6% (http://mortgage.x.com/general/indexes/prime_rate_forecast.asp)

MSWH - Uption 3 (Leachate Evaporator)

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2053 29	1		62,400 146,200	101,600	(310,200) (310,200) (8,561,300) (131,700) (5,607,700)
	ŝ		0 N 0	0 \$	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2052 28	,		62,400 146,200	101,600	(310,200) (310,200) (8,251,100) (135,600) (5,476,000)
	ŝ		00 S	S 00	s s s s s s s s s s s s s s s s s s s
2051 27			62,400 146,200	101,600	s (310,200) s (310,200) s (7,940,900) s (139,700) s (5,340,400)
	\$		20 S	\$ 00	
2050 26	1		62,400 146,200	101,600	(310,200) (310,200) (7,630,700) (143,900) (143,900) (5,200,700)
	69		00 S	\$ 00	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
2049 25	2		62,400 146,200	101,600	(310,200) (310,200) (7,320,500) (148,200) (5,056,800)
	\$		00 s	\$ OC	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
2048 24	,		62,400 146,200	101,600	(310,200) (310,200) (7,010,300) (152,600) (4,908,600)
	ŝ		00 S	\$ 00	s s s s s 0 0 0 0 0 0
2047 23	1		62,400 146,200	101,600	(310,200) (310,200) (6,700,100) (157,200) (4,756,000)
	\$		s s 0 0	\$ 0	s s s s 0 0 0 0 0
2046 22	L.		62,400 146,200	101,600	(310,200) (310,200) (6,389,900) (161,900) (4,598,800)
	\$		00 S	\$ 00	() () () () () () () () () () () () () (
2045 21	C		62,400 146,200	101,600	(310,200) (310,200) (6,079,700) (166,800) (4,436,900)
	\$		0 5	\$ 00	s s s s s (0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2044 20	U.		62,400 146,200	101,600	<pre>\$ (310,200) \$ (310,200) \$ (5,769,500) \$ (5,769,500) \$ (171,800) \$ (4,270,100)</pre>
	ŝ		00 S	00 S	
2043 19	1		62,400 146,200	101,600	(310,200) (310,200) (5,459,300) (177,000) (4,098,300)
	\$		00 S	\$ 00	00000
2042 18	'		62,400 146,200	101,600 \$	Net Income         \$ (260,200)         \$ (310,200)         \$ (310,200)         \$ (310,200)           Cash Flow         \$ (260,200)         \$ (310,200)         \$ (310,200)         \$ (310,200)           Cash Flow         \$ (260,200)         \$ (310,200)         \$ (310,200)         \$ (310,200)         \$ (310,200)           Cumulative Cash Flow         \$ (4,528,700)         \$ (4,838,900)         \$ (3,49,100)         \$ (347,700)           Of Cash Flow (NPV, i=3%)         \$ (162,200)         \$ (187,700)         \$ (182,300)         \$ (4,098,300)           Cumulative Present Value         \$ (3,551,300)         \$ (3,739,000)         \$ (3,321,300)         \$ (4,098,300)
	\$		20 S	\$ 00	2000 2000 2000 2000 2000 2000 2000 200
2041			62,400 146,200	: 101,600 \$	(310,2) (310,2) (4.838,9) (4.838,9) (187,7) (187,7) (3,739,0)
	00		62,400 S 46,200 S	00	
2040 16	50,000		-	\$ 101,600 \$	(260,2 (260,2 (4,528,7 (162,2 (162,2 (3,551,3
Year ation	Annual Return ^(a) S	(q) (s) (p)	Annual O&M Cost LFG Collection System (\$) 8 Annual O&M Cost Energy System(\$) 8	Annual Debt Service ^(c) \$	Net Income S Cash Flow S Cumulative Cash Flow S Present Value of Cash Flow (NPV, i=3%) S Cumulative Present Value S Net Present Value (NPV, i=3%)
Year Year of operation	Retui	tem (	yster	Servic	Net Income Cash Flow Cash Flow alue of Cash Flow (NPV, j=3%) Cumulative Present Value Net Present Value (NPV, j=3%)
ar of e	nnual	or Sys	tion S ergy S	Debt	Ne C C Dw (N Dw (N Pres Ue (N
Ye	A	llectic	collect st En	nnual	umula Ish Flo Ilative nt Val
		FG Co te Eva	M Co:	A	Cr of Ca Cumu
		tost L sacha	Cost Ial 08		Value Net
		Installed Capital Cost LFG Collection System (\$)^{(b)} ilized Capital and O&M Costs Leachate Evaporator System (\$)^{(b)}	I O&M Annl		esent
		ed Ca &M Cc	Innua		ā
		Install and O	-		
		pital			
		ted Ca			
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ial Return was calculated from the capital cost of additional leachate pond construction that would be replaced by the leachate evaporator system. tal costs for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. al Debt Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp) MSWF - Uption 3 (Leachate Evaporator)

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2068 44	ī.		62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (13,606,700) \$ (13,606,700) \$ (7,307,000) \$ (7,307,000)
	69		\$	69	
2067 43	х		62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (13,264,900) \$ (95,900) \$ (7,213,800)
	\$		s s o o	0 \$	
2066 42			62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$(12,923,100) \$ (7,117,900) \$ (7,117,900)
	69		00 \$	\$ 00	
2065 41			62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (12,581,300) \$ (101,800) \$ (7,019,100) \$ (7,019,100)
			00 2	00 \$	
2064 40	, 63		62,400 146,200	\$ 133,200	\$ (341,800) \$ (341,800) \$ (12,239,500) \$ (104,800) \$ (6,917,300)
			000	000	
2063 39	6		\$ 62,400 \$ 146,200	\$ 133,200	\$ (341,800) \$ (341,800) \$ (11,897,700) \$ (108,000) \$ (6,812,500)
			000	000	
2062 38	5		6 62,400 5 146,200	133,200	\$ (341,800) \$ (341,800) \$ (11,555,900) \$ (111,200) \$ (6.704,500)
			000	000	
2061 37	(8		62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (11,214,100) \$ (114,600) \$ (6,593,300)
	07		00 S	00 \$	
2060 36	10		62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (10,872,300) \$ (118,000) \$ (6,478,700) \$ (6,478,700)
			000	\$ 00	
2059 35			62,400 146,200	133,200	\$ (341,800) \$ (341,800) \$ (10,530,500) \$ (121,500) \$ (6,360,700) \$ (6,360,700)
			00 S	00 S	
2058 34			62,400 146,200	133,200	s (341,800) s (341,800) s (10,188,700) s (125,100) s (6,239,200)
			000	500	
2057 33	6		62,400 146,200	133,200	<ul> <li>(341,8)</li> <li>(341,8)</li> <li>(341,8)</li> <li>(9,846,9)</li> <li>(128,9)</li> <li>(128,9)</li> <li>(6,114,1)</li> </ul>
			000	000	
2056 32	s		\$ 62,400 \$ 146,200	\$ 133,200 \$	Net Income         \$         (291,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$         (341,800)         \$ <t< td=""></t<>
	50,000		62,400 146,200	200	800) 800) 400) 400)
2055 31				Annual Debt Service ^(e) \$ 133,200 \$	\$ (291,8 \$ (291,8 \$ (9,163,5 \$ (116,8 \$ (5,852,4
Year ation	Annual Return ^(a) S	(\$) ^(b)	n (\$) m(\$)	(ce ^(c)	Flow 3%) alue 3%)
Year Year of operation	l Retu	stem	Syster	Servi	Net Income Cash Flow Cumulative Cash Flow Cash Flow (NPV, j=3%) Cumulative Present Value Net Present Value (NPV, j=3%)
ear of	Annua	on Sy tor Sy	tion (	I Debt	N low (N lue (N
×		ollecti apora	Collect Dist Er	Annua	tumuk ash Fl nulativ ent Va
		FG C ate Ev	t LFG &M Co		e of C Curr t Pres
		Cost each.	O&M Cost LFG Collection System (\$) Annual O&M Cost Energy System(\$) \$		ıt Valu Net
		Installed Capital Cost LFG Collection System (\$) $^{(b)}$ and O&M Costs Leachate Evaporator System (\$) $^{(b)}$	Annual Q&M Cost LFG Collection System (\$) \$ Annual Q&M Cost Energy System(\$) \$		resen
		offed C	Annu		-
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		Installed Capital Cost LFG Collection System (\$)^{(b)} ilized Capital and O&M Costs Leachate Evaporator System (\$)^{(b)}			
		lized (			
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Ial Return was calculated from the capital cost of additional leachate pond construction that would be replaced by the leachate evaporator system. Ial costs for both LFG collection systems and energy production systems included an additional 40% cost factor for on-island construction in Saipan. Ial Debt Service was calculated based on a projected prime interest rate of 6% (http://mortgage-x.com/general/indexes/prime_rate_forecast.asp)



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